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Design of Planar Transformer and Inductor for 7 kilo-Watt Application

## Standard Questions for any Application

1. Power Topology
2. Frequency
3. Input Voltage Range – minimum to maximum
4. Output Voltage
5. Output Power
6. Dielectric and Creepage requirements and Standards.
7. Mechanical Constraints – e.g. usually low-profile height for planar



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## Power Topologies [Circuits]

1. Forward – 2 types --Active Clamp Forward [ACF] or Diagonal Bridge [2-transistor]
2. Flyback – [3] modes – Continuous [CCM], Discontinuous [DCM], Borderline [BCM]
3. Push-Pull
4. Phase Shifted Full Bridge – Center Tap or Current Doubler
5. Dual Active Bridge [DAB] – popular use in bi-directional converters for EV charging.
6. LLC [CLLC, etc]



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## Standard Questions for any Application

1. Power Topology: Full Bridge to Current Doubler
2. Frequency: 75-200 KHz
3. Input Voltage Range [minimum to maximum]: 165-320
4. Output Voltage: 28
5. Output Power: 7KW
6. Mechanical Constraints – Low Profile Planar. Thermal conduction



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The customer had a TI Reference Design in mind: TIDA-020031  
Automotive 400-V battery to 12-V, 3.6-kW DC/DC converter reference design

Source: <https://www.ti.com/tool/TIDA-020031>





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$$V_{in} := 165 \quad V_{inmax} := 320 \quad V_{out} := 28$$

$$N_p := 5 \quad N_s := 2 \quad freq := 75 \cdot 10^3 \quad freq = 75 \text{ KHz}$$

$$Reg := 1.03 \quad A_c := 5.66 \quad I_m := 9.3$$

$$Vol := I_m \cdot A_c \quad Vol = 52.638$$

$$D_{max} := \frac{V_{out}}{V_{in}} \cdot \frac{N_p}{N_s} \cdot 1 \cdot Reg \quad D_{max} = 0.437 \quad D_{max} \cdot 2 = 87.394 \%$$

$$T_p := \frac{1}{freq} \quad T_p = 13.333 \text{ uSec}$$

$$t_{on} := D_{max} \cdot T_p \quad t_{on} = 5.826 \text{ uSec}$$



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$$B_{pkpk} := \frac{V_{in} \cdot t_{on} \cdot 10^8}{N_p \cdot A_c} \quad B_{pkpk} = 3.397 \times 10^3$$

$$B_{rms} := \sqrt{\frac{2}{T_p} \int_0^{t_{on}} \left( \frac{V_{in} \cdot t_{on} \cdot 10^8}{2 \cdot N_p \cdot A_c} \right)^2 dT_p} \quad B_{rms} = 1.588 \times 10^3$$

$$B := B_{rms} \cdot 10^{-4} \quad B = 0.159 \quad \text{RMS Flux in Tesla}$$

$$\text{Temp} := 65 \quad C_m := 5.12 \quad x := 1.34 \quad y := 2.66$$

$$C_{t2} := 5.48 \cdot 10^{-4} \quad C_{t1} := 1.10 \cdot 10^{-1} \quad C_{t0} := 6.56$$

$$P := C_m \cdot \text{freq}^x \cdot B^y \cdot \left( \frac{C_{t0} - C_{t1} \cdot \text{Temp} + C_{t2} \cdot \text{Temp}^2}{1000} \right) \quad P = 225.341$$

$$\text{Core\_loss} := P \cdot \text{Vol} \cdot 10^{-3} \quad \text{Core\_loss} = 11.861$$



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$$\text{Power} := 7000$$

$$\text{Power} = 7 \times 10^3$$

$$I_{in} := \frac{\text{Power}}{V_{in}} \quad I_{in} = 42.424$$

$$I_o := \frac{\text{Power}}{V_{out}} \quad I_o = 250$$

$$I_{circ} := \left( \frac{T_p - 2 \cdot t_{on}}{T_p} \right) \cdot \frac{I_o}{2}$$

$$I_{circ} = 15.758$$

$$I_{sec} := \left( \frac{I_o}{2} \cdot \sqrt{D_{max} \cdot 2} \right)$$

$$I_{secy} := I_{sec} + I_{circ}$$

$$I_{secy} = 132.613$$

$$\frac{I_o}{2} = 125$$

$$I_{pri\_rms} := \left( \frac{I_o}{2} \cdot \sqrt{D_{max} \cdot 2} \right) \cdot \frac{N_s}{N_p}$$

$$I_{pri\_rms} = 46.742$$



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$$\Delta_{\text{ripple}} := 0.33 \cdot I_o \quad \Delta_{\text{ripple}} = 82.5 \quad \sim 33\% \text{ ripple current}$$

$$I_{\text{secy\_rms}} := I_{\text{sec}} + I_{\text{circ}} + \frac{\Delta_{\text{ripple}}}{3} \quad I_{\text{secy\_rms}} = 160.113$$

$$I_{\text{secy\_pk}} := I_{\text{sec}} + I_{\text{circ}} + \frac{\Delta_{\text{ripple}}}{2} \quad I_{\text{secy\_pk}} = 173.863$$

$$I_{\text{pri\_pk}} := \frac{I_{\text{pri\_rms}}}{\sqrt{D_{\text{max}} \cdot 2}} + \frac{N_s}{N_p} \cdot I_{\text{circ}} + \frac{N_s}{N_p} \cdot \frac{\Delta_{\text{ripple}}}{2} \quad I_{\text{pri\_pk}} = 72.803$$

$$I_{\text{pri\_rms}} := \left( \frac{I_o}{2} \cdot \sqrt{D_{\text{max}} \cdot 2} \right) \cdot \frac{N_s}{N_p} + \frac{N_s}{N_p} \cdot I_{\text{circ}} + \frac{N_s}{N_p} \cdot \frac{\Delta_{\text{ripple}}}{3} \quad I_{\text{pri\_rms}} = 64.045$$





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$$\text{Sec\_DCR} := .0003 \quad \text{Sec\_loss} := \left[ (I_{\text{secy\_rms}})^2 \cdot \text{Sec\_DCR} \right] \quad \text{Sec\_loss} = 7.691$$

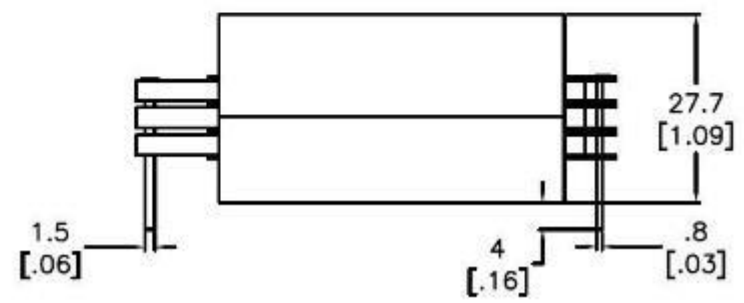
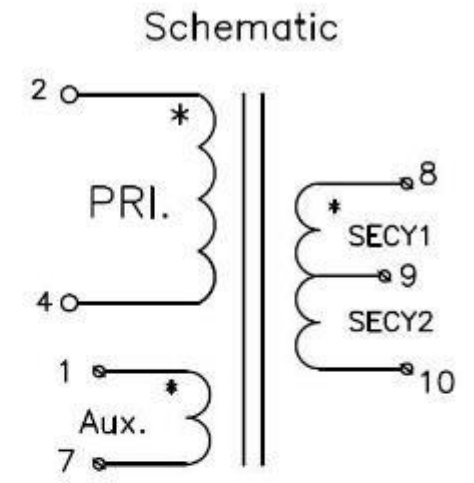
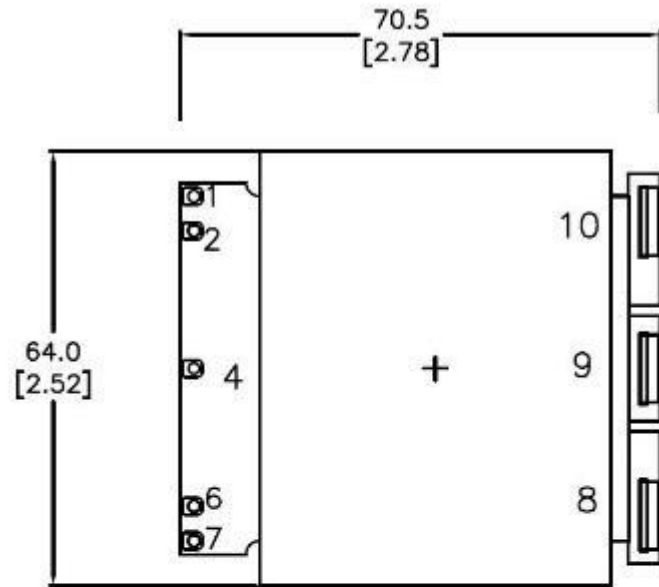
$$\text{Pri\_DCR} := .0025 \quad \text{Pri\_loss} := \left( (I_{\text{pri\_rms}}) \right)^2 \cdot \text{Pri\_DCR} \quad \text{Pri\_loss} = 10.255$$

$$\text{Total\_Loss} := \text{Sec\_loss} + \text{Pri\_loss} + \text{Core\_loss} \quad \text{Total\_Loss} = 29.807$$

$$\text{Cu\_Loss} := \text{Sec\_loss} + \text{Pri\_loss} \quad \text{Cu\_Loss} = 17.945 \quad \text{Core\_loss} = 11.861$$



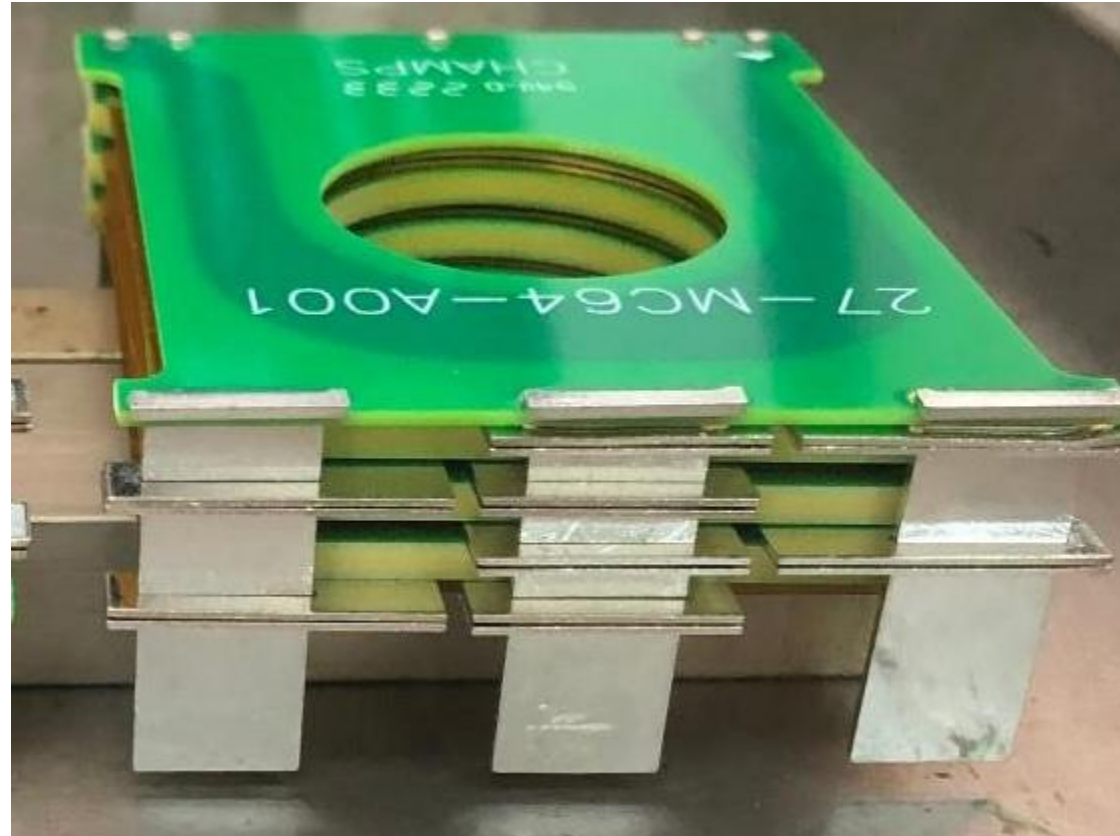
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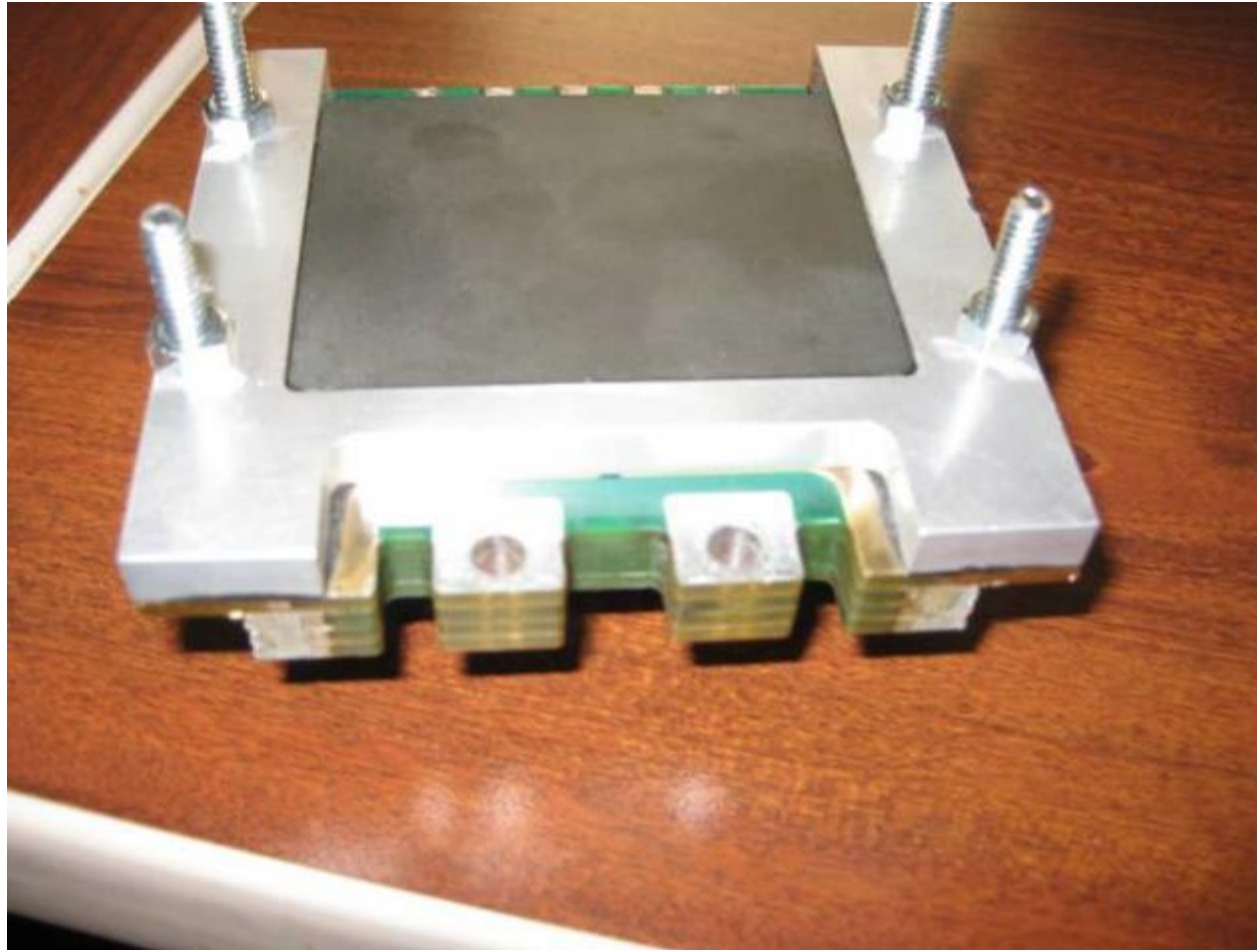
Transf. Stack: View Sec'y Terminals





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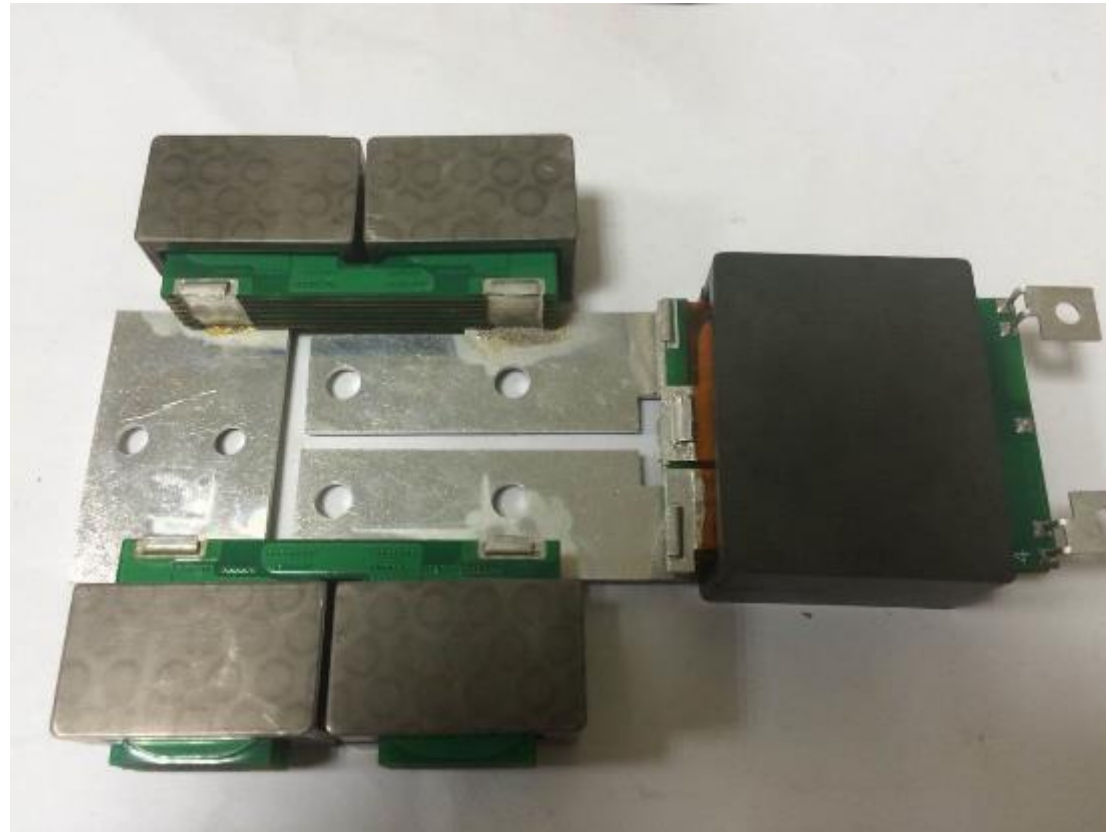
## Aggressive Thermal Solution





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## Distributed Thermal Solution





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## Output Inductor Calculations

$$D_{\min} := \frac{V_{\text{out}}}{V_{\text{inmax}}} \cdot \frac{N_p}{N_s} \cdot 1 \cdot \text{Reg} \quad D_{\min} = 0.225 \quad t_{\text{onmin}} := \frac{D_{\min}}{1} \cdot T_p \quad t_{\text{onmin}} = 3.004 \times 10^{-6}$$

$$D_{\min} \cdot 2 = 45.063\% \quad t_{\text{offmax}} := T_p - t_{\text{onmin}} \quad t_{\text{offmax}} = 1.033 \times 10^{-5}$$

$$V_{\text{pk}} := \left( V_{\text{inmax}} \cdot \frac{N_s}{N_p} \right) \quad V_{\text{pk}} = 128 \quad V_{\text{inductor}} := \frac{V_{\text{pk}}}{1} - V_{\text{out}} \quad V_{\text{inductor}} = 100$$

$$I_{\min} := I_o \cdot 0.33 \quad I_{\min} = 82.5 \quad L_{\text{omin}} := \frac{(V_{\text{inductor}}) \cdot t_{\text{onmin}}}{I_{\min}} \quad L_{\text{omin}} = 3.641 \times 10^{-6}$$



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$$L_o := 3.6 \cdot 10^{-6} \quad \Delta I := \frac{V_{\text{inductor}} \cdot t_{\text{onmin}}}{L_o} \quad \Delta I = 83.449 \quad \frac{\Delta I}{I_o} = 0.334$$

$$L_{\text{calc}} := \frac{[V_{\text{out}} \cdot (1 - D_{\text{min}})]}{\Delta I \cdot \text{freq}} \quad L_{\text{calc}} = 3.466 \times 10^{-6}$$

$$\Delta I_{\text{off}} := \frac{V_{\text{out}} \cdot t_{\text{offmax}}}{L_o} \quad \Delta I_{\text{off}} = 80.338 \quad \frac{\Delta I_{\text{off}}}{I_o} = 0.321$$

$$\text{Inductor\_DCR} := .00045 \quad I_{\text{rms}} := \frac{I_o}{2} + \frac{\Delta I}{3} \quad I_{\text{rms}} = 152.816$$

$$\text{Inductor\_loss} := (I_{\text{rms}})^2 \cdot \text{Inductor\_DCR} \quad \text{Inductor\_loss} = 10.509$$



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$$D_{\min} = 0.225 \quad L_o = 3.6 \times 10^{-6} \quad I_o = 250$$

$$D_t := D_{\min} \quad N_t := \frac{N_p}{N_s} \quad N_t = 2.5$$

$$\Delta I_L := \frac{\frac{V_{inmax}}{N_t} - V_{out}}{L_o} \cdot \frac{D_t}{\text{freq}} \quad \Delta I_L = 83.449 \quad \text{Peak Current for each individual inductor}$$

$$\Delta I_L := \frac{V_{inmax} \cdot D_t - (D_t \cdot N_t \cdot V_{out})}{\text{freq} \cdot N_t \cdot L_o} \quad \Delta I_L = 83.449 \quad \frac{\Delta I_L}{I_o} = 0.334$$

Source: Current Doubler Rectifier Offers Ripple Current Cancellation

TI Application Note SLUA323 Steve Mappus || <https://www.ti.com/lit/an/slua323/slua323.pdf>





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$$D_{\min} = 0.225 \quad L_o = 3.6 \times 10^{-6} \quad I_o = 250$$

$$D_t := D_{\min} \quad N_t := \frac{N_p}{N_s} \quad N_t = 2.5$$

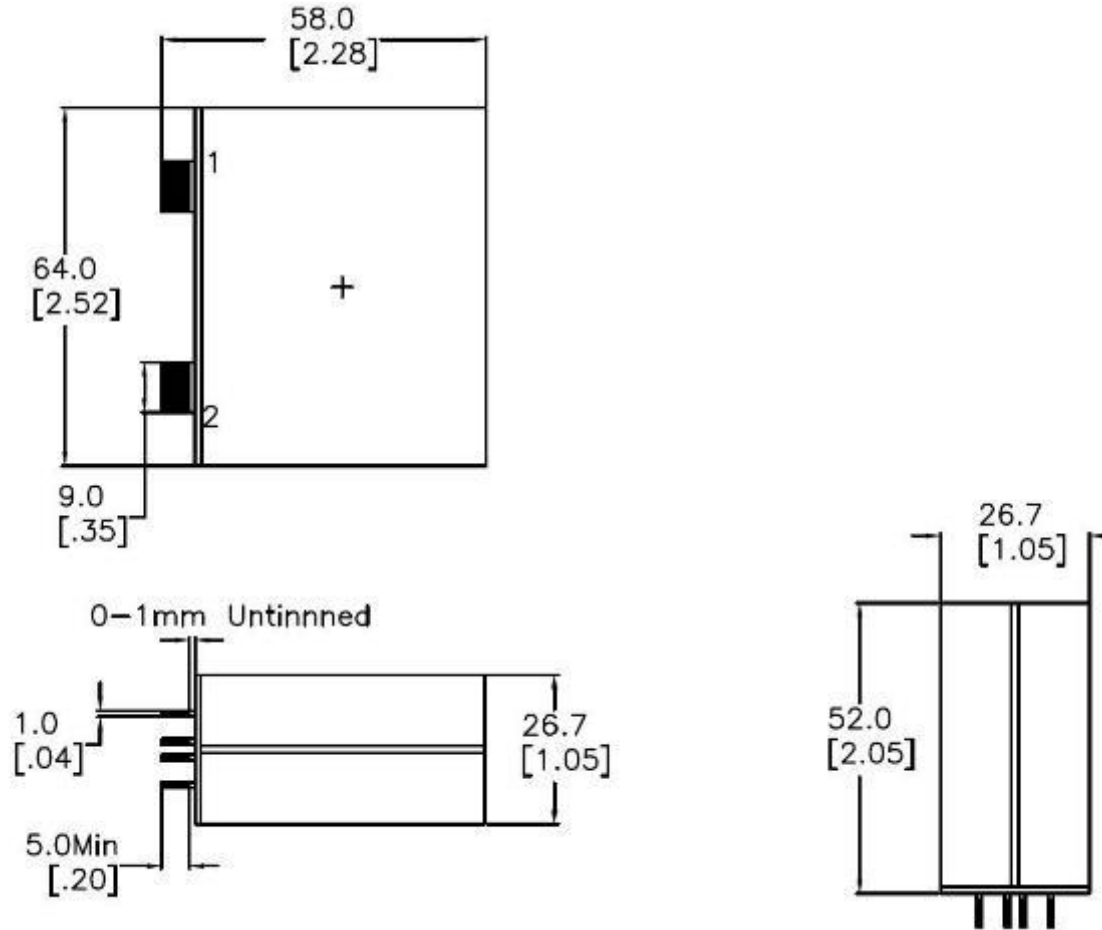
$$\Delta I_{\text{out}} := \frac{V_{\text{inmax}} \cdot D_t - (2 \cdot D_t \cdot N_t \cdot V_{\text{out}})}{\text{freq} \cdot N_t \cdot L_o} \quad \Delta I_{\text{out}} = 60.083 \quad \frac{\Delta I_{\text{out}}}{I_o} = 0.24$$

$$K := \frac{1 - D_t \cdot 2}{D_t \cdot 2 - 1} \quad K = 0.709$$



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## Output Inductor Spec





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## Output Inductors





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## 3D Composite Design

