

GaN Integration Enables Next Generation USB-C Chargers with Ultra-High Power Density and Wide Output Voltage Range

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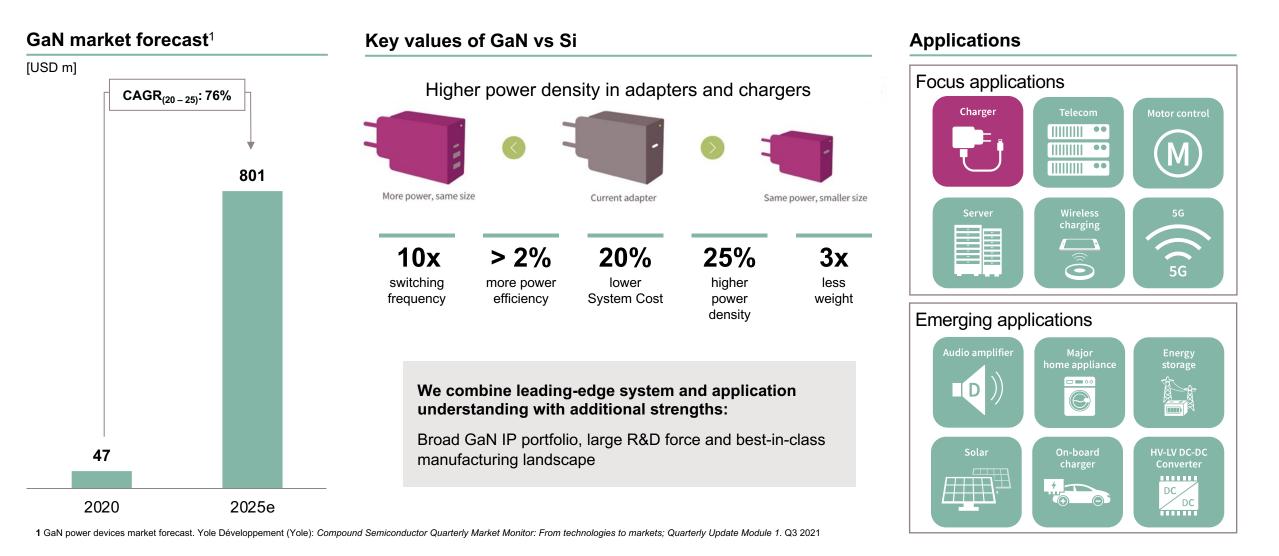




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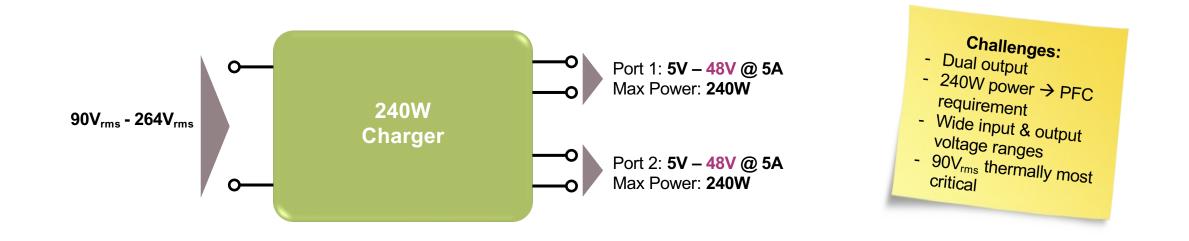


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Specifications of the over-next 240W ultra-high density charger generation

- > State-of-the-art 65W chargers soon no longer enough to charge all consumer devices → Increase to future-proof 240W
 > Dual USB-C output ports to support simulatenous charging of two mobile devices
- Increase of output voltage to 48V (USB PD Rev. 3.1)

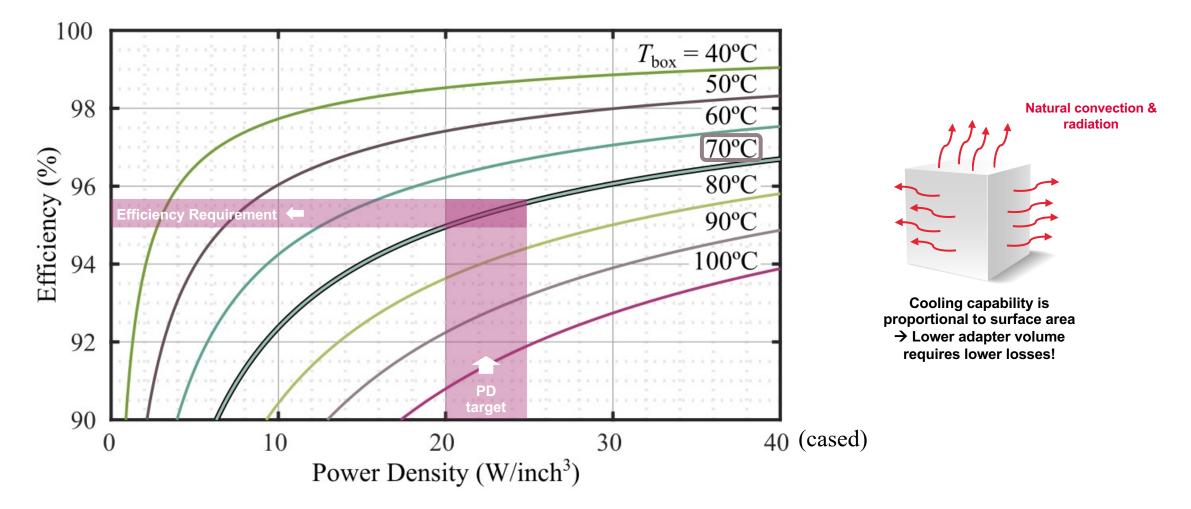


Charger specifications become more similiar to other applications with 48V and >200W like SmartTVs or All-in-One PCs!

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Efficiency & power density performance target for maximum case temperature

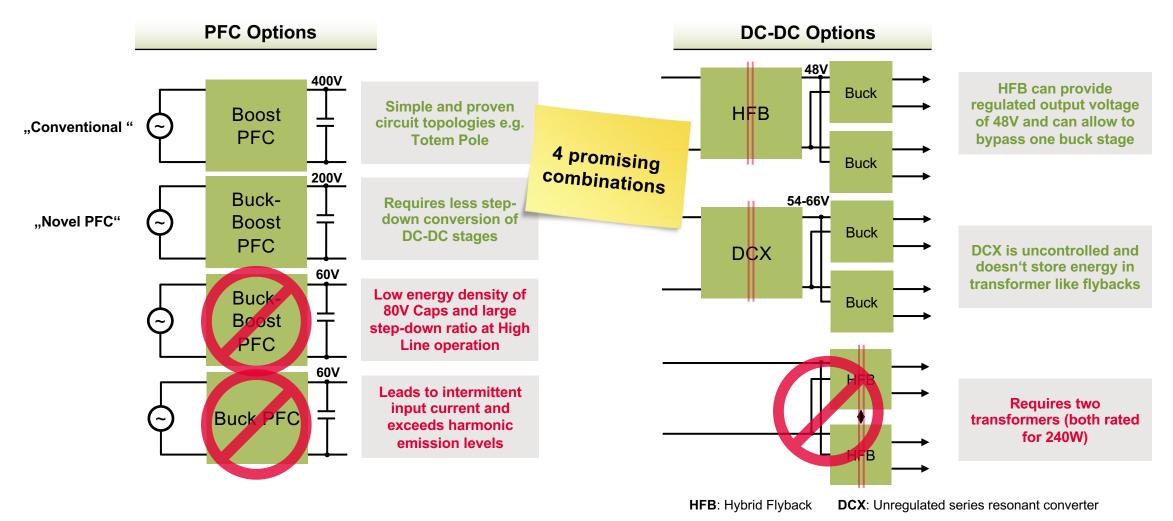
> Increasing power density requires higher efficiency to keep case temperature within limits!





Possible topologies and system partitioning

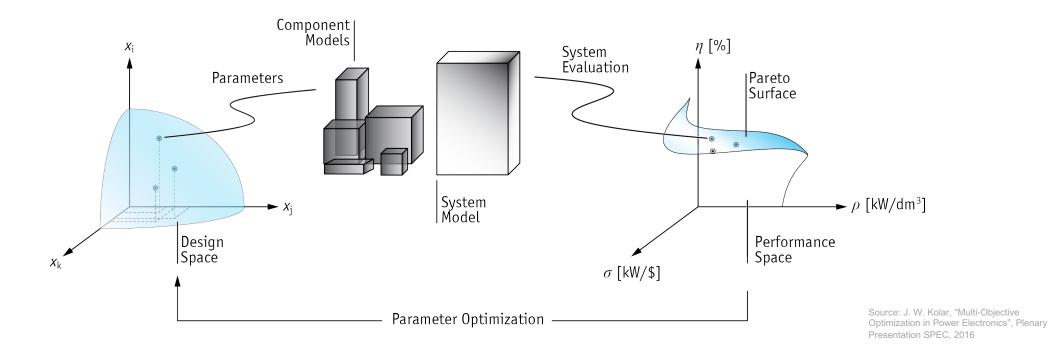
- > Final solution needs to have a PFC, galvanic isolation, and two regulated output ports.
- > Based on circuit simulations and rough size/loss estimations several solutions can be ruled out for this project.





Multi-objective Pareto optimization

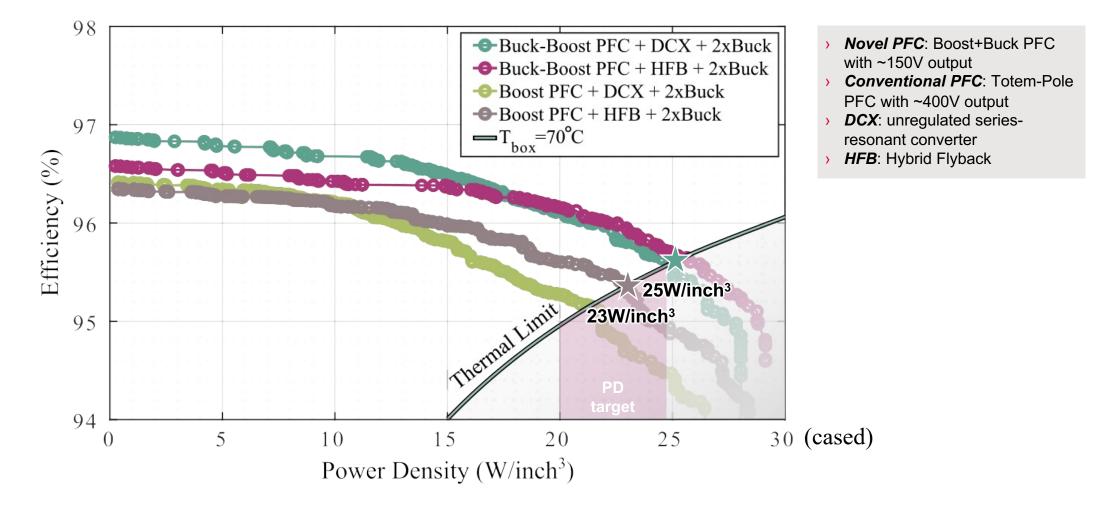
- > Systematic approach to consider all degrees of freedom
 - E.g.: Semiconductor technologies, # of HF legs in totem-pole, # of matrix transformers, switching frequencies, current/voltage ripples, magnetic component realizations,
 paralleling of switches
- > Comprehensive and **detailed modeling** of **components** and **systems behavior**
- > Finding trade-offs ("Pareto-Front") between Efficiency, Power Density, and Costs



Pareto optimization of 4 remaining converter options for the most challenging operating point



> Optimization results for **full load (240W)** and low line **(90V**_{rms})





23 W/in³

Conventional Solution (400V DC link): TP + HFB + 2x Buck

Why to use this solution:

- > Straightforward solution
- Proven controllers
- > Explore higher frequencies (within bounds of controllers)

Risks:

- Might miss target of 20W/in³
- > Not going to extreme power densities
- > Not learning about new topologies
- Missing chance to go to "new territory"

25 W/in³

Novel Solution (160V DC link): Boost+Buck PFC + DCX or HFB + 2x Buck

Why to use this solution:

- > Highest power density
- > Learning about new topology
- > Explore highest frequencies with proprietary control

Risks:

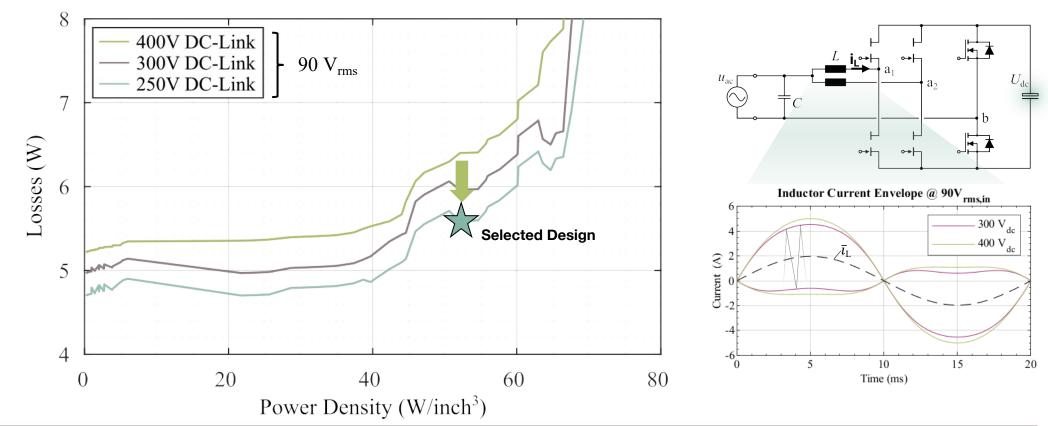
- > Not fulfilling requirements:
 - Standby power; Harmonics/EMI; Surge; ESD; Safety test (i.e. Short circuit)
- > Cost
 - High number of devices; controller development



Possibility to combine both solutions: "Boost Follower" Totem-Pole which is a conventional Totem-Pole that is operated with lower DC-link voltage depending on line voltage



Boost-Follower PFC operation to maximize efficiency at low-line operation



> Optimization of **Boost-Follower Totem-Pole PFC** stage at 240W and 90V_{rms} input

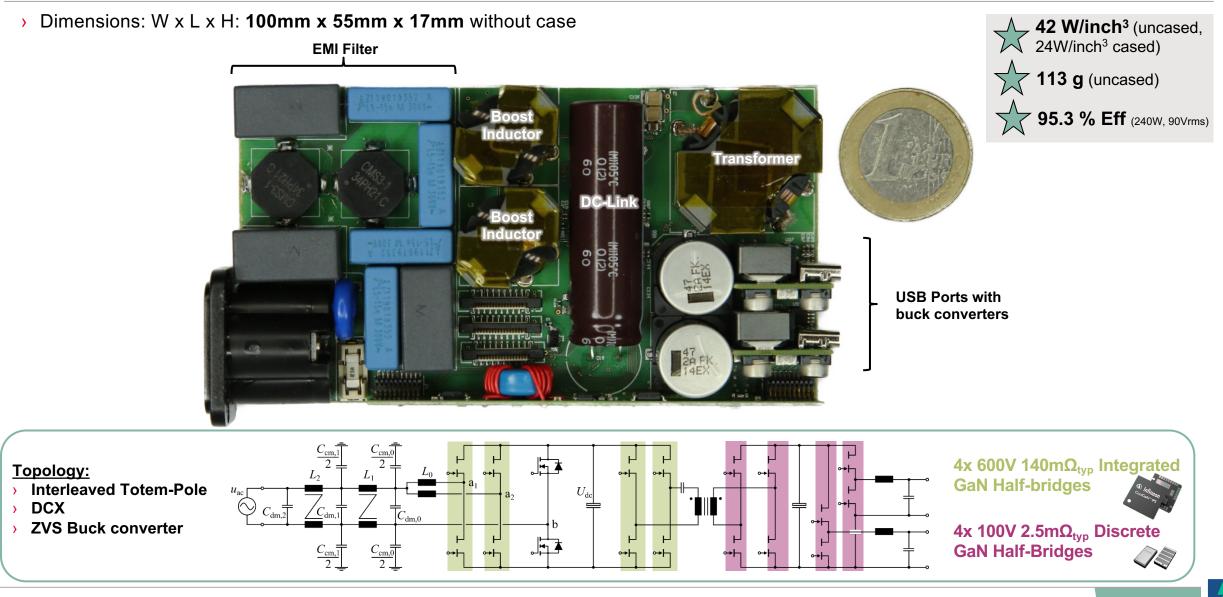
Novel Control Scheme: Variation of DC-link voltage for diff. line voltages to achieve ZVS at fixed f_{sw}

- > Reduction of losses at most critical $90V_{rms}$ operating point \rightarrow High $f_{sw} \rightarrow$ Low converter volume
- > Simplified control without variation of switching frequency like in TCM control
- > Easier EMI filter design with defined noise spectrum

 \rightarrow



Hardware Demonstrator of Next-Gen 240W USB-C Charger

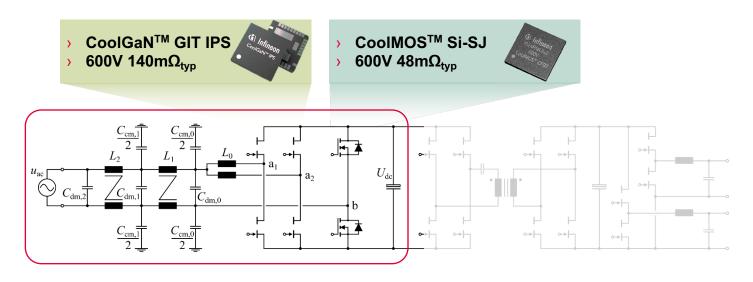


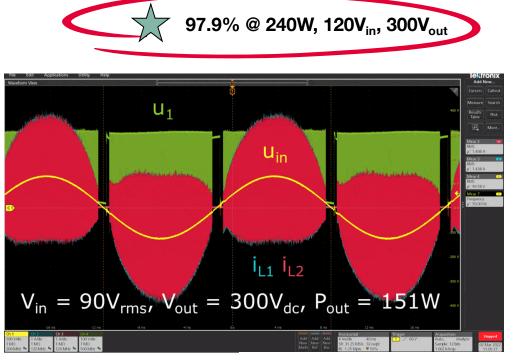


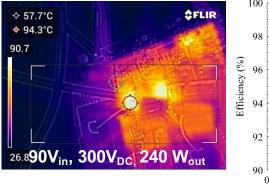
PFC Stage – Details and Measurement Results

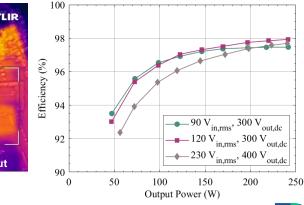
ZVS Totem-pole PFC with 2x interleaving

- > Fixed f_{sw} = 400kHz CCM PFC
- > Effective 800kHz for EMI Filter
- → Large Δi_L (L = 35 µH, Litz Wire) for natural ZVS → For All Voltage Ranges
- > **Operating-Point-Dependent** U_{dc} **variation** to always achieve ZVS
- > Easy-to-Implement Avg. Current Control



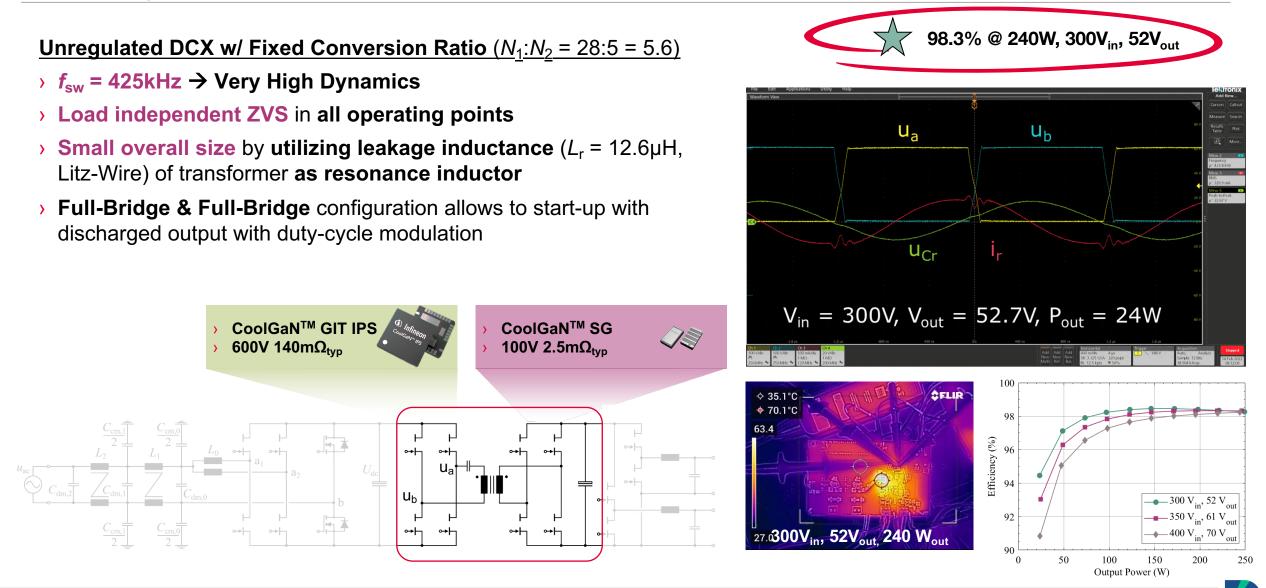








DCX stage details and measurement results

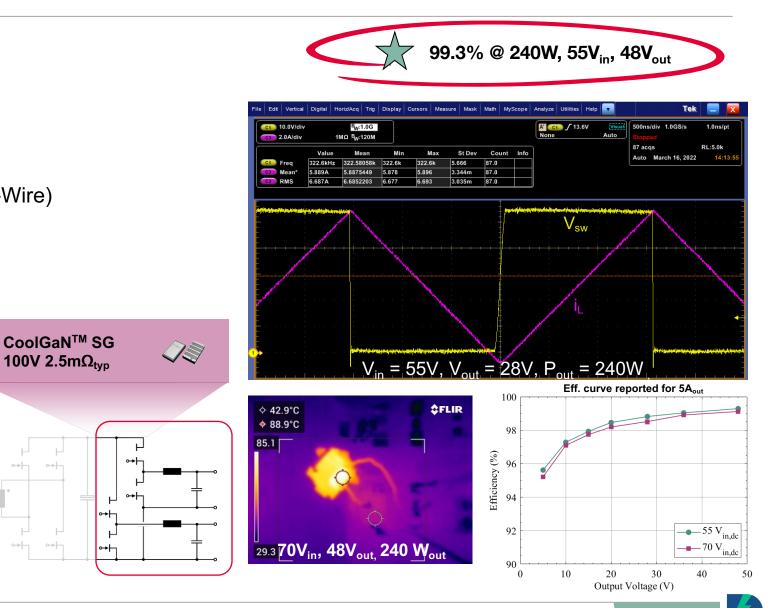




ZVS Buck Converter Stage

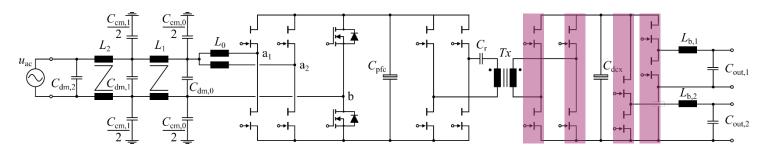
Full-ZVS Buck Stage

- > ZVS in All Operating Points
- > Enabled by:
 - Variable frequency: f_{sw} = 120...420 kHz
 - **Optimal Inductor Design** ($L = 3.6 \mu$ H, Litz-Wire)





Outlook: 100V CoolGaN[™] SG Integrated Power Stage

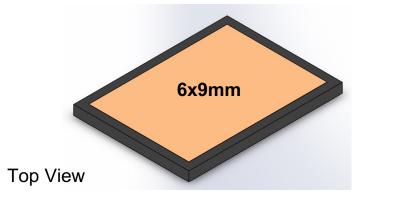


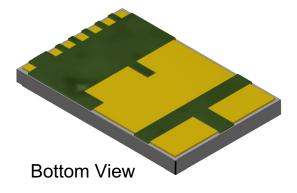
Size and BOM reduction with integrated 100V power stages

- > Half-bridge multi-chip module (MCM) in 6x9 mm laminate package:
 - 2x 100V 2.5mΩ_{typ} CoolGaN[™] SG HEMTs in half-bridge configuration
 - GaN-optimized half-bridge gate driver with regulated bootstrapping supply
 - ALL high-frequency capacitors included! PCB layout has no impact on switching performance or overshoot voltages, even on a single-layer PCB

> Thermally optimized package

- Copious thermal microvias connecting to large PCB pads
- Galvanically isolated top-side metal pad for easy heatsink attachment





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Conclusions

- > Unprecedented 240W USB-C charger power density (42 W/inch³ & 113g uncased, 24W/inch³ cased)
- Thoroughly optimized system performance due to Infineon's comprehensive technology portfolio and system expertise:
 - 600V CoolGaN[™] GIT Integrated Power Stage
 - 100V CoolGaN[™] Schottky Gate HEMTs
 - Matching gate drivers
 - Digital control with advanced modulation methods
 - Pareto multi-objective system optimization









Thank you for your interest!

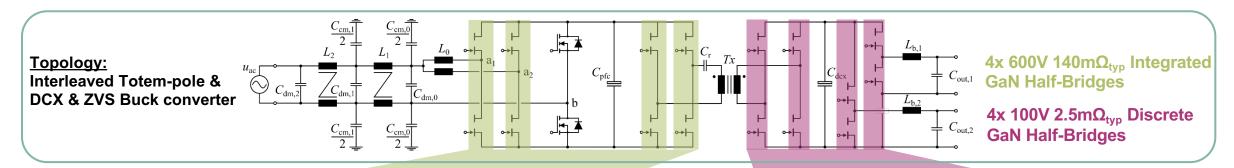
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Infineon CoolGaN[™] Solutions for 600V and 100V





600V CoolGaN[™] GIT Integrated Power Stage (IPS)

- > Isolated digital input with digital-in, power-out building block
- > Application configurable switching behavior
- > Fast, highly accurate, and stable timing
- Thermally enhanced 8x8mm QFN-28 and 6x8mm QFN-26 packages

- 100V CoolGaN™ Schottky Gate (SG) HEMT
- > Lower Q_{OSS} & more linear C_{OSS}
- > Lower Q_G and no Q_{rr}
- > 3x5 mm PQFN package with dual-sided cooling



TDI EiceDRIVER[™] for SG GaN

- > Optimized driving strength no gate resistors
- > Featuring TDI & active Miller clamp
- > 1.8x1.8mm TSNP package