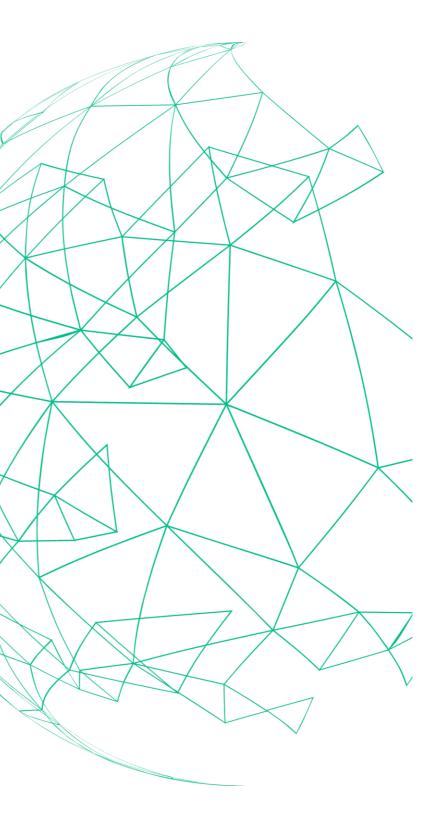


SiC MOSFET Corner and Statistical SPICE Model Generation

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- Motivation for Corner and Statistical SPICE models for power devices
- Discussion on Physically Based SPICE Models
- Backward Propagation of Variance (BPV) Technique Applied to SiC **MOSFETs**
- Experimental Results and Verification
- Conclusion

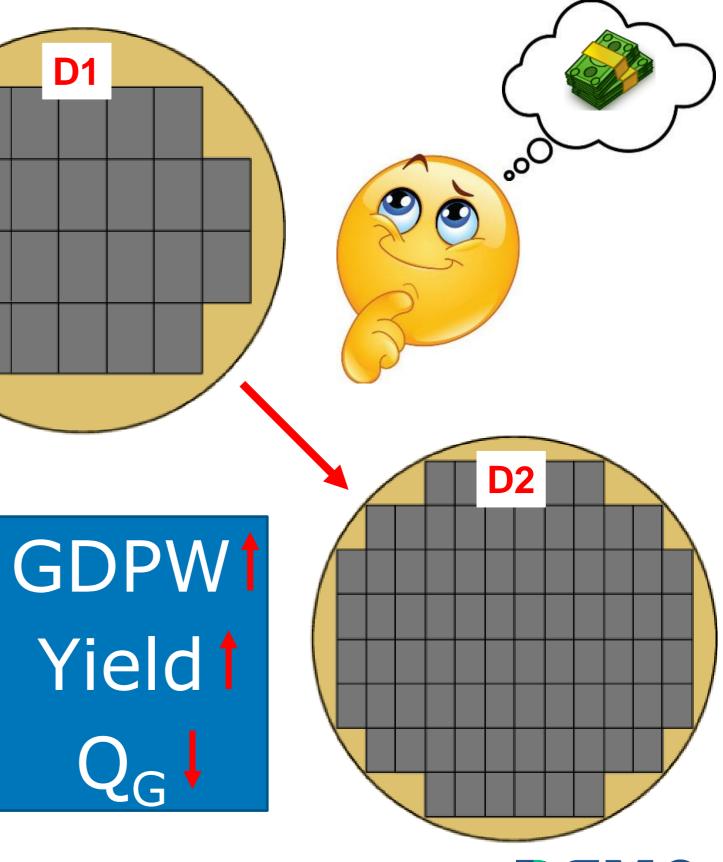




Why do we care about corner and statistical SPICE models in power devices?

 Datasheets historically contain wide uncorrelated parameter ranges that are not always representative of the true manufacturing process variation.

RDSon Variation	RDSon MAX	RDSon Typical	Die Area	D1 > D2
25%	1	0.8	D1	
11%	1	0.9	D2	







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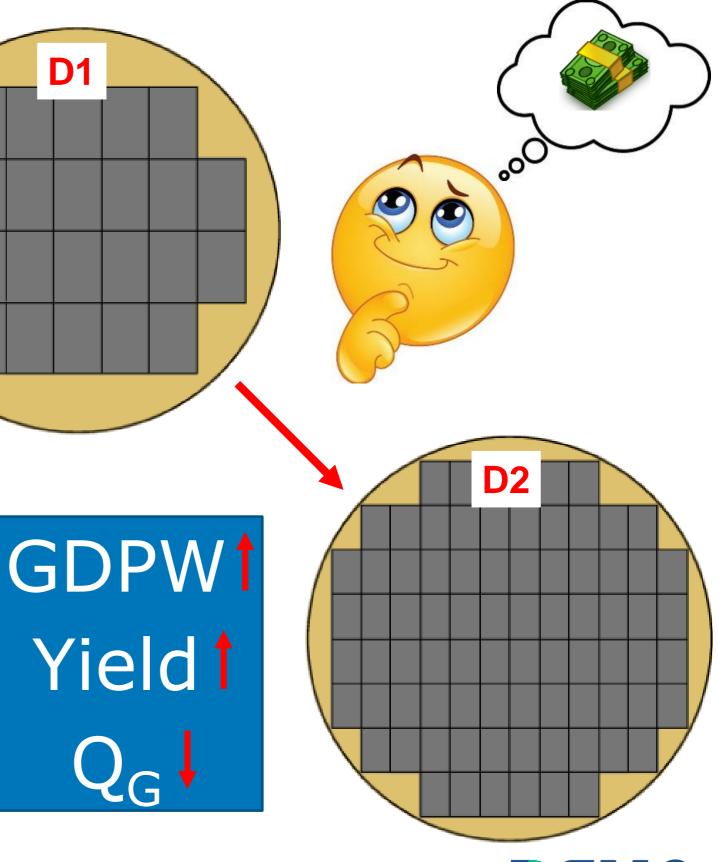
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Design for optimized performance and robustness to semiconductor process variation through simulation is critical to ensure high yield and high performance of a chip throughout the manufacturing lifetime. This is well understood in the IC CAD industry.

Why not in power devices?

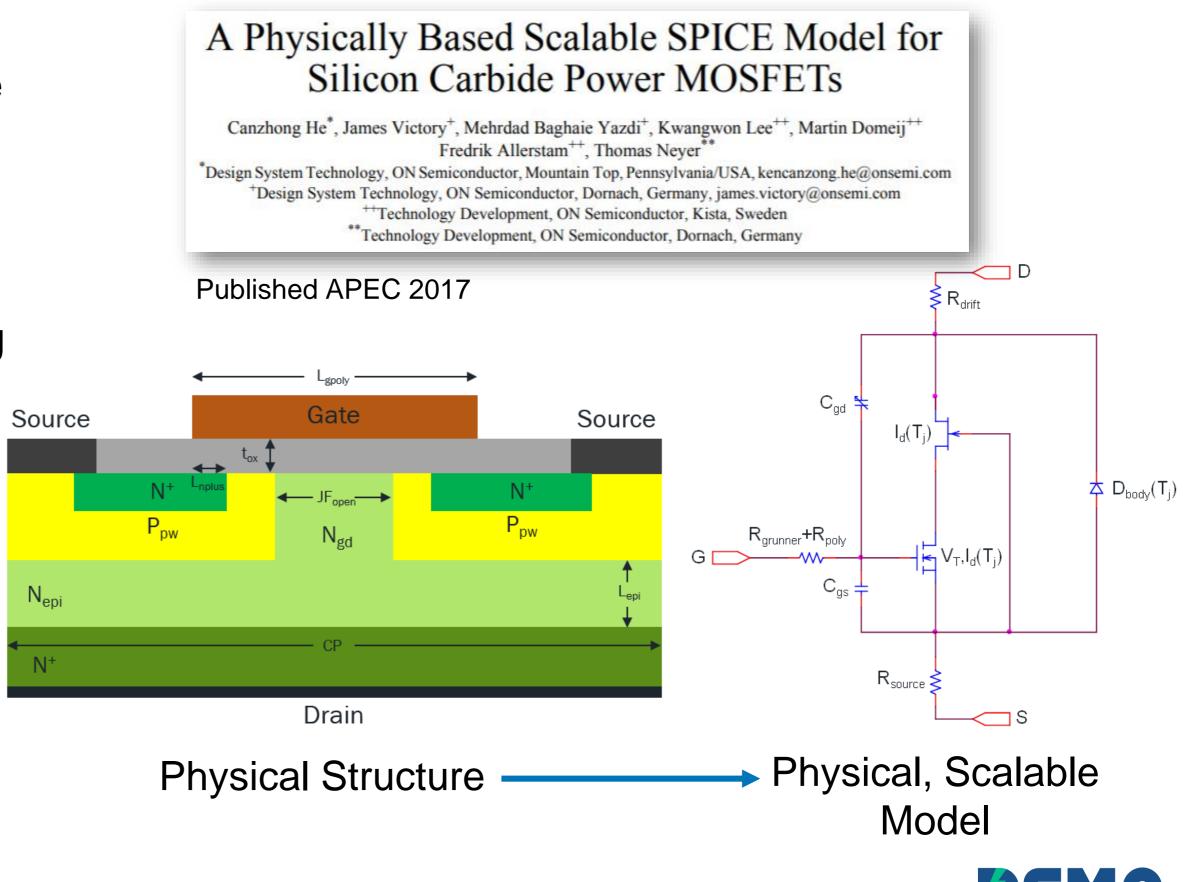
D1





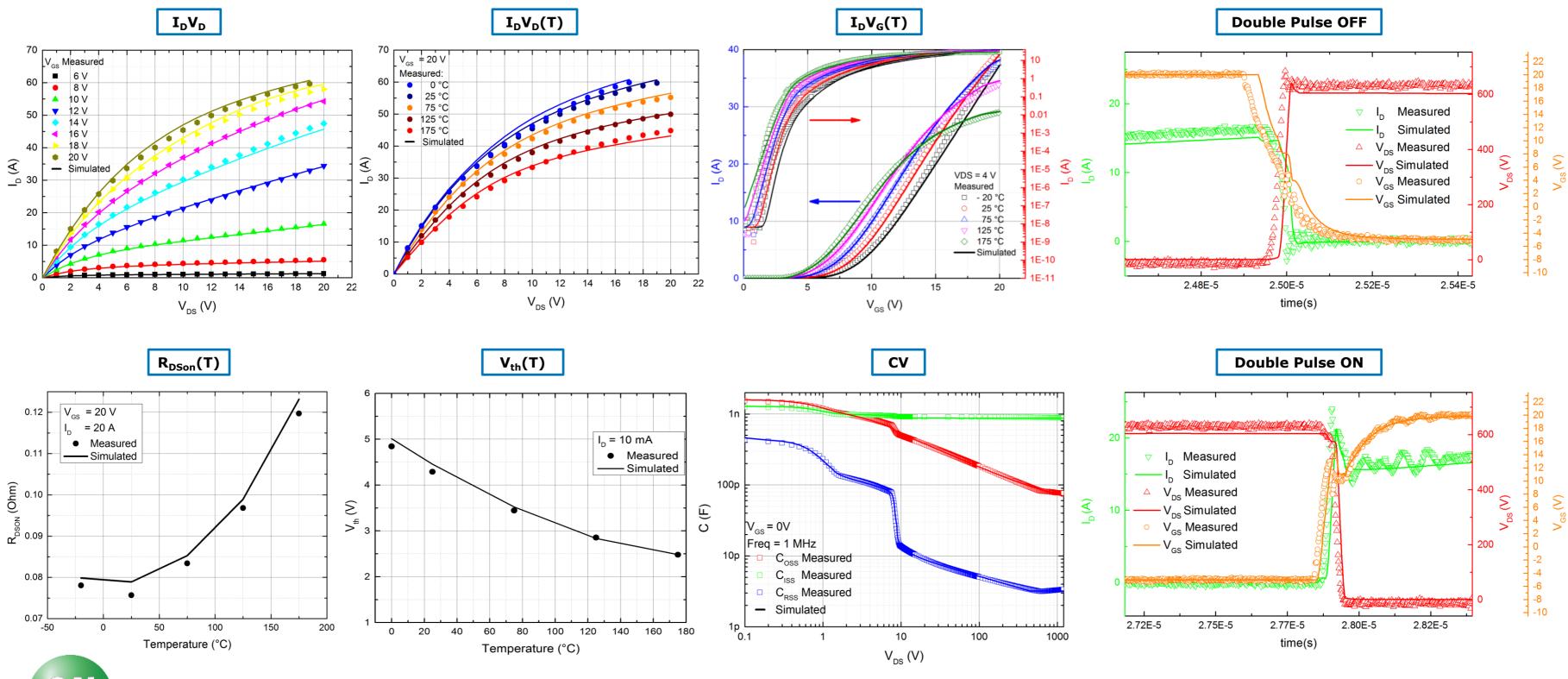
Discussion on Physically Based SPICE Models

- SPICE models should be physically based and scalable with process and layout parameters.
 - Enables accurate, consistent, and correlated process variation modeling and simulation
 - IC industry standard practice
- Recent advances in power device modeling has opened the door to apply physically based, statistical techniques for process variation simulation.





Typical SiC MOSFET SPICE Model Results







- Variances (σ^2) of electrical • performances E are based on manufacturing data.
- Sensitivities $\frac{\partial E_i}{\partial P_i}$ are computed through SPICE model simulation.
- Goal is to accurately simulate the \bullet variation of electrical performances E.
- BPV equations solve for the variances of the SPICE model process parameters P.

"Guarantees"

SPICE E = Measured E

SPICE Process Parameters P Electrical Performances E

Parameter	Description
Тох	Gate Oxide Thickness
Lnplus	Gate Poly Overlap of N+ Source
JFopen	JFET Width
Lgpoly	Gate Poly Length
Nchpk	Peak Channel Doping
Ppw	Pwell Doping
Ngd	Epi Doping under Gate Poly, JFET
Lepi	Epi Thickness, distance btw deep Pwell
Nepi	Epi Doping
Mj	Body Diode Grading Coeff.
μch	Channel Mobility
μdr	Drift Mobility

$$\sigma_{\delta E_i}^2 = \sum_j \left(\frac{\partial E_i}{\partial P_j}\right) \cdot \sigma_{\delta P_j}^2$$



E	Description
Vth	Vth @ 5mA
RDSonhi	RDSon @ VG=20, ID=20
RDSonlo	RDSon @ VG=15, ID=5
BVdss	BV @ 100uA
CissHV	Ciss @ VD=20V
CrssLV	Crss @ VD=1mV
CrssMV	Crss @ VD=5V
CrssHV	Crss @ VD=20V
CossLV	Coss @ VD=1mV
CossHV	Coss@ VD=20V
Qg	Qg @ VDS=800, VG=20, ID=20

BPV Solution



BPV (Backward Propagation of Variance) Technique Applied to SiC MOSFETs

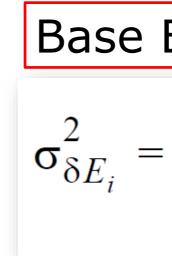
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"Guarantees"

SPICE E = Measured E

SPICE Process Parameters P

R_{DSon} or C There are un parameters that shifts in





ers P Electrical Performances E

There are <u>NO</u> parameters

$R_{\text{DSon}} \text{ or } C_{\text{rss}} \text{ for example}$

There are uncorrelated process parameters that induce correlated

shifts in R_{DSon} or C_{rss} .

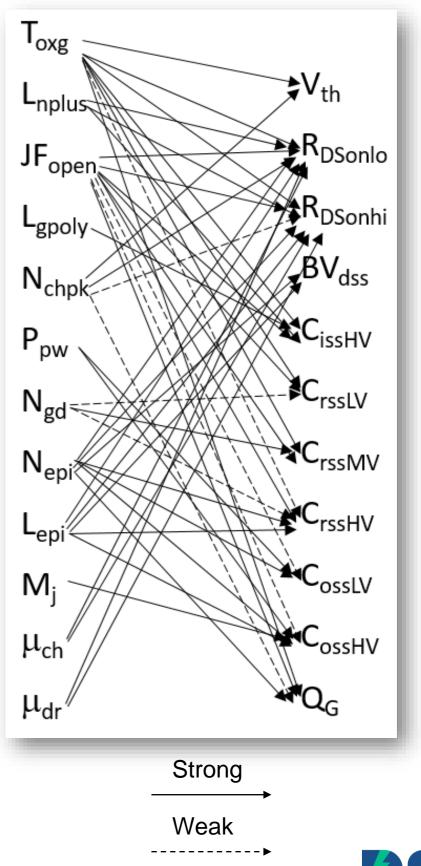
Base BPV Solution

$$= \sum_{j} \left(\frac{\partial E_i}{\partial P_j} \right) \cdot \sigma_{\delta P_j}^2$$



- E and P must be chosen such that perturbations in P are observable in of E.
 - Need a physical SPICE model with well defined P
 - Need consistent and sufficient E
 - In general, system should be X "equations" and X "unknowns".
 X=11 in our SiC MOSFET case.
- The technique fails when
 - There are inconsistencies in specification of the E statistics.
 Computed P variances can become negative.
 - The underlying SPICE models are inaccurate and unphysical leading to an ill conditioned sensitivity matrix.
- Not a "garbage in garbage out" process
 - Issues with the SPICE models and manufacturing data can be exposed through the BPV technique.







Full SiC MOSFET BPV Solution

$$\begin{bmatrix} \sigma_{\delta r_{ih}}^{2} - \left(\frac{\delta V_{ih}}{\delta I_{\sigma x}}\right)^{2} \sigma_{\delta r_{sc}}^{2} \\ \sigma_{\delta s D souh}^{2} - \left(\frac{\delta V_{ih}}{\delta I_{\sigma p x}}\right)^{2} - \left(\frac{\delta P_{ih}}{\delta I_{\sigma p x}}\right$$

FPV T_{ox}: Forward propagated parameters, $\sigma^2_{\delta T_{ox}}$ known from manufacturing

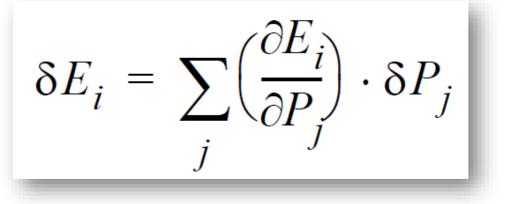




- Corner model solution has delta E as inputs and delta P as outputs.
- Same sensitivity matrix is used.
- E definition must be physically consistent based on known device correlations.
- Simple Worst and Best case could be defined based on R_{DSon} for example.
 - R_{DSon} and BV are positively correlated
- Corner definitions depends on what is important for designers.



Corner Model Solution

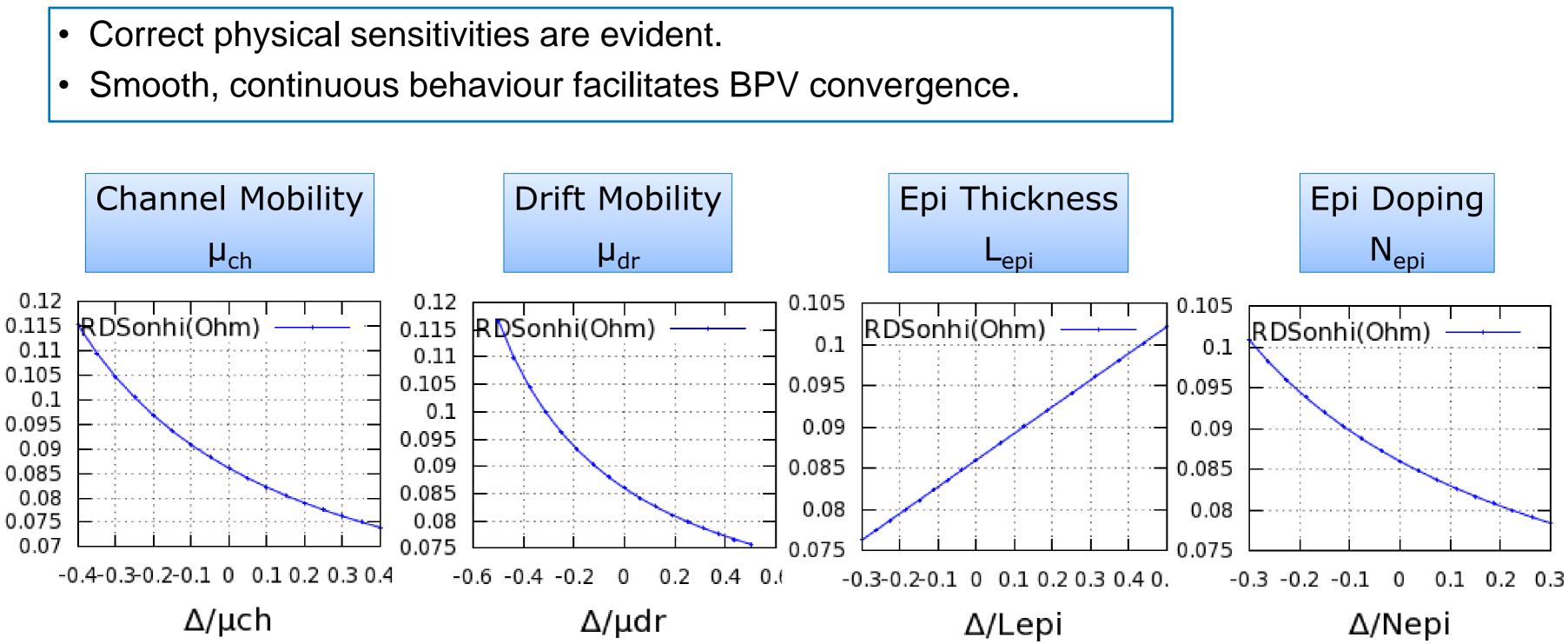


Е	Corner 1	Corner 2
Vth	LOW	HIGH
RDSonhi	LOW	HIGH
RDSonlo	LOW	HIGH
BVdss	LOW	HIGH
CissHV	HIGH	LOW
CrssLV	HIGH	LOW
CrssMV	HIGH	LOW
CrssHV	HIGH	LOW
CossLV	HIGH	LOW
CossHV	HIGH	LOW
Qg	HIGH	LOW



Sample R_{DSonhi} Sensitivity Plots

- Correct physical sensitivities are evident.







Variances in Electrical Performances Generated from Characterization Data

- Characterization (CZ) measurements of Electrical Specifications (E) performed on a small sample size.
- 4 Lots with 30 samples each = 120 points is enough to establish the physical correlations among the E.
- Variances (σ^2) of electrical performances E are established for the BPV solve. ullet

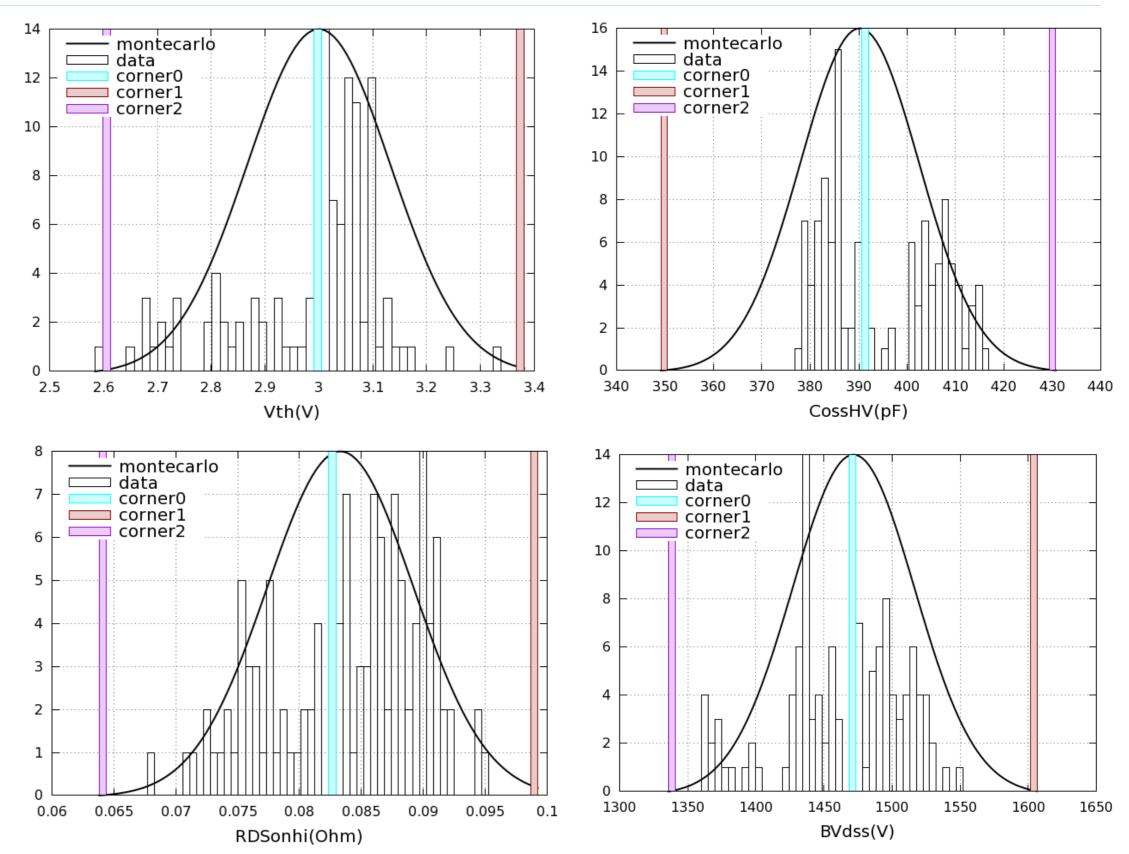
E	corner2	corner0	corner1	Description
Vth	0.8665	1	1.1335	Vth @ 5mA
RDSonhi	0.7879	1	1.2121	RDSon @ VG=20, ID=20
RDSonlo	0.7406	1	1.2594	RDSon @ VG=15, ID=5
BVdss	0.9073	1	1.0927	BV @ 100uA
CissHV	1.0814	1	0.9186	Ciss @ VD=20V
CrssLV	1.0669	1	0.9331	Crss @ VD=1mV
CrssMV	1.1092	1	0.8908	Crss @ VD=5V
CrssHV	1.1985	1	0.8015	Crss @ VD=20V
CossLV	1.032	1	0.968	Coss @ VD=1mV
CossHV	1.0902	1	0.9098	Coss@ VD=20V
Qg	1.0906	1	0.9094	Qg @ VDS=800, VG=20, ID=20

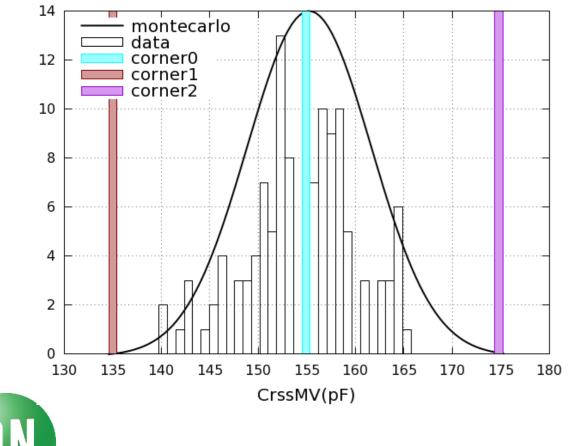




Sample Corner / Monte Carlo Gaussian Plots

- Gaussian distribution shows up for individual lots.
- Global Gaussian distribution starting to show up.

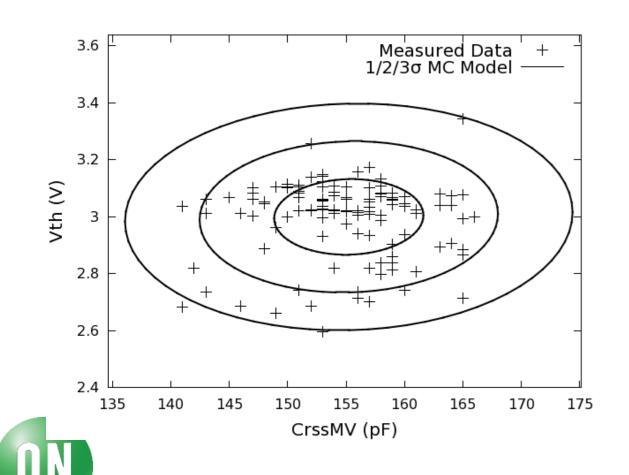


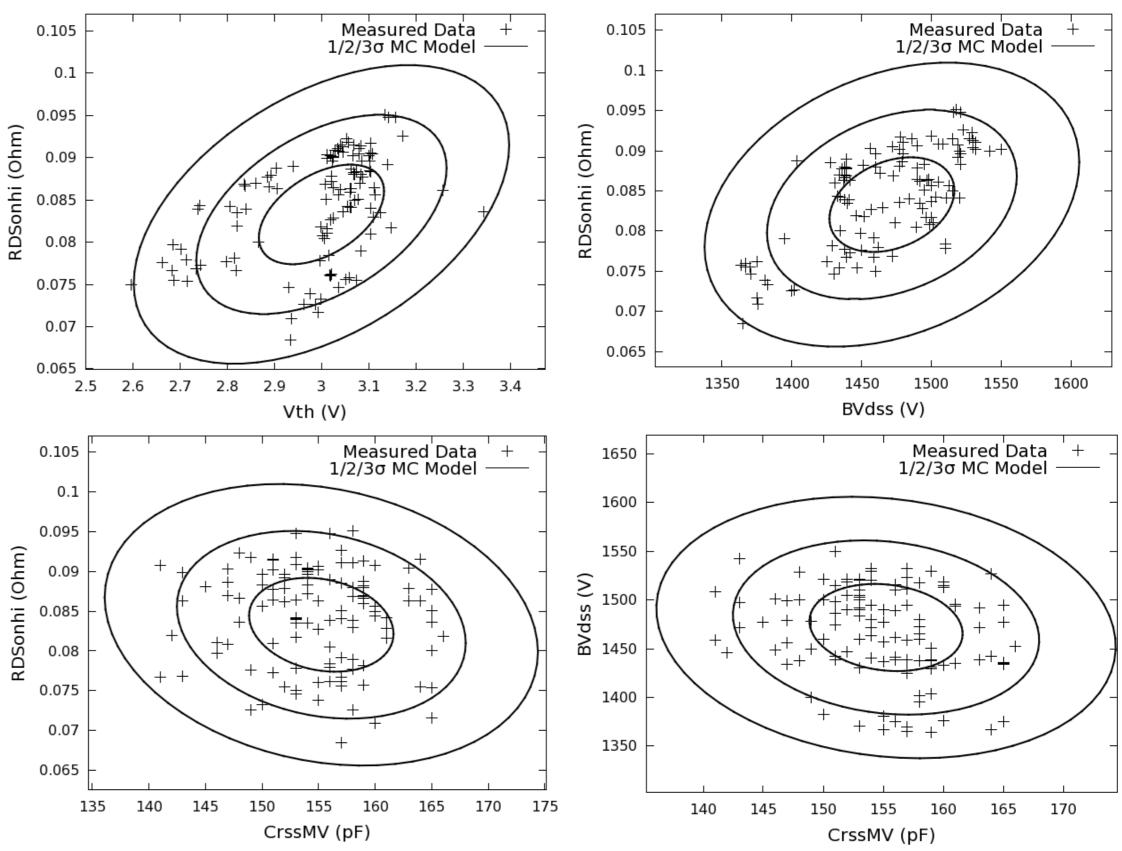




Correlation Between Electrical Performances

- Correlations are evident.
- There are strong or weak correlations between E.
- Physically based model catches these correlations.







- Final Test (FT) represents a statistically stable snapshot of the process variation.
 - FT shows wider E variation than CZ larger statistical sample
- Why not use FT from the beginning? \bullet
 - FT data typically has no AC specs (capacitances, Q_G , etc.)
 - Incomplete BPV solution
- Physical Model: \bullet
 - Correlations between E is built into the physical model and validated through the CZ data. The results are not perfect, but reasonable.
 - The model physics are relied upon to predict the "virtual" FT AC parameter variation.





Sigma Expansion from Characterization to Final Test

Steps:

1. FT data shows larger sigma, calculate ratios as:

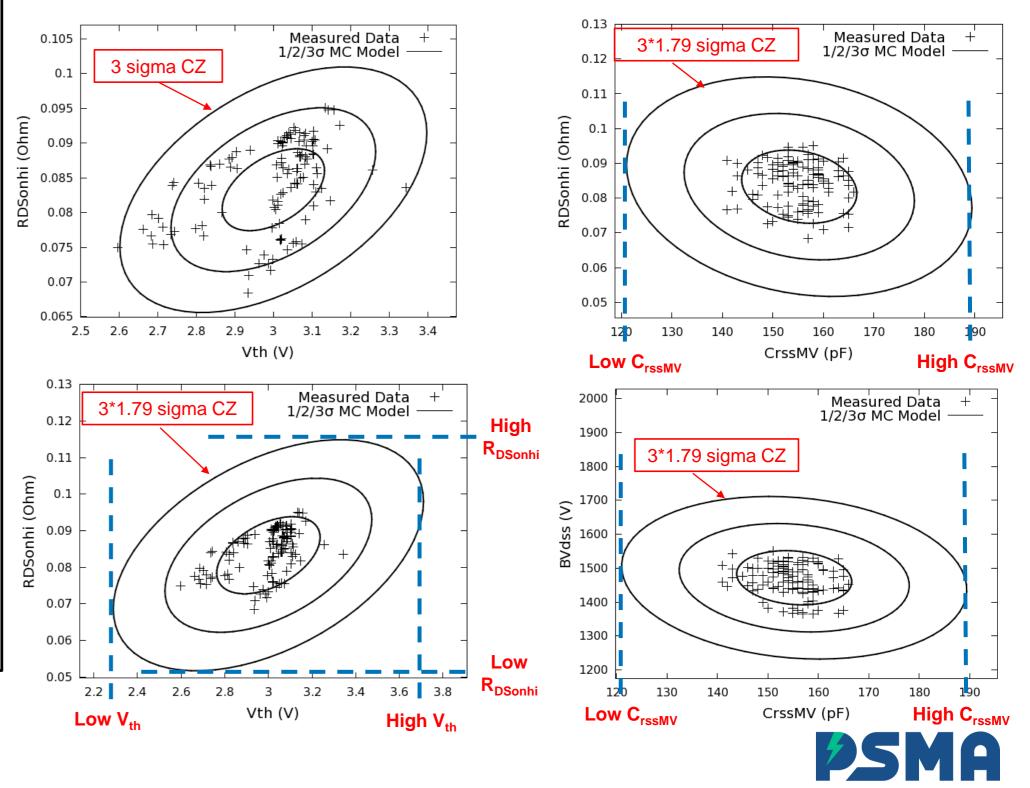
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BV<sub>dss</sub>: 1.78 (=16.49/9.27)
```

V_{th}: 1.79 (=23.85/13.35)

R_{DSonhi}: 1.51 (=32.03/21.21)

- 2. Largest ratio of 1.79 is used to expand the E variation to match FT. So, 3 sigma of FT is equal to 5.37 (=1.79*3) sigma of CZ.
- 3. Low and high E values are extracted from the simulated correlation plots to establish virtual E spec limits for AC parameters and some missing DC parameters in FT needed for BPV.
 - Plots on the right show consistent C_{rssMV} spec generation from R_{DSonhi} and BV_{dss} correlation.
- 4. A new set of BPV models aligned to the complete E from FT are generated.

Daramatar	Characteri	zation Lab	(CZ) : ~120 pts	Final Test (FT) : ~18350 pts			
Parameter	median	stdev	3*std/median	median	stdev	3*std/median	FT/CZ ratio
BVdss	1472	45.49	9.27%	1467	80.67	16.49%	1.78
Vth	3.02	0.135	13.35%	2.88	0.229	23.85%	1.79
RDSonhi	0.0856	0.0061	21.21%	0.0779	0.0083	32.03%	1.51



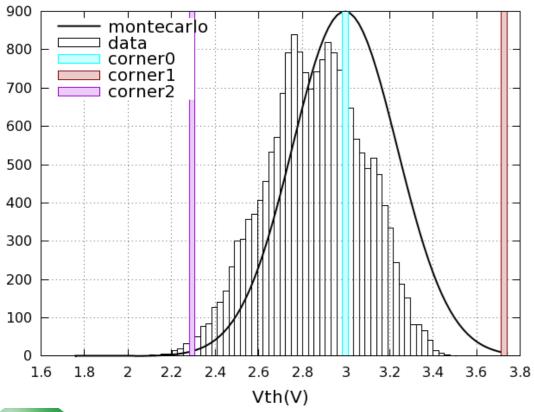


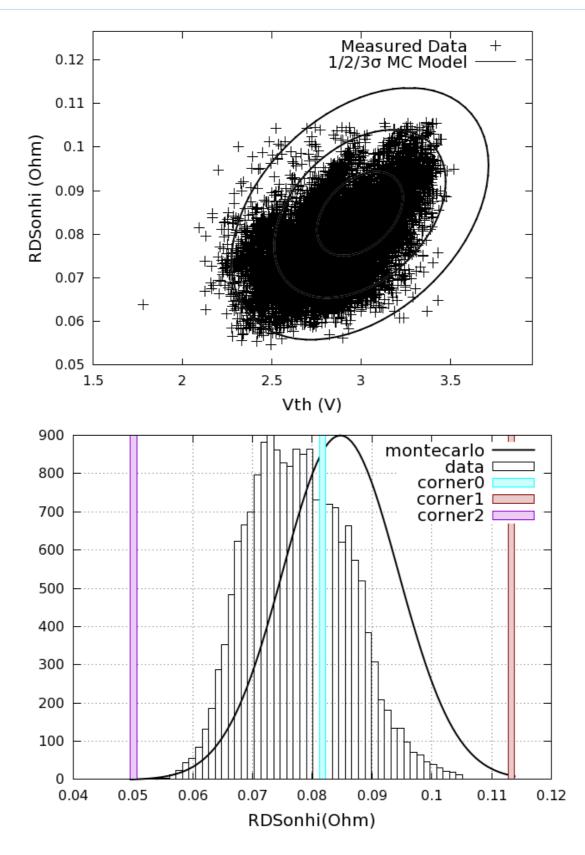
Corner / MC Correlation Plots with Final Test data

E variation widened for FT

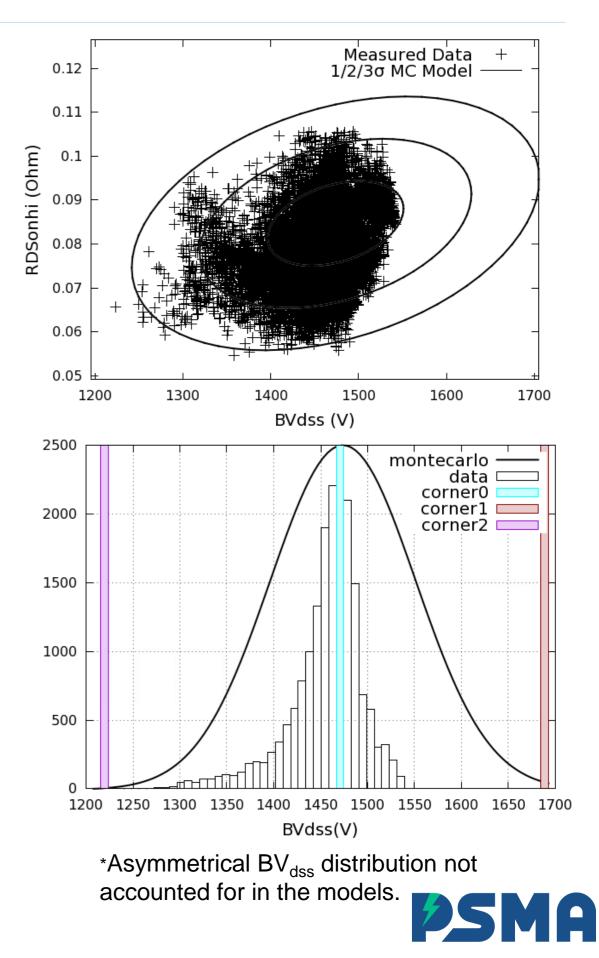
- Model is centered to CZ median
- Mean of CZ and FT don't match perfectly

E (FT)	corner2	corner0	corner1
Vth	0.758	1	1.242
RDSonhi	0.617	1	1.383
RDSonlo	0.561	1	1.439
BVdss	0.837	1	1.163
CissHV	1.136	1	0.864
CrssLV	1.122	1	0.878
CrssMV	1.221	1	0.779
Crss20	1.217	1	0.783
CrssHV	1.081	1	0.919
CossHV	1.143	1	0.857
Qg	1.160	1	0.840









Conclusion

- Modern day power electronic design requires accurate and aggressive electrical specifications to eliminate over design.
- Very important in SiC MOSFET due to material supply and costs
- BPV based SPICE models accurately represent the real process variations \bullet throughout a technology manufacturing lifetime.
- Techniques presented allow for datasheet AC parameter limit setting in the absence of production level AC data.
- The proposed models enable circuit designers to produce optimized, \bullet robust, high yield products through simulation.







