

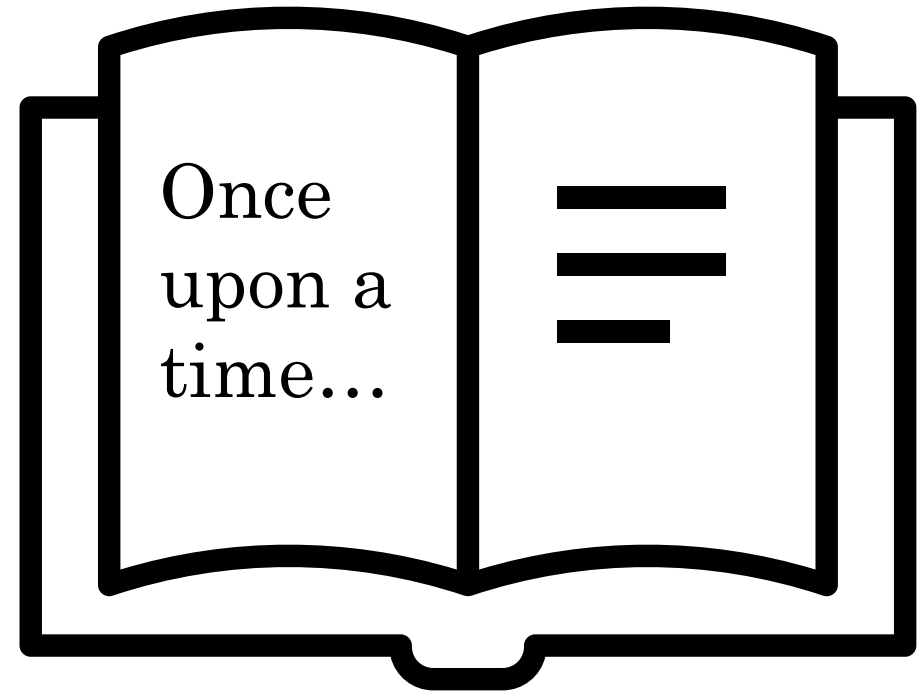
Custom Magnetics

Stories of Conflict, Tradeoff and Creation

Victor W. Quinn

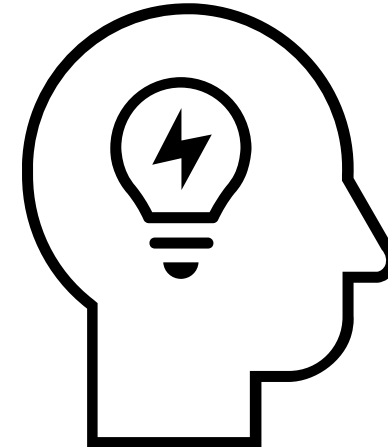
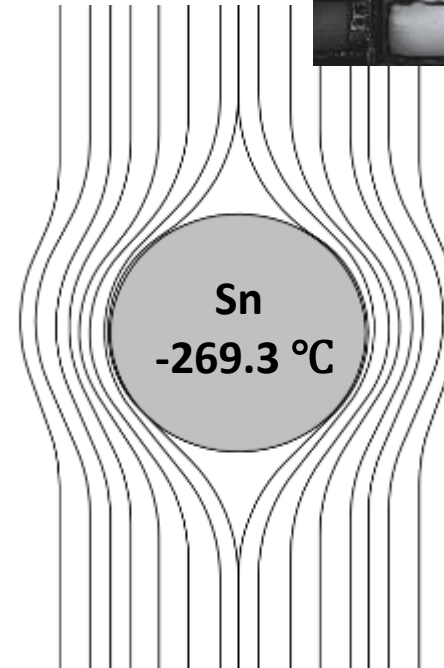
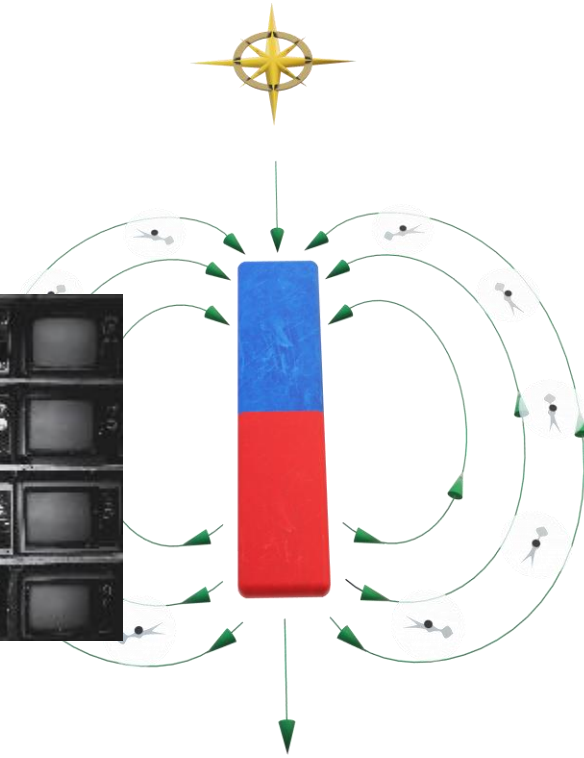
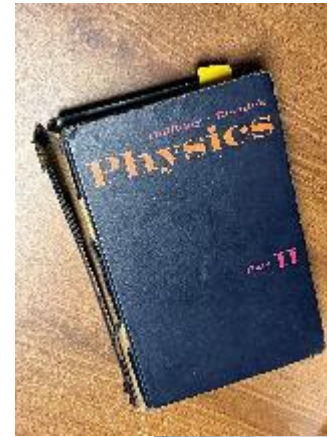
Stories of Conflict, Tradeoff and Creation

- Inherent Conflict
- Moving forward ... Risk Mitigation
- Densities Teeter
- Shell Games
- Reactive Tradeoffs
- Inductor or Capacitor?
- Adventures in Design
- For the love of Custom Magnetics ...

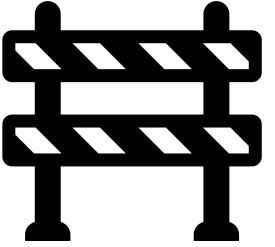


Induced by Magnetics

- NASA heroes & model rockets
- Resnick & Halliday Part II (Chapter 33)
- Meissner Effect Sn (bobbin winding)
- CRT Tubes vs Magnetics

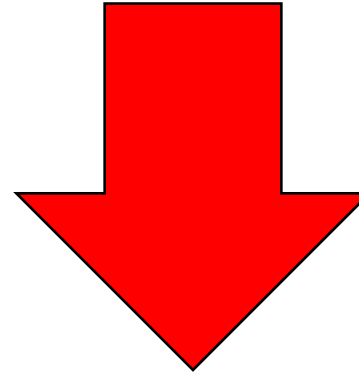


Inherent Conflict



- Technical Challenge

- design method
- component material
- design verification
- production method
- production control

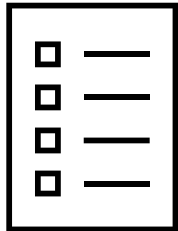


- Resource Constraints

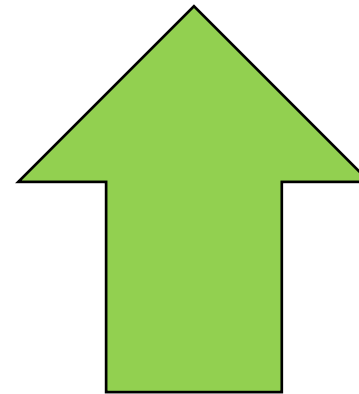
- personnel
- time
- material
- equipment

CONFLICTS

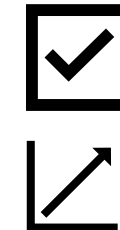
- Customer Need



- performance
- reliability
- cost
- schedule



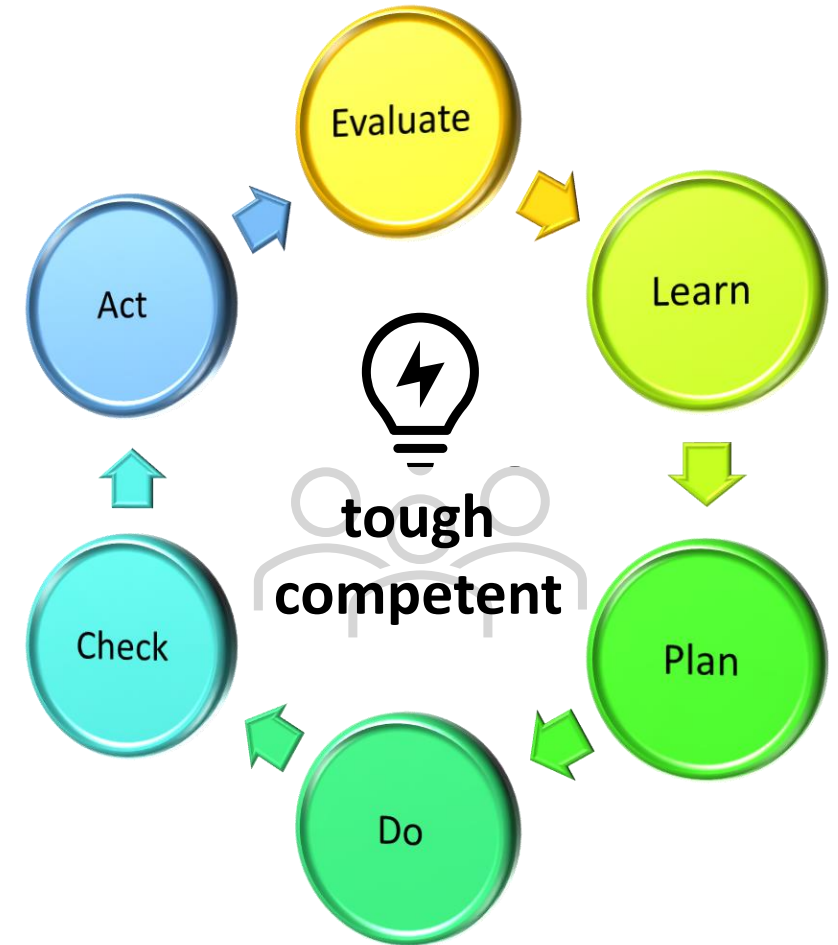
- Business Opportunity



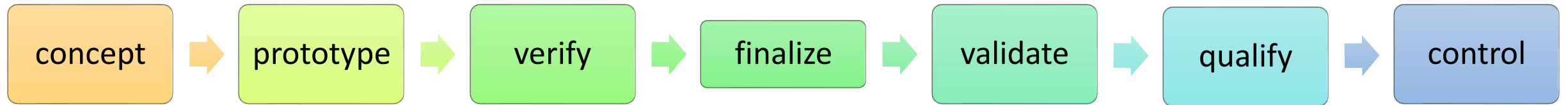
- technical achievement
- revenue growth

Realization ...

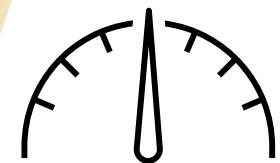
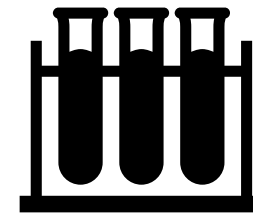
- Technology advancement
 - we don't know what we don't know
- Limited resources
 - we can't do everything we wish to do



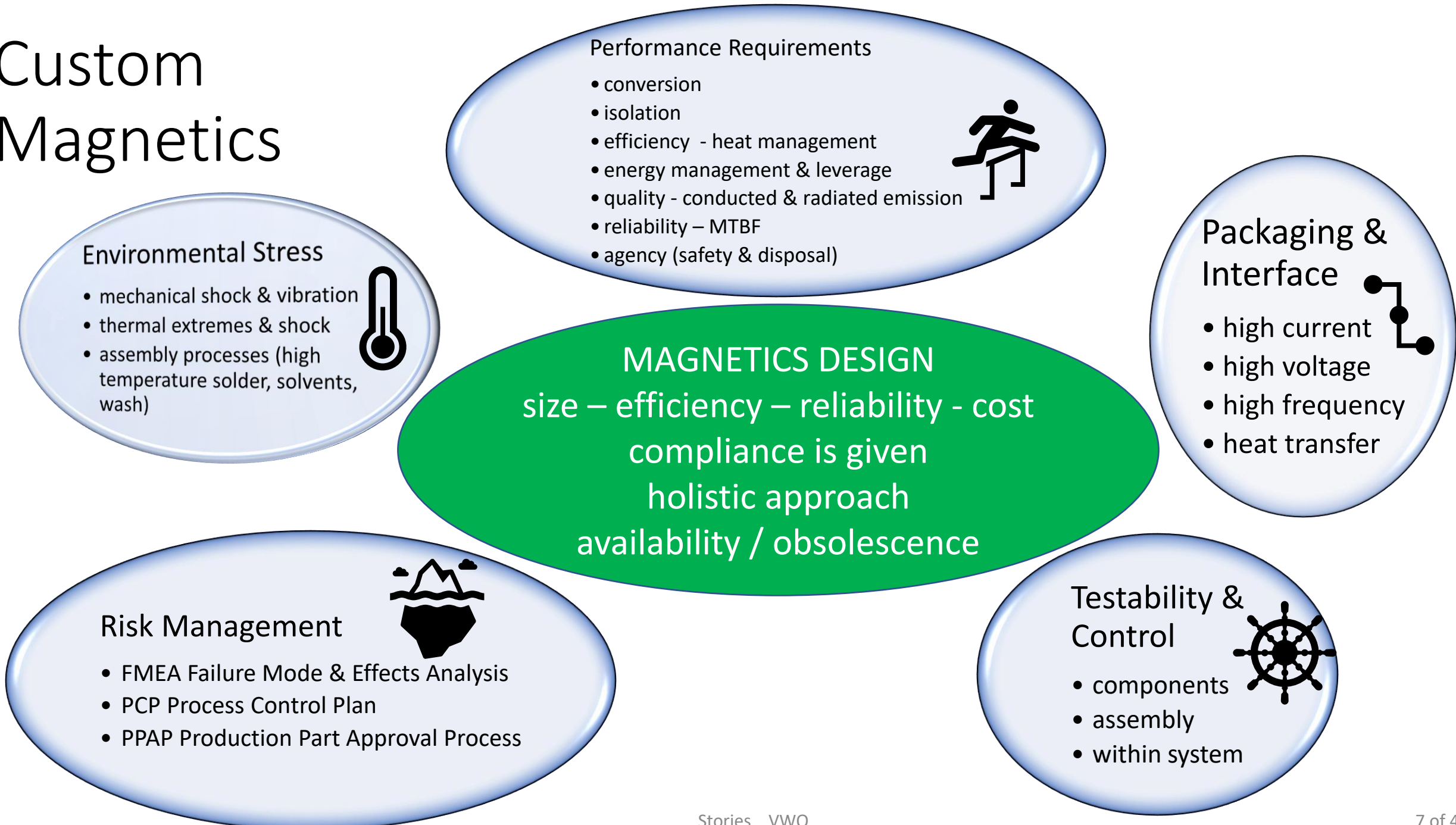
Moving Forward ... Risk Mitigation



- Selectively Research
 - systematic investigation to support innovation
- Design of Experiments
 - evaluate how selected variables affect result
- Test Comprehensively
 - verify convergence of results with design method
- Control Process
 - proactively monitor



Custom Magnetics



Densities Seesaw (*ci-ça*)



Coil Loss $\propto (J^2)$

Core Loss $\propto (\Delta B^\beta)$

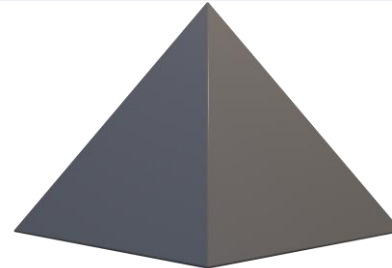
to minimize total loss - neglecting saturation

$$\frac{\text{Core Loss}}{\text{Winding Loss}} = \frac{2}{\beta}$$

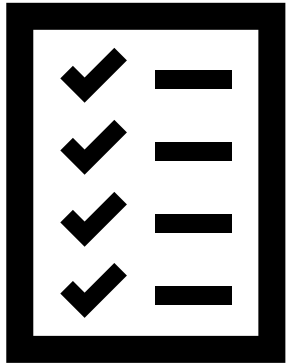
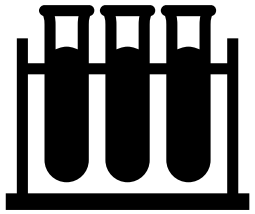
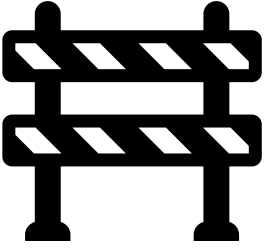
J (current density)

ΔB (flux density)

TRADEOFFS



What do we know about cores?



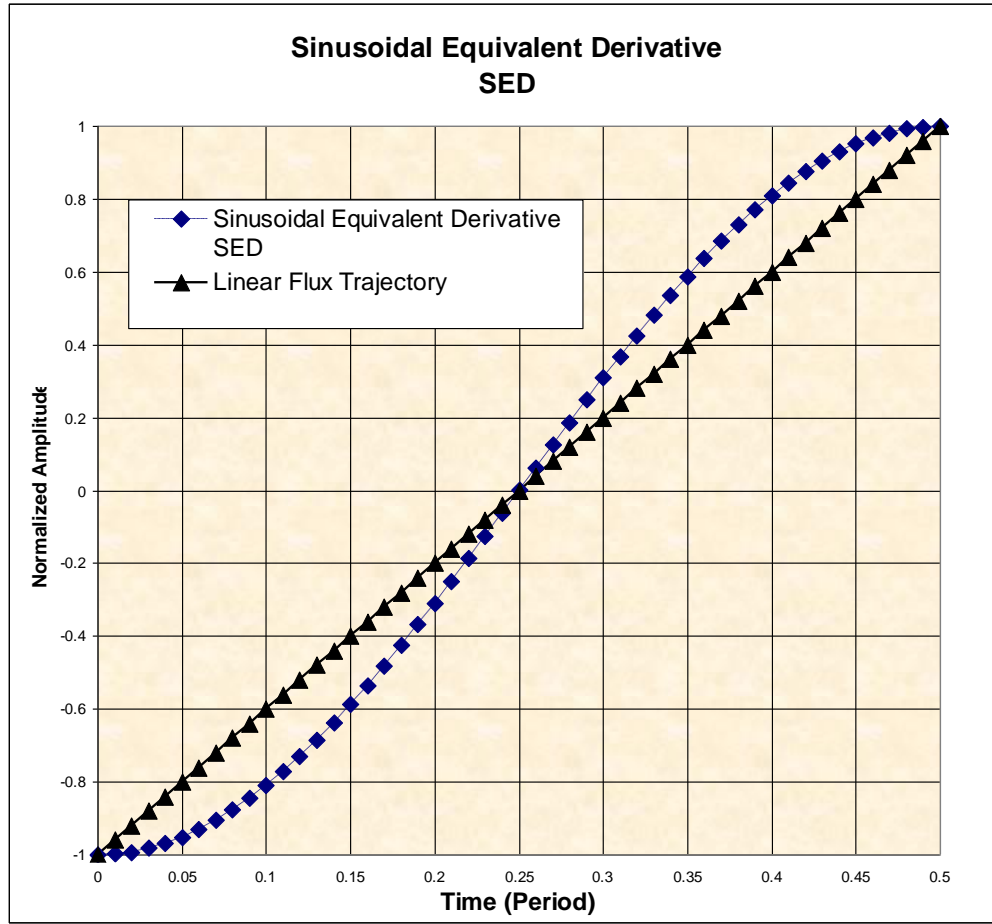
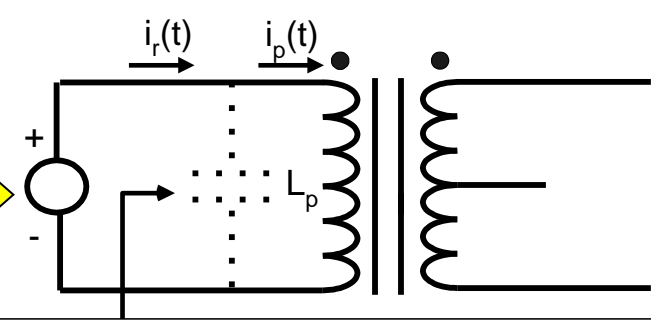
- nonlinear - inconsistent
- increasing frequency
- bias & transients
- interfaces & packaging impacts
- wide temperature range
- reliability

So we test ... and test repeatedly ...

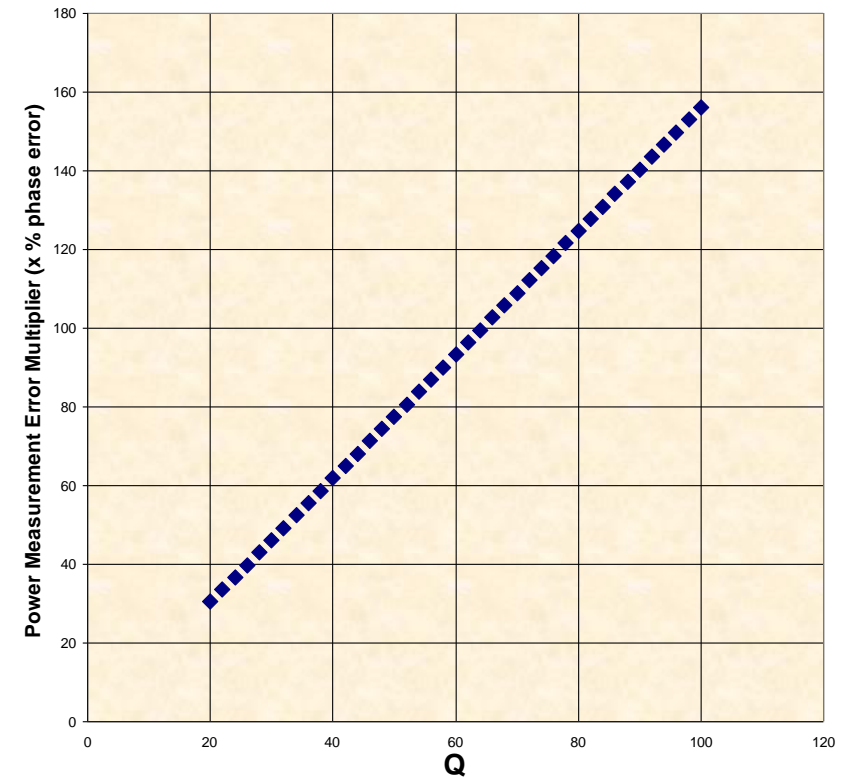
- Loss density, incremental permeability, hysteresis loop versus AC field density
 - over frequency, temperature
- Complex permeability versus DC bias field density
 - over frequency, temperature
- Other normalized methods to evaluate composite materials in flux path

High AC Swing

Parallel resonant capacitor facilitates accurate loss measurement

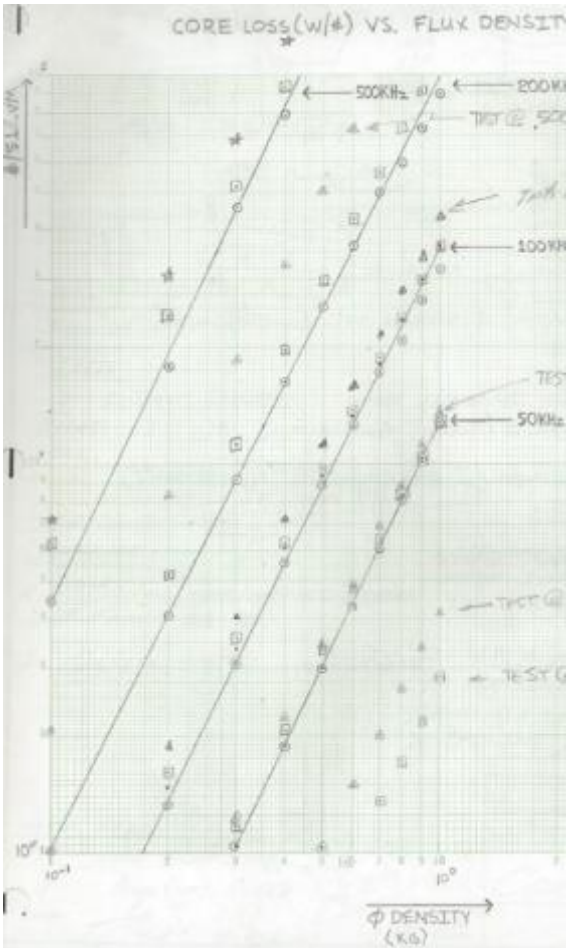
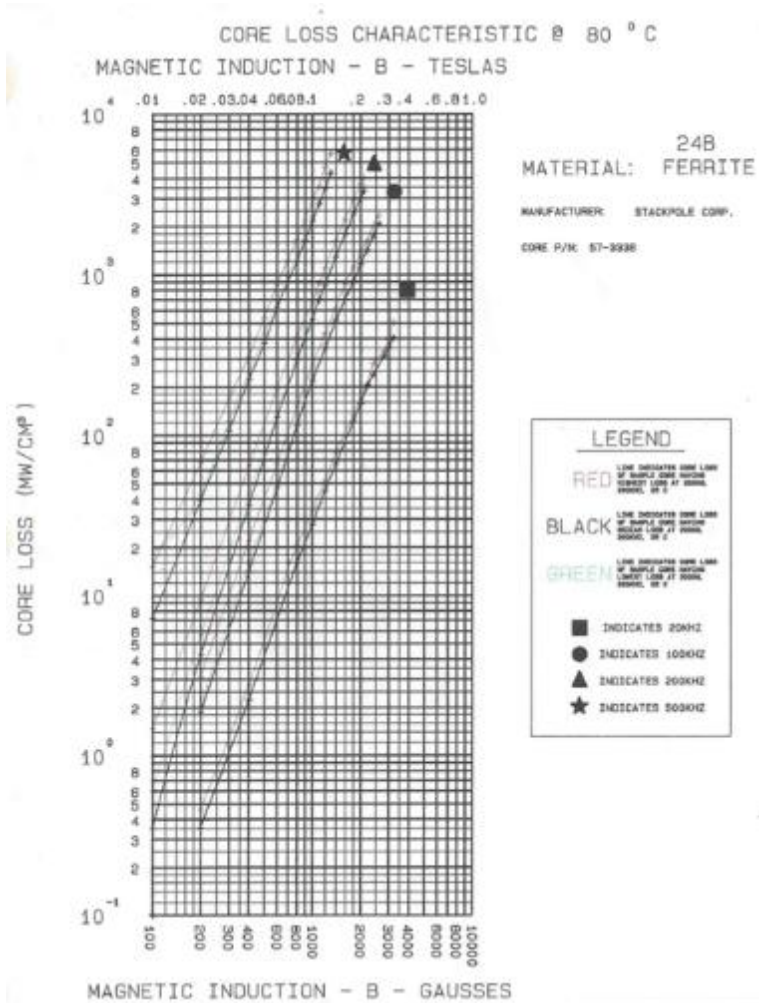
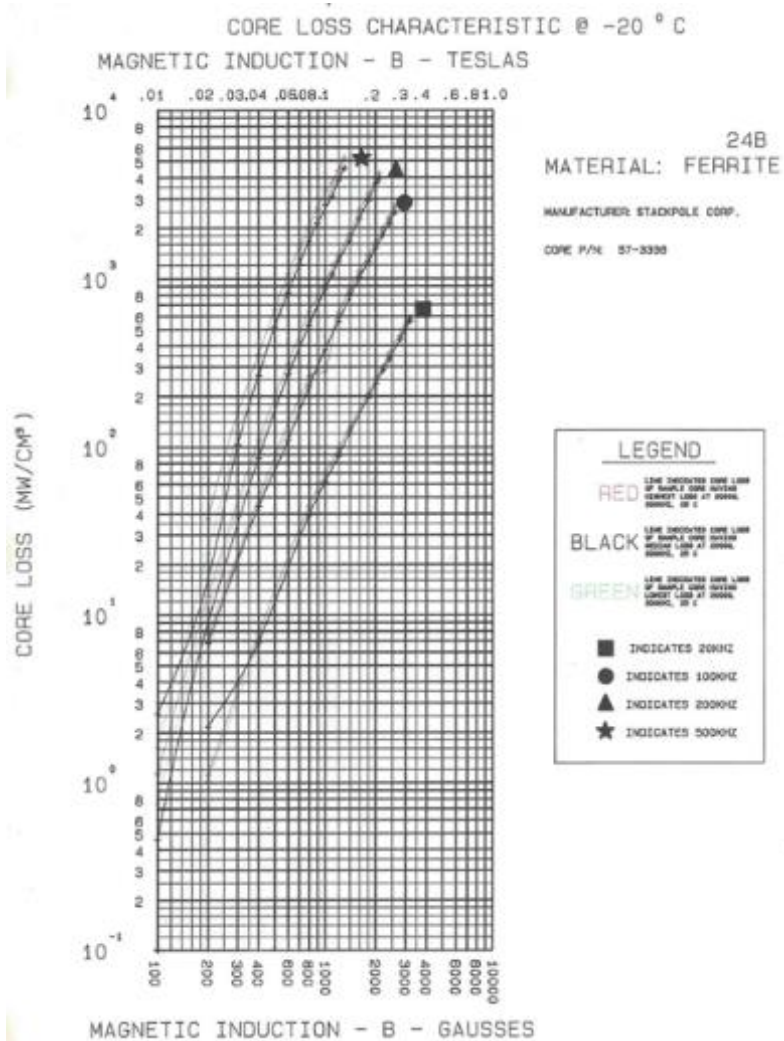
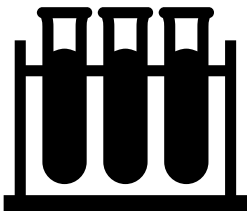


Measured Loss Error from Uncompensated Phase Shift vs Inductor Q Sine Wave



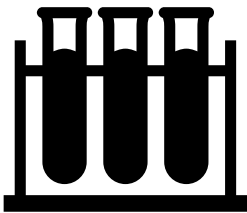
Resonant circuit facilitates measurement.

Core Test: Loss DOE



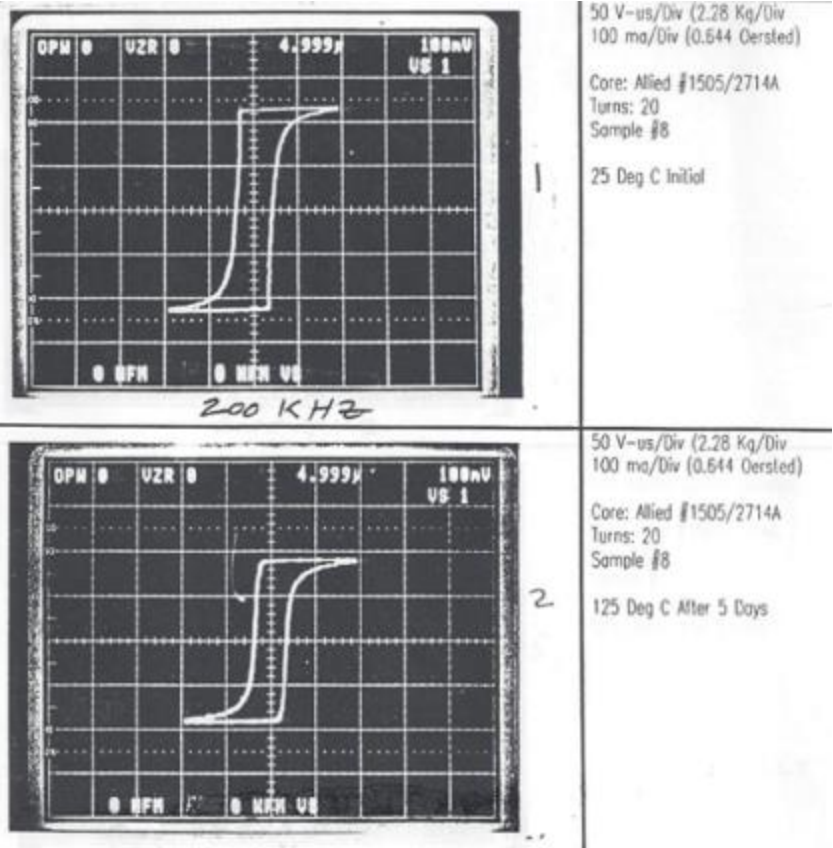
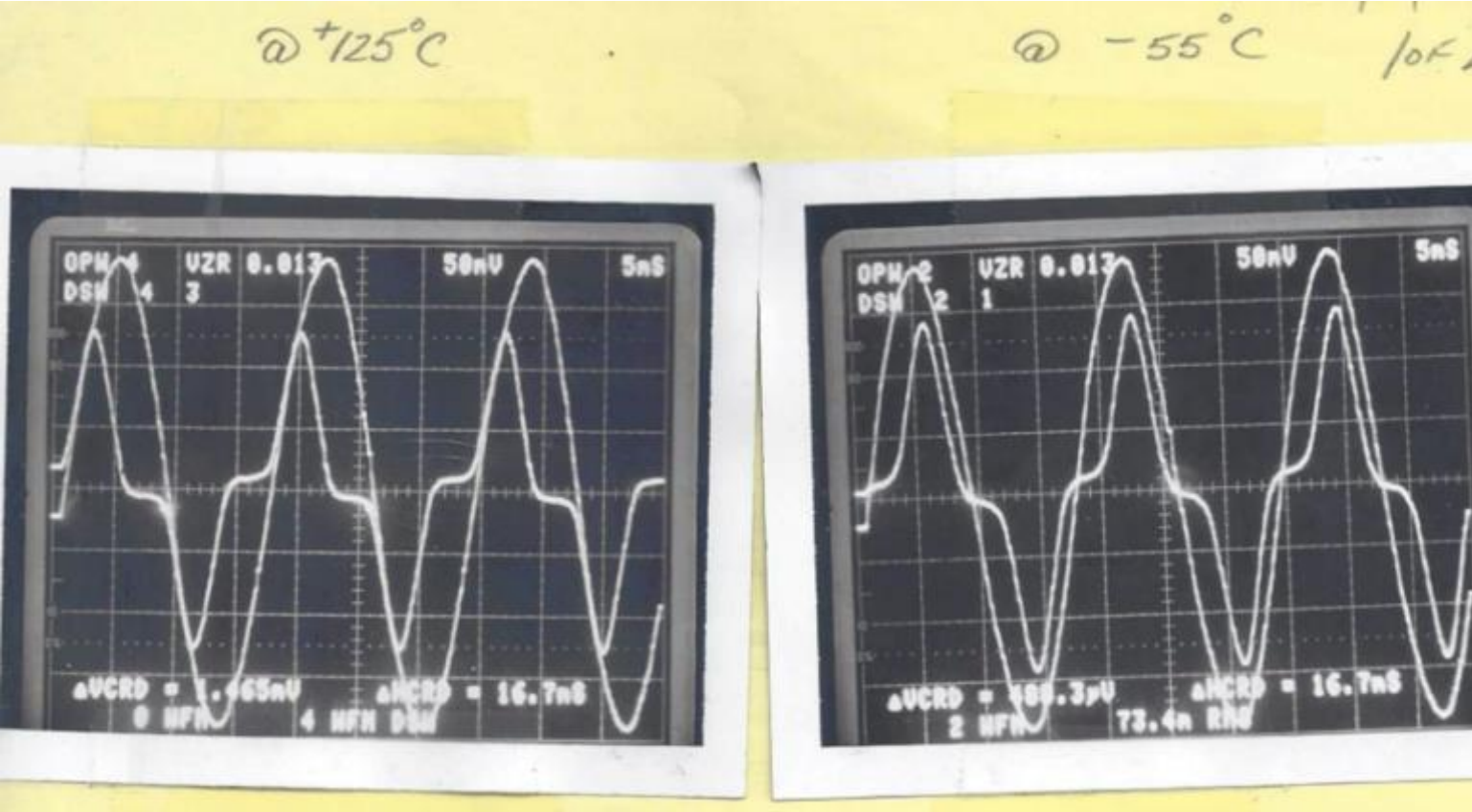
Collect and expand data with each new product development.

Core Test: Hysteresis DOE



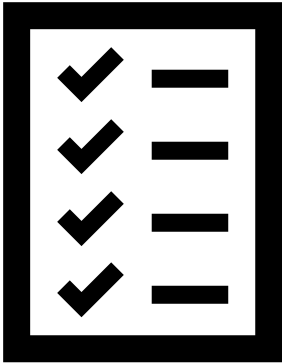
Co/Fe/V ribbon

Co based amorphous ribbon

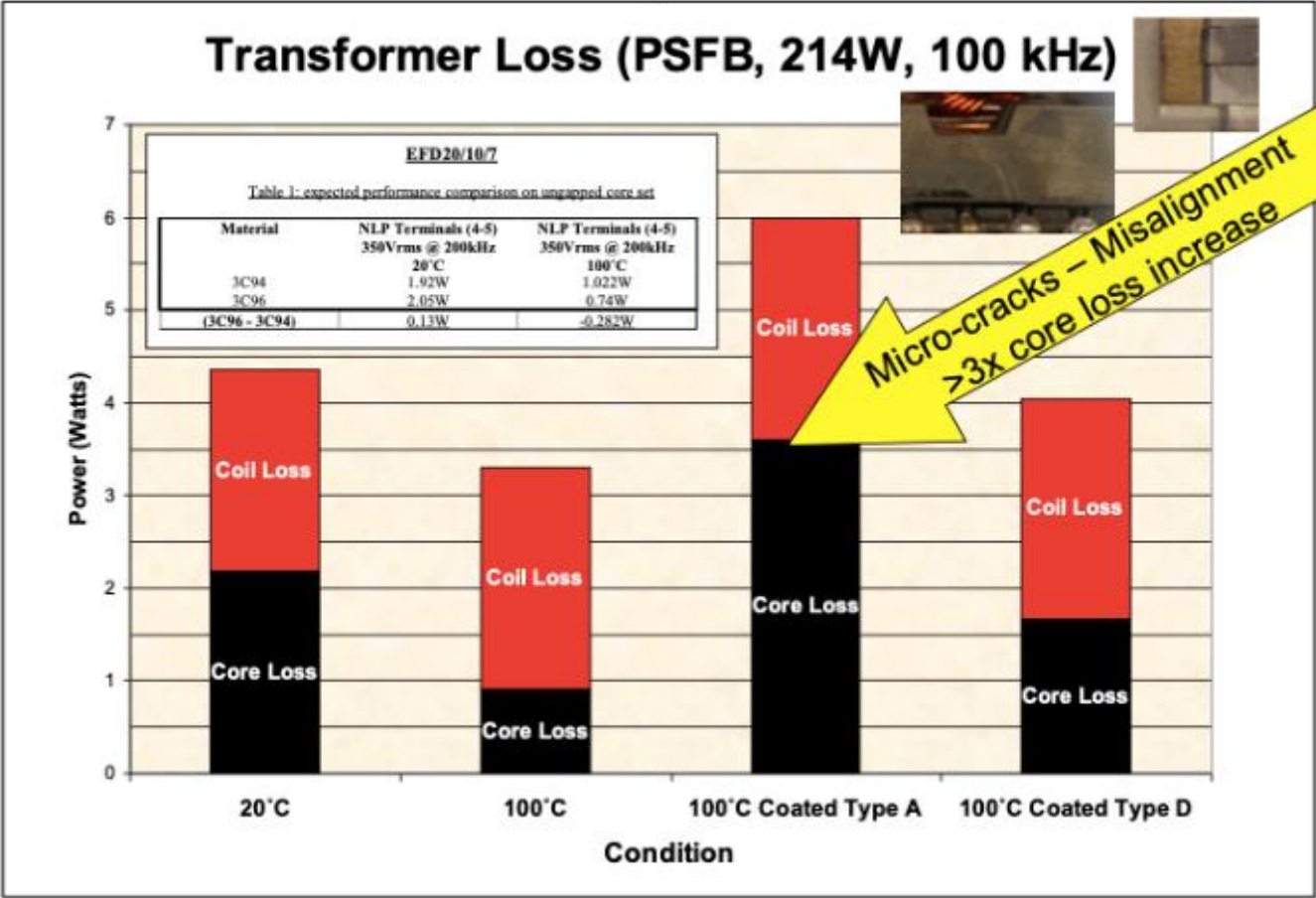


Characterize non linearities and verify endurance.

Core Test: Loss Validation

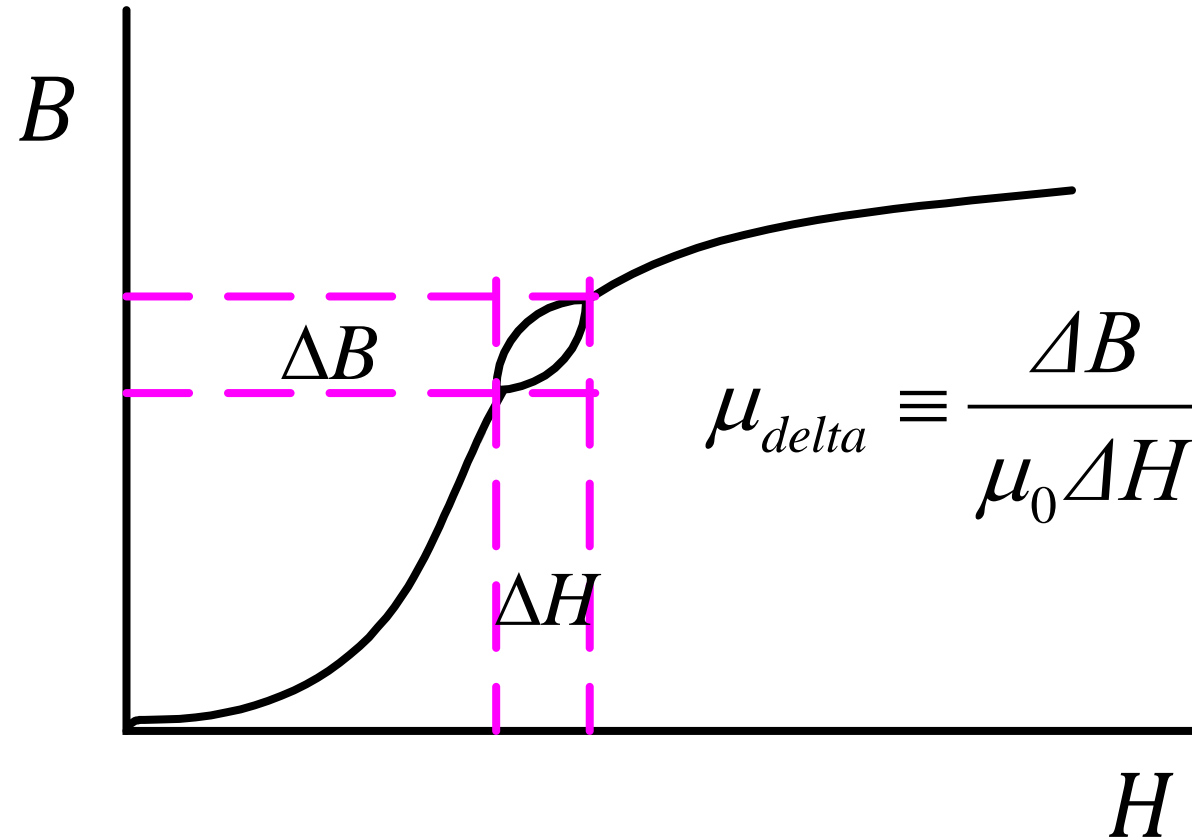


Core Loss Experiences



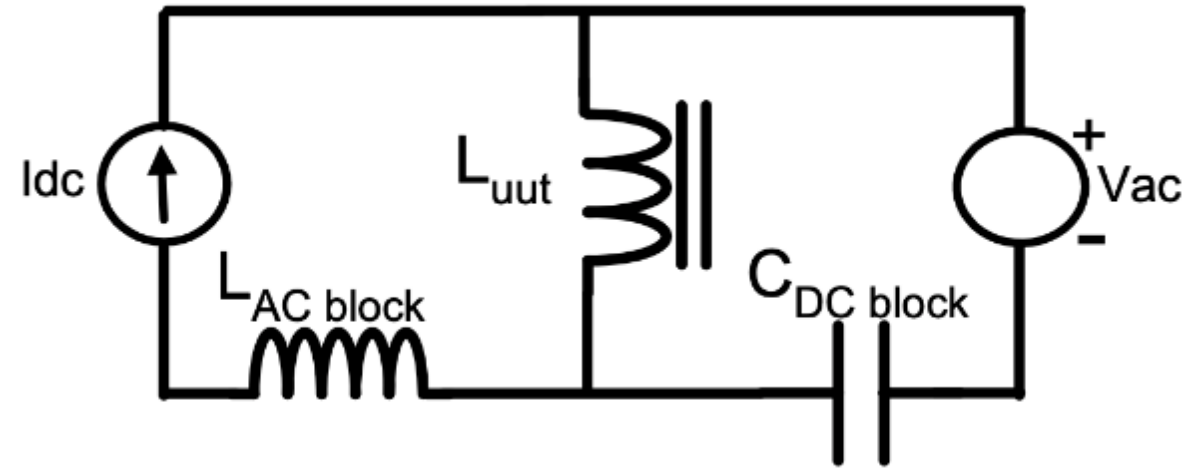
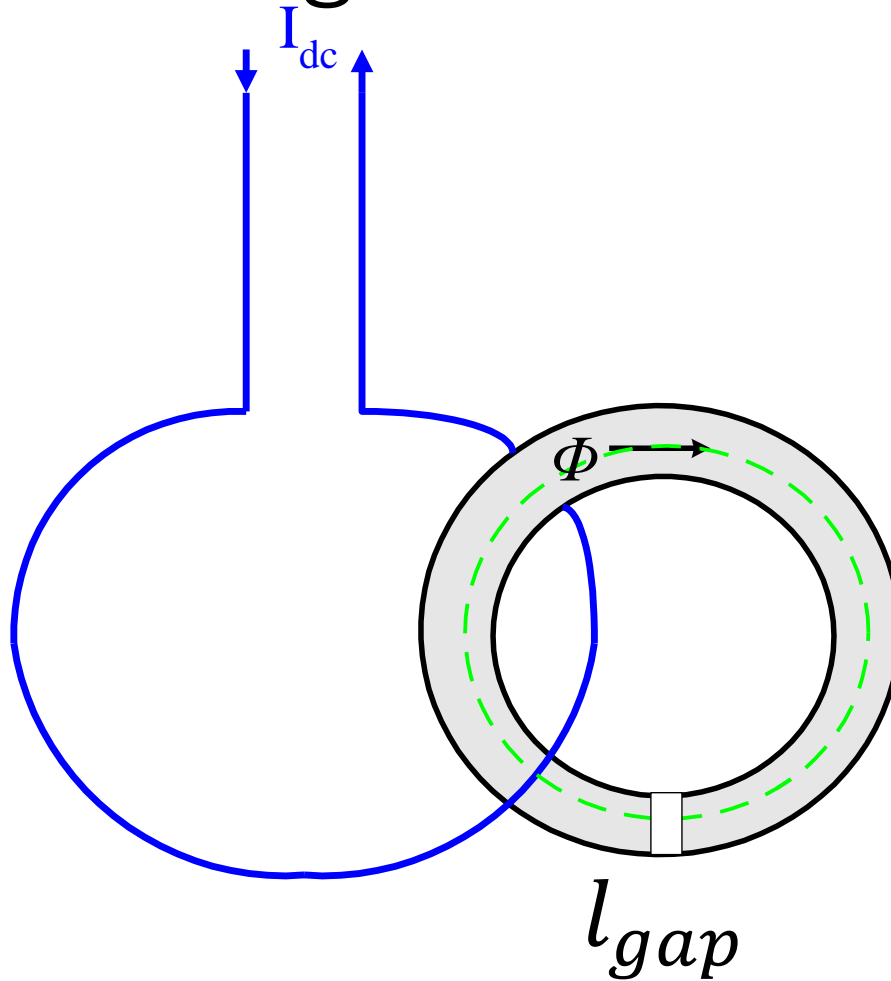
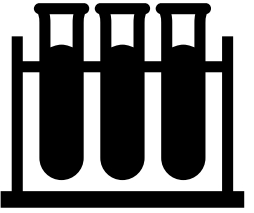
Validate results after manufacturing processes.

Incremental AC Permeability with Bias



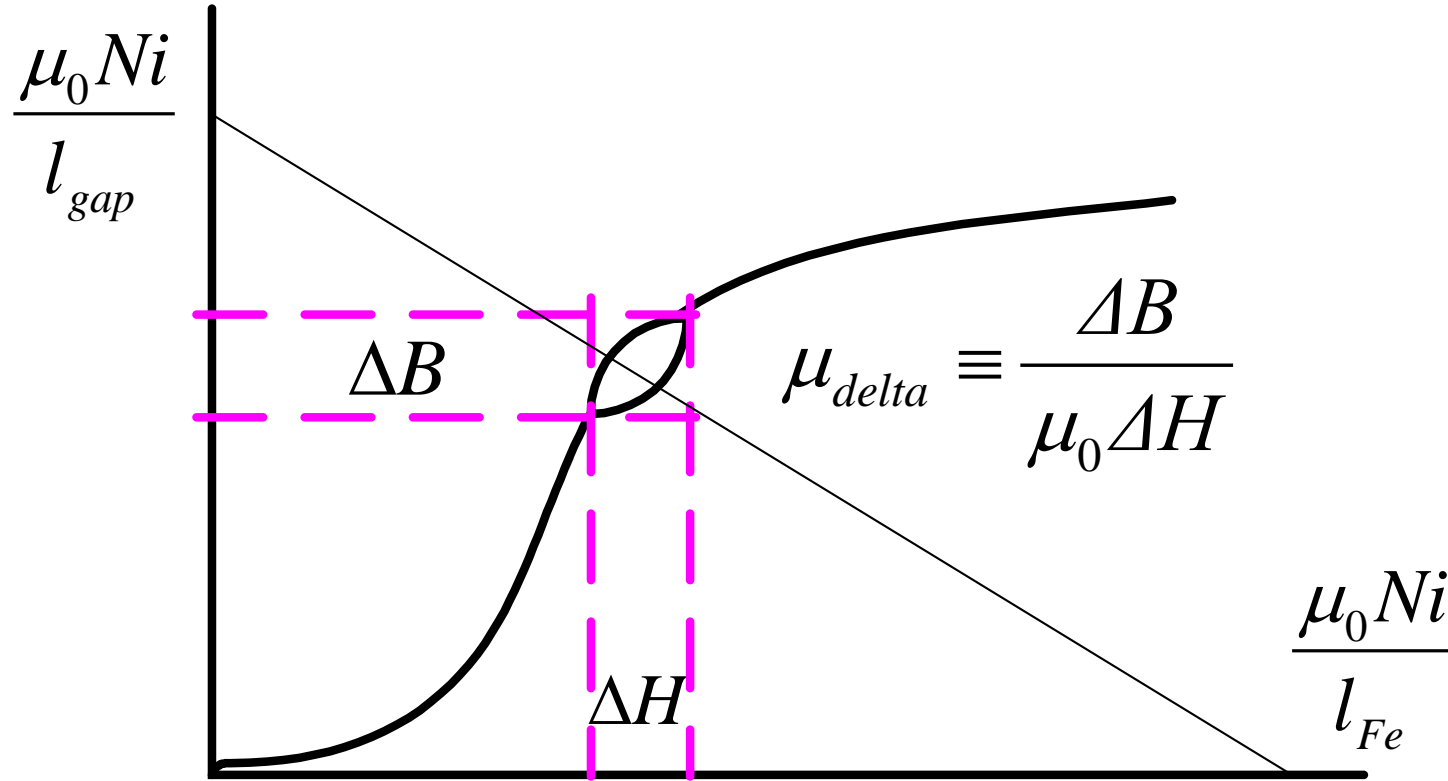
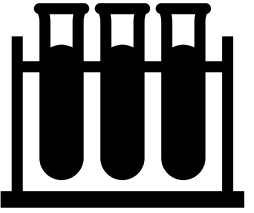
Permeability depends on nonlinear AC and DC magnetization.

Core Test: High DC Bias DOE



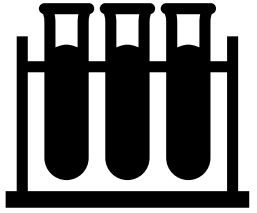
Test circuit facilitates AC measurement with superimposed bias.

Core Test: DC Quiescent Point



Develop DOE conditions based on normalized field densities.

Core Test: Biased Permeability DOE

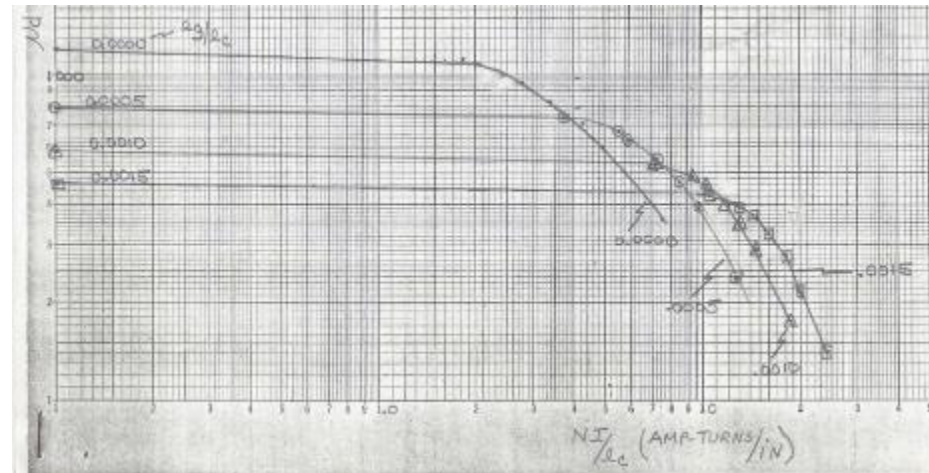


$$L \propto \frac{N^2 A_{Fe}}{l_{Fe}} \left[\frac{\mu_{delta}}{\frac{l_{gap}}{l_{Fe}} \mu_{delta} + 1} \right]$$

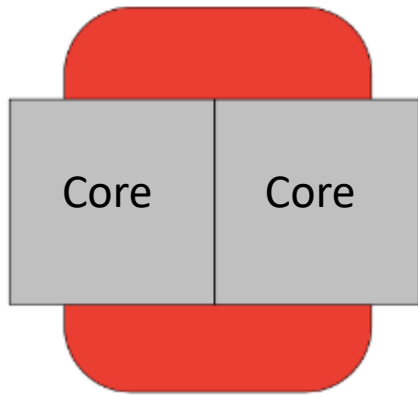
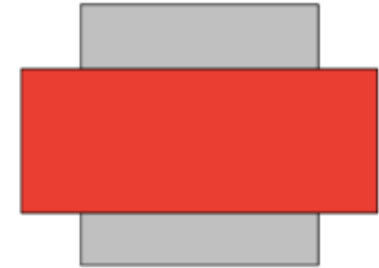
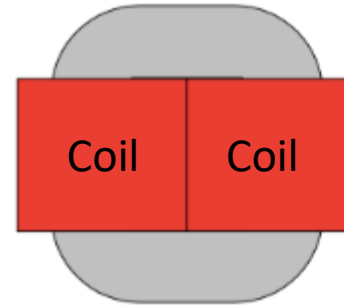
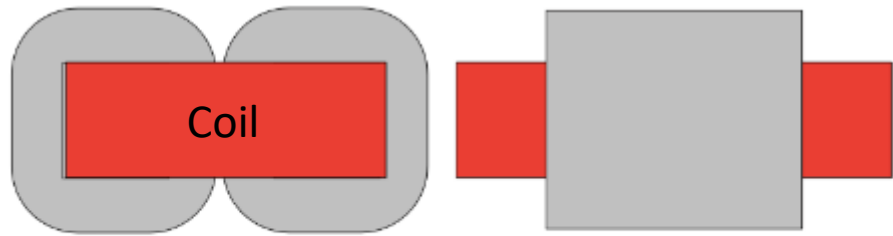
Perform DOE based on:

- given AC density
- given DC density
- setting composite core at given effective permeability

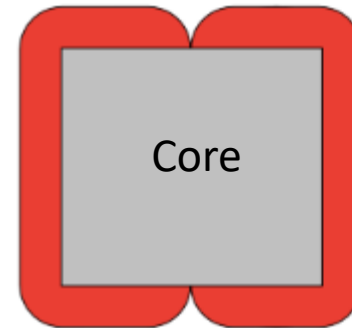
$$B_{Fe} \propto \frac{Ni}{l_{Fe}} \left[\frac{\mu_{DC}}{\frac{l_{gap}}{l_{Fe}} \mu_{DC} + 1} \right]$$



Shell Games



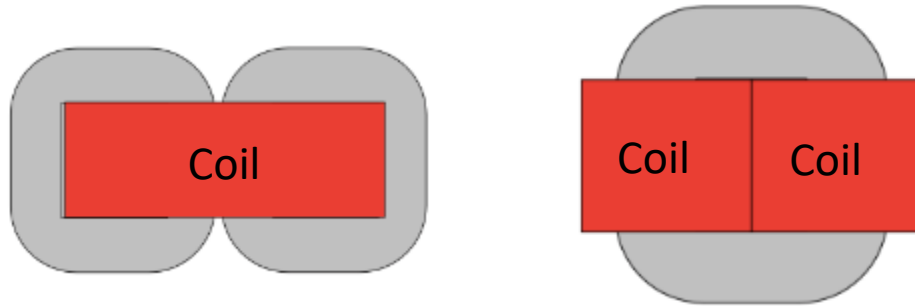
E Core type



U Core type

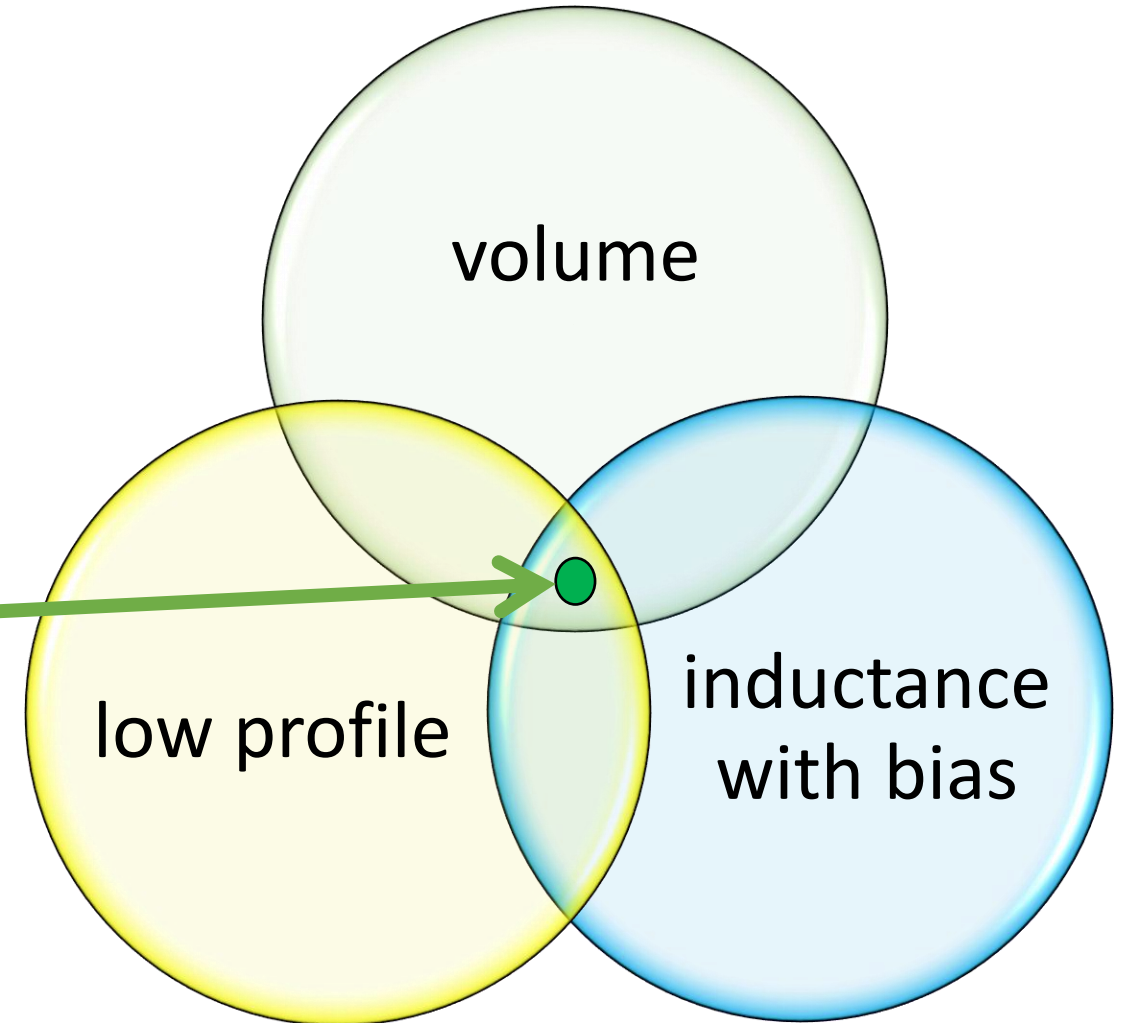
For a given volume, configuration possibilities seem endless.

Shell Games



E Core type U Core type

Use iterative computer method to select lowest loss configuration for increasing constraints:



Shell Games: Expected Relationships



$$VA_{Rating} \propto A_{core} \cdot A_{window} \cdot J_{AC} \cdot B_{AC} \cdot frequency$$

$$L_{DC} I_{DC}^2 \propto A_{core} \cdot A_{window} \cdot J_{DC} \cdot B_{DC}$$

$$\frac{dL}{L} \sim \frac{1}{\frac{l_{gap}}{l_{path}} \mu_{\Delta} + 1} \frac{d\mu_{\Delta}}{\mu_{\Delta}}$$

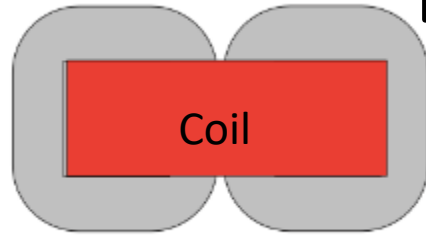
$$Coil Loss_{DC} \propto l_{gap}$$

$$B_{DC} \propto B_{AC} \propto \frac{1}{\sqrt{l_{gap}}}$$

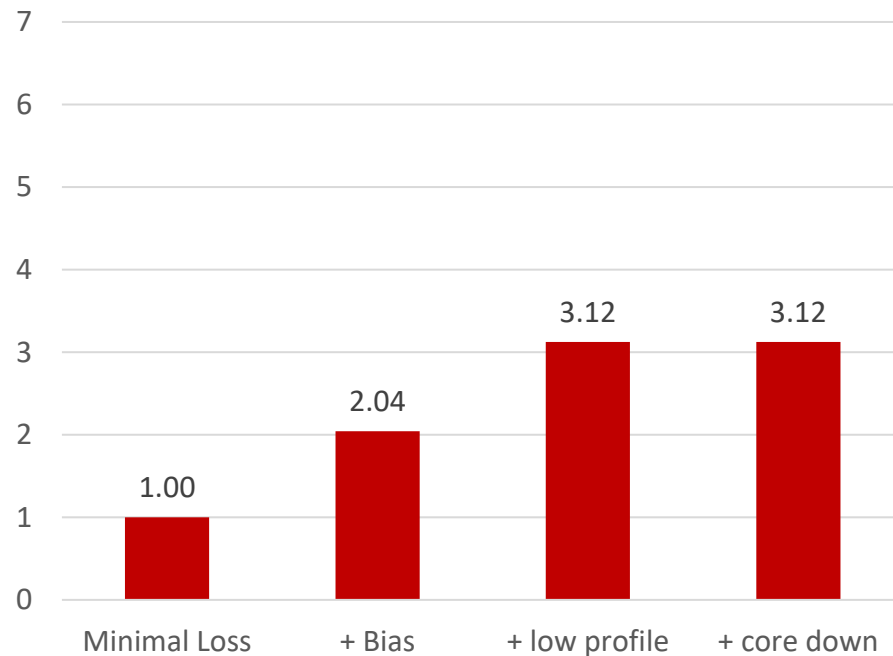
Understanding relationships facilitates tradeoffs.

Shell Games

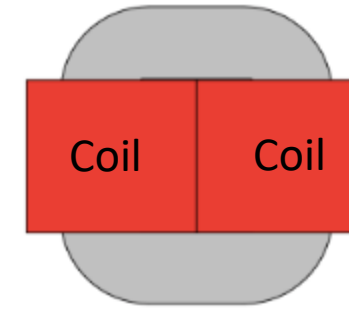
E Core type



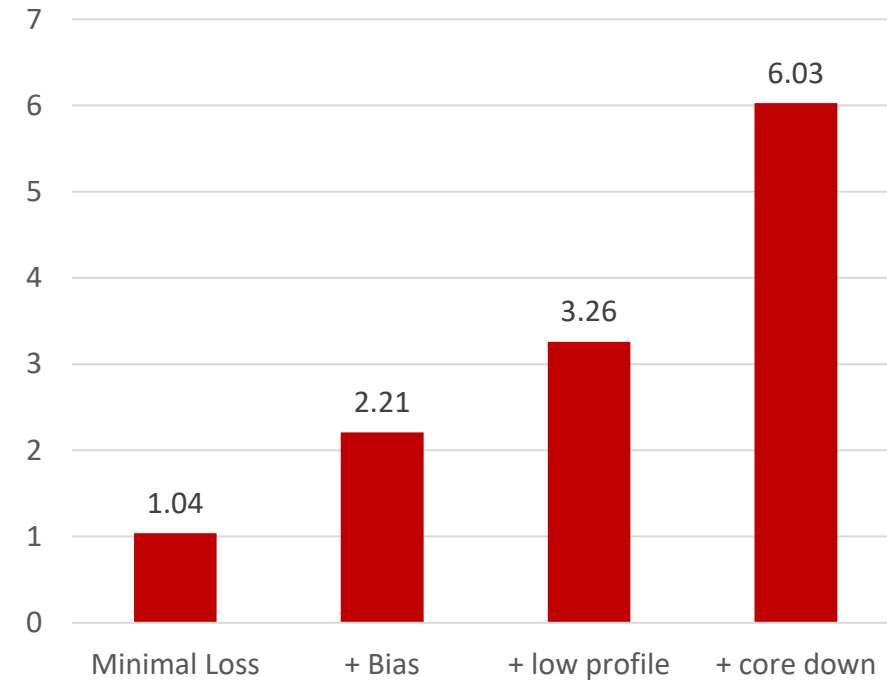
Normalized Loss



U Core type



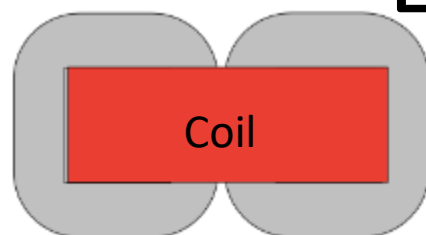
Normalized Loss



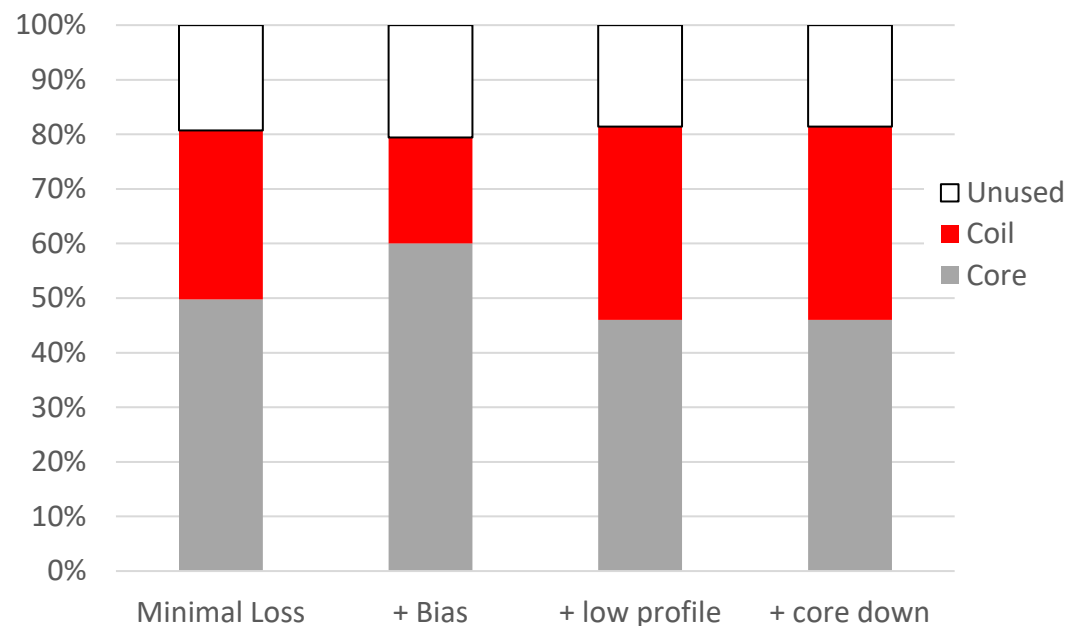
U core yields minimal loss at low profile when coil surface may be at base.
E core yields minimum loss at low profile when core is required at base.

Shell Games

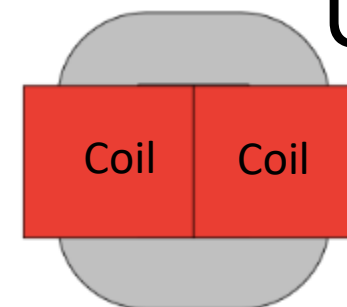
E Core type



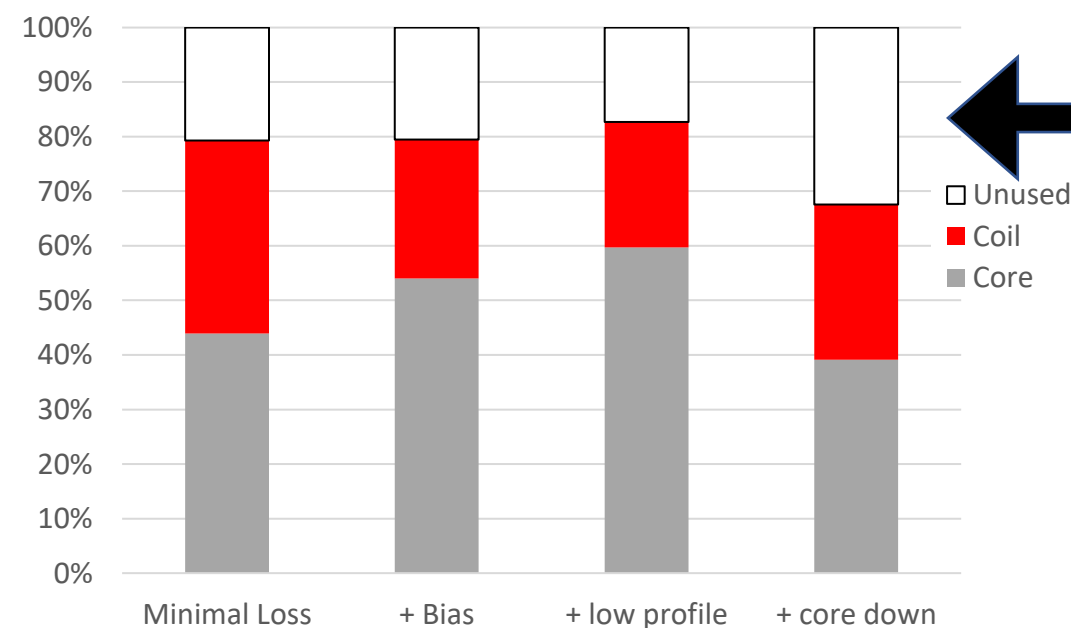
Relative Volume



U Core type

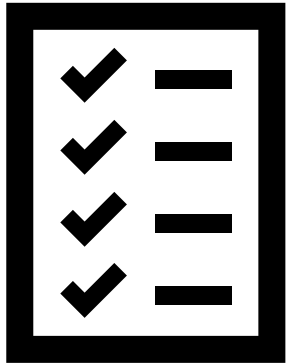
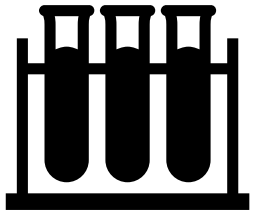
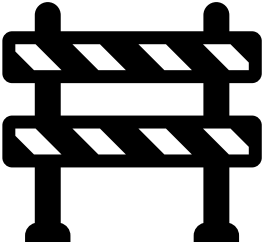


Relative Volume



Core down increases unused volume at low profile.

What do we know about coils?



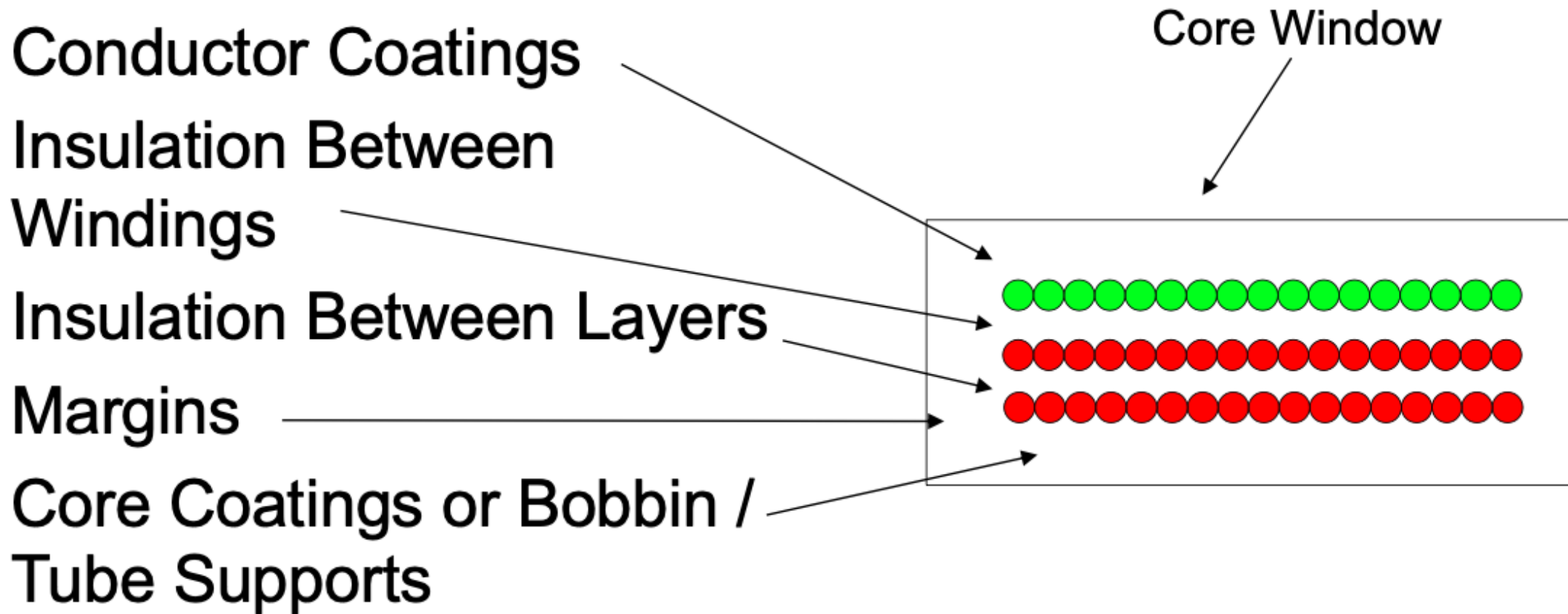
- linear – but process impacts
- insulation lowers net cross section
- often complex waveforms
- connections & packaging impacts
- wide temperature range
- reliability

So we evaluate, tradeoff ...
and evaluate again ...



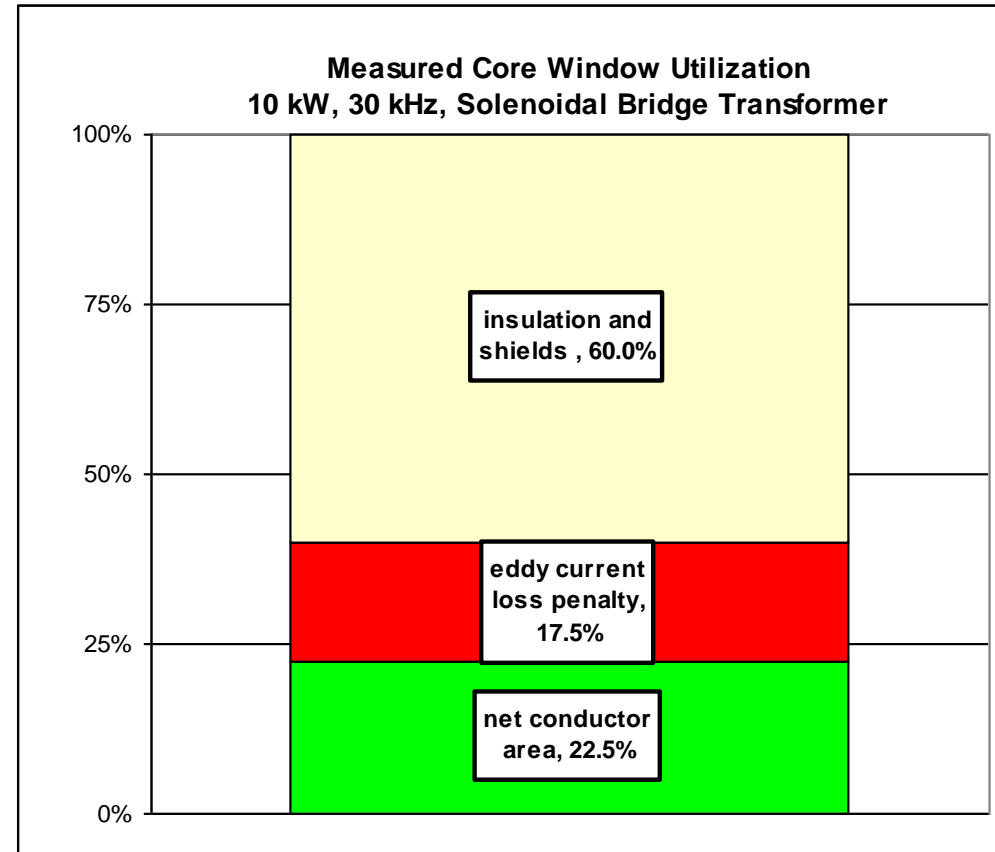
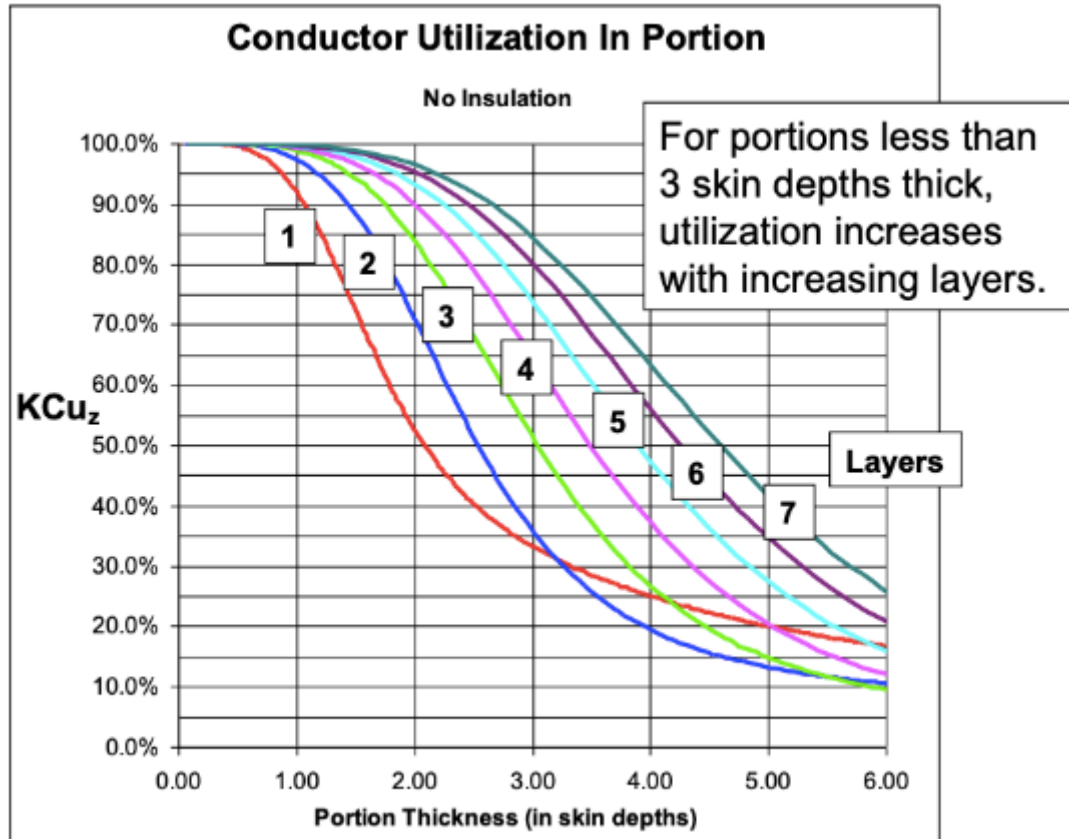
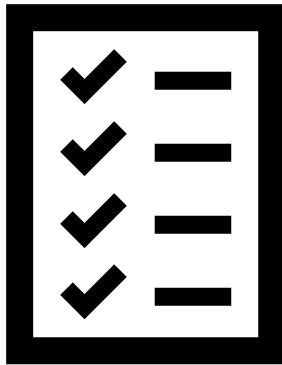
- Interleaves can increase effective utilization at high frequency
- Insulation reduces available window for conductors
- High current connections & terminals can drive total loss and design configuration
- Parallel conductors may not be effective from disparate coupling
- Normalized methods can facilitate understanding

Window Utilization: Insulation Penalty



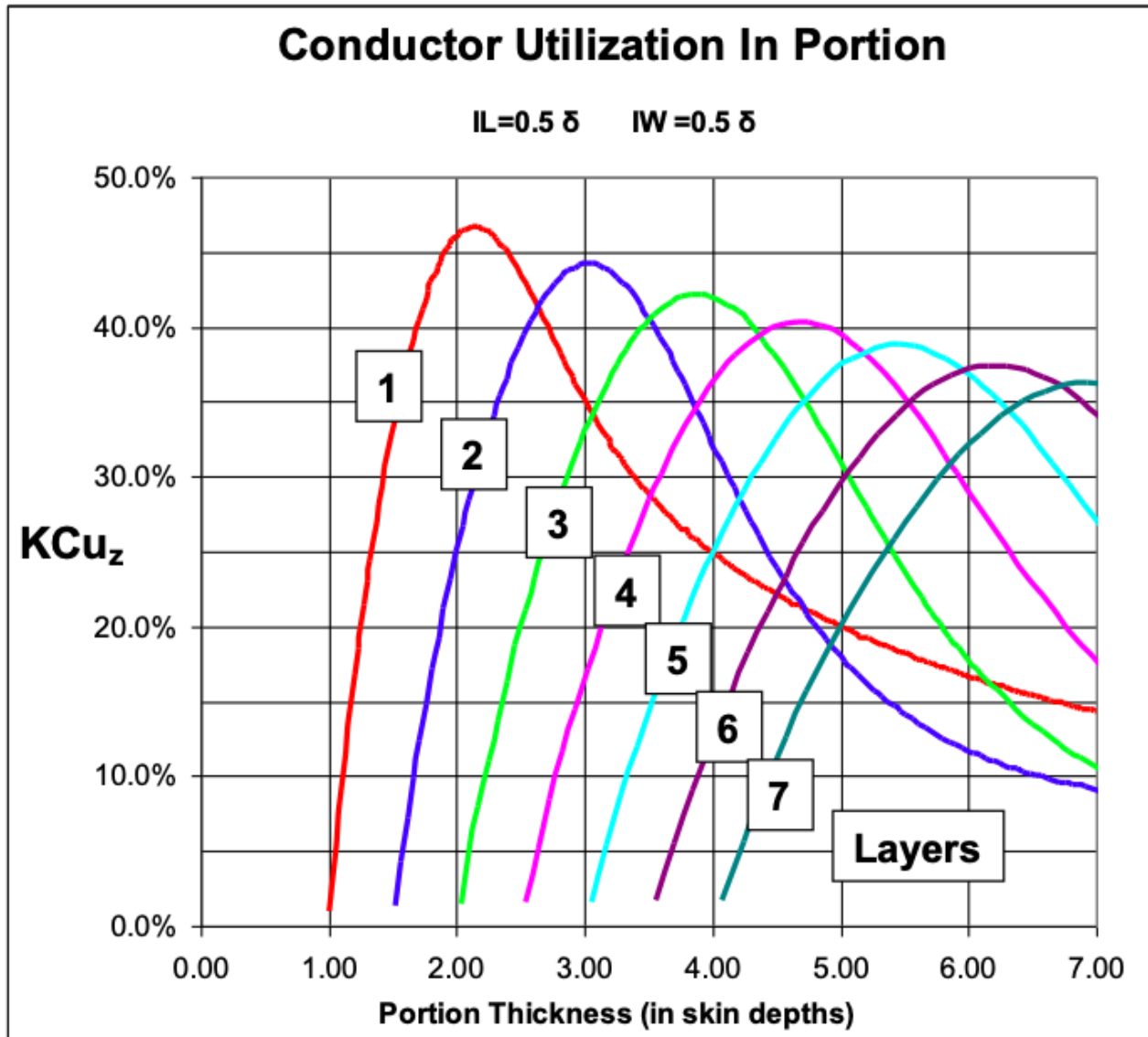
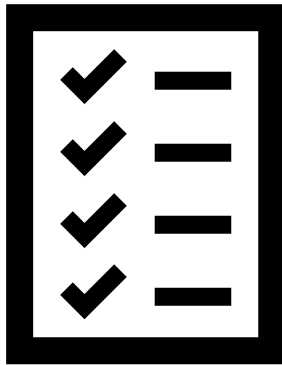
Insulation can lower utilization to less than a third of window.

Window Utilization: Eddy Current Impact



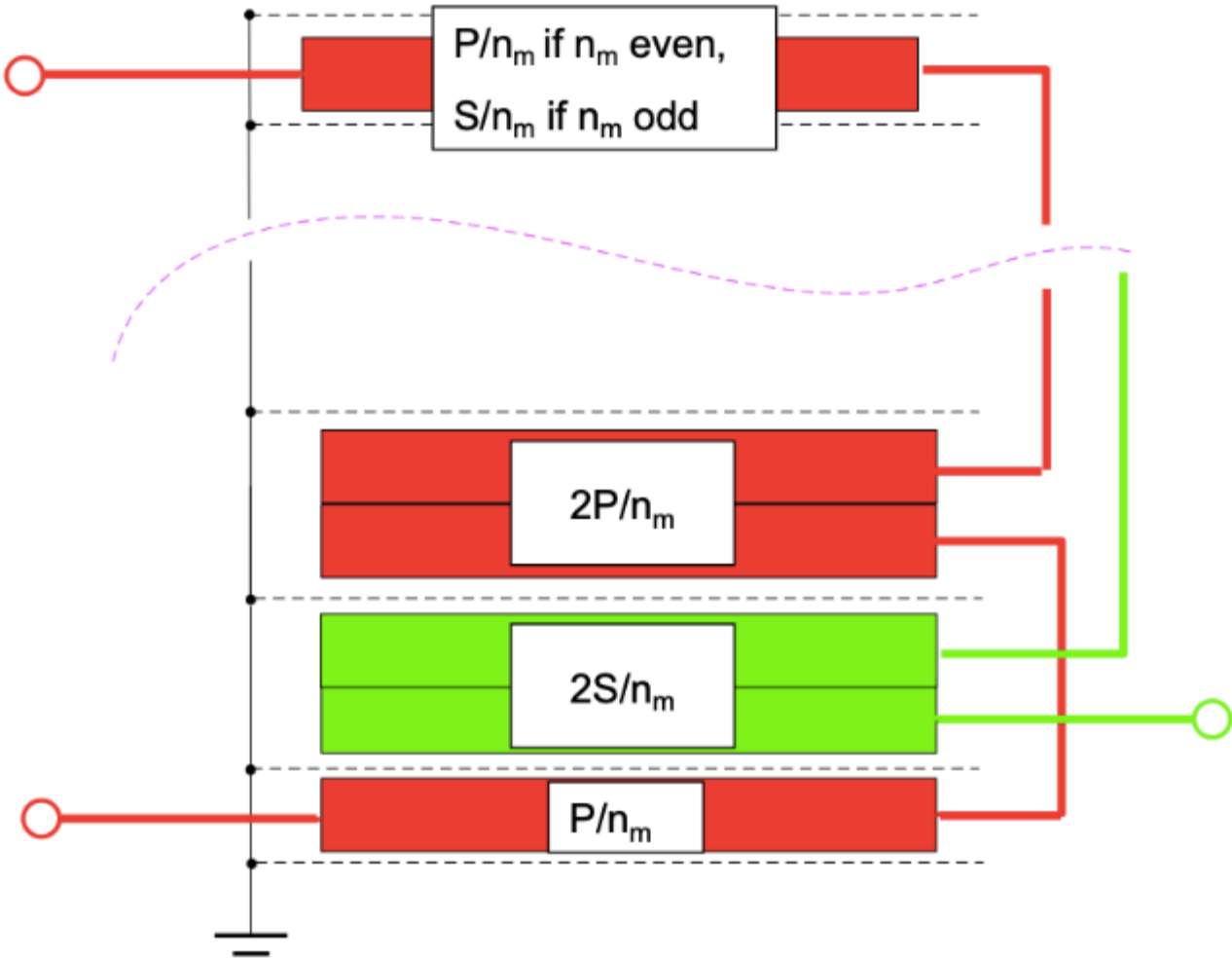
Dynamic field effects can lower utilization significantly further.
Coil loss is nonuniform, concentrated in layers at higher field strength.

Net Utilization (combined impacts)



Maximal conductor utilization is achieved with single layer portions, but large number of portions is required using multiple interleaves.

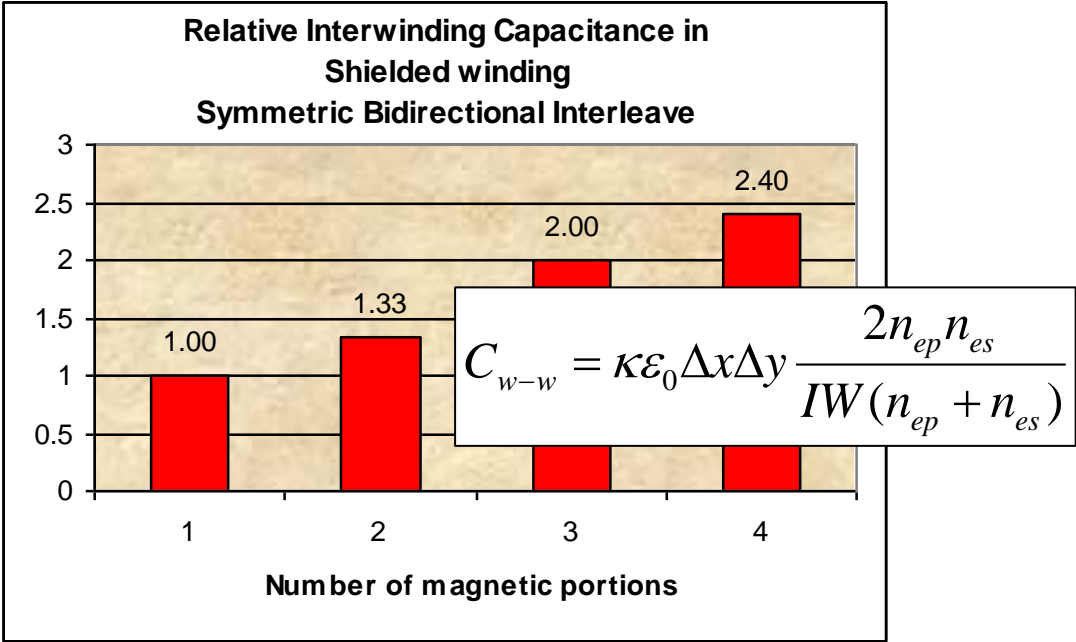
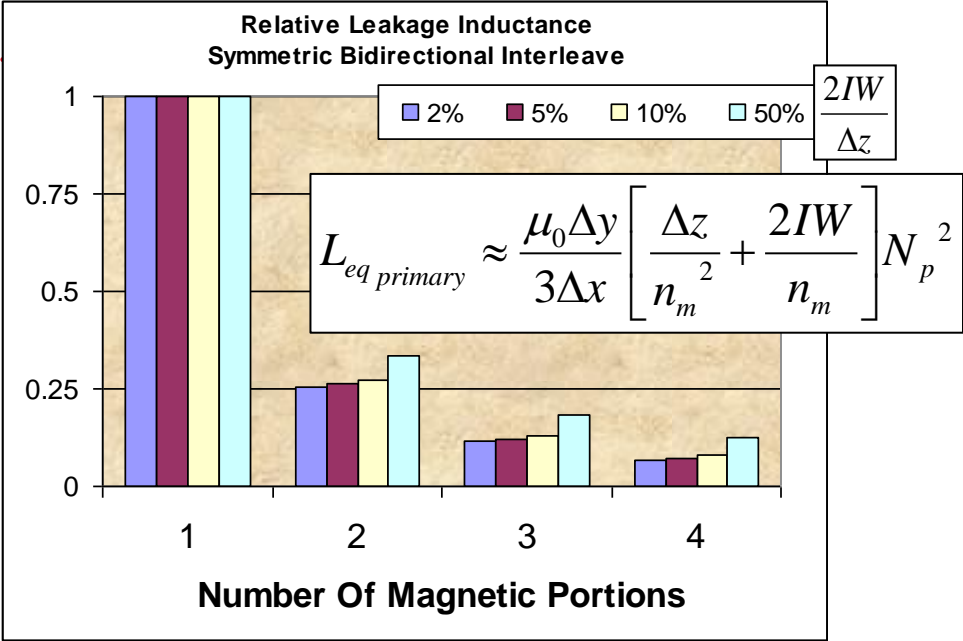
Bidirectional Interleaves



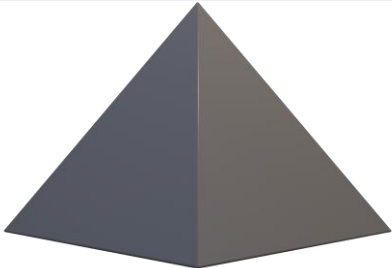
n_m	n_{ep}	n_{es}
1	1	1
2	2	1
3	2	2
4	3	2

For uniform construction; Primary must have at least n_m total layers. If n_m even, secondary must have at least $n_m/2$ total layers. For n_m odd, secondary must have at least nm total layers.

Reactive Tradeoffs



TRADEOFFS



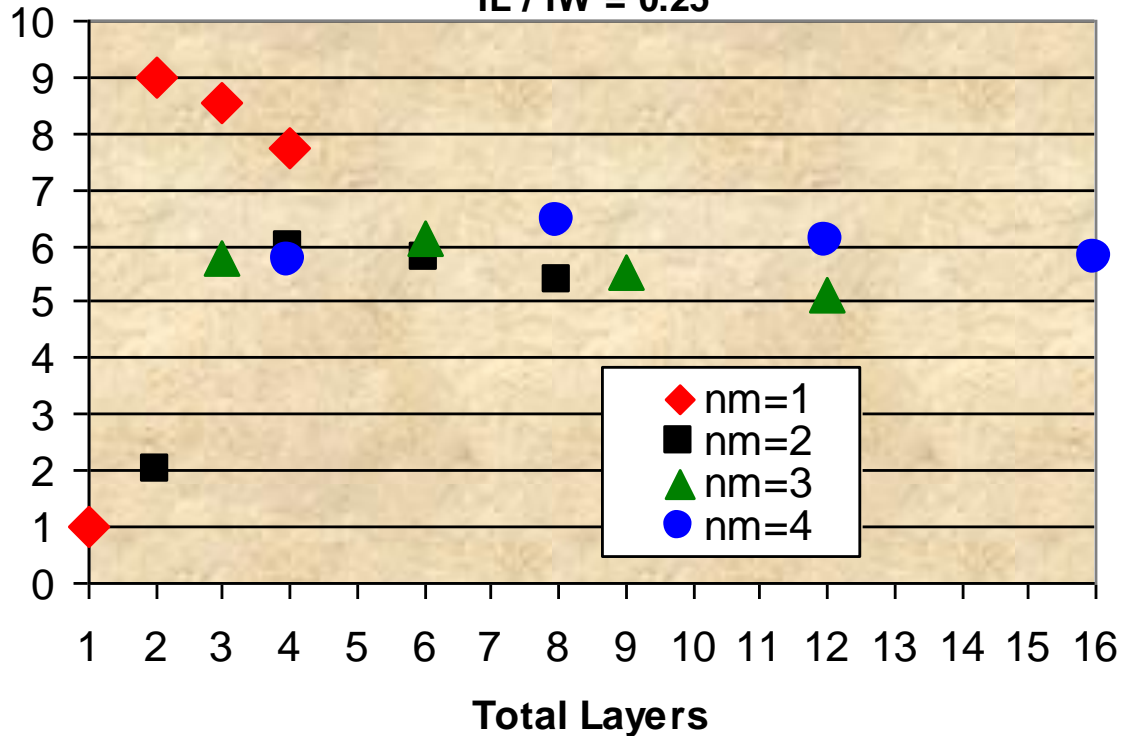
Distributed Capacitance

inductor or capacitor?

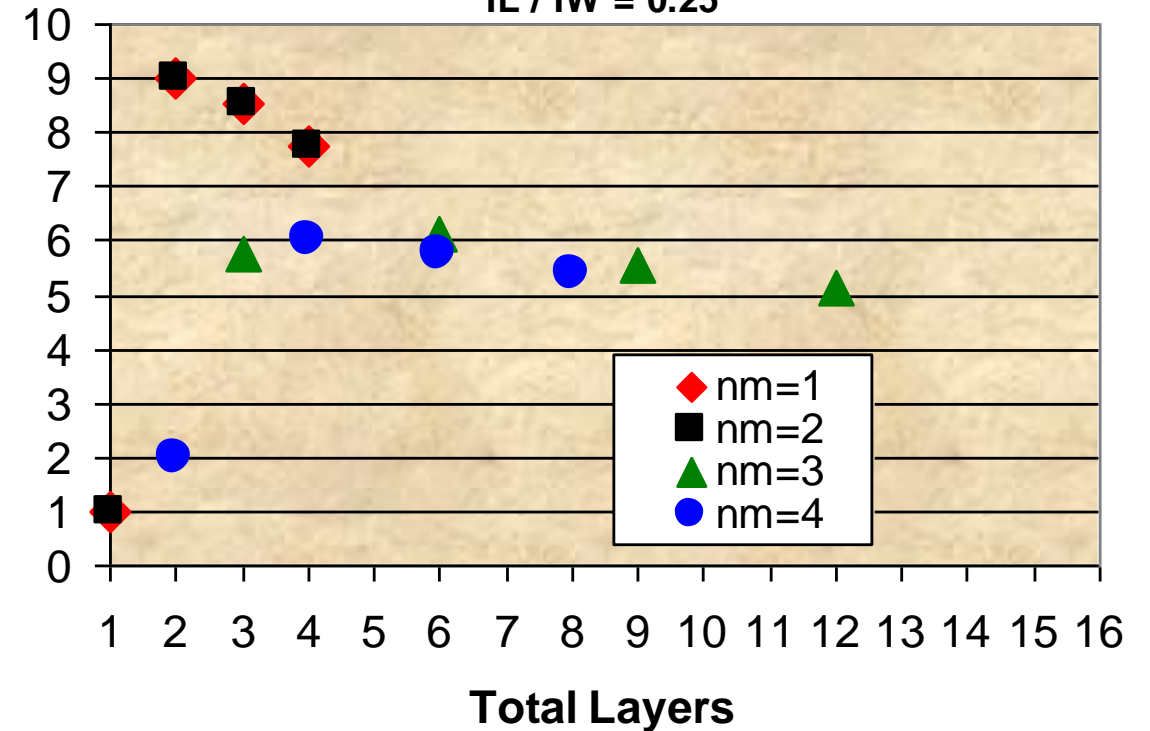
$$\text{Normalized Distributed Capacitance}_{\text{portion}} = \frac{\kappa \epsilon_0 \Delta x \Delta y}{6 IW}$$



Relative Distributed Capacitance In Shielded Winding
Symmetric Bidirectional Interleave: P winding
IL / IW = 0.25



Relative Distributed Capacitance In Shielded Winding
Symmetric Bidirectional Interleave: S winding
IL / IW = 0.25

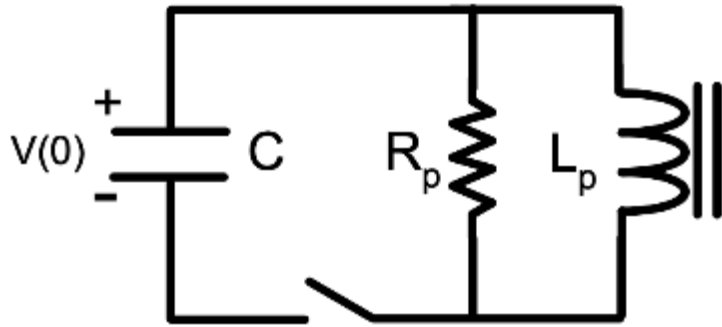
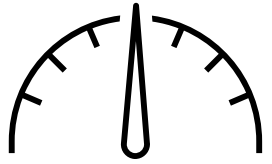


For single interleave, splitting high voltage winding into two discrete portions is beneficial to reduce total coil distributed capacitance.



Adventures in Design

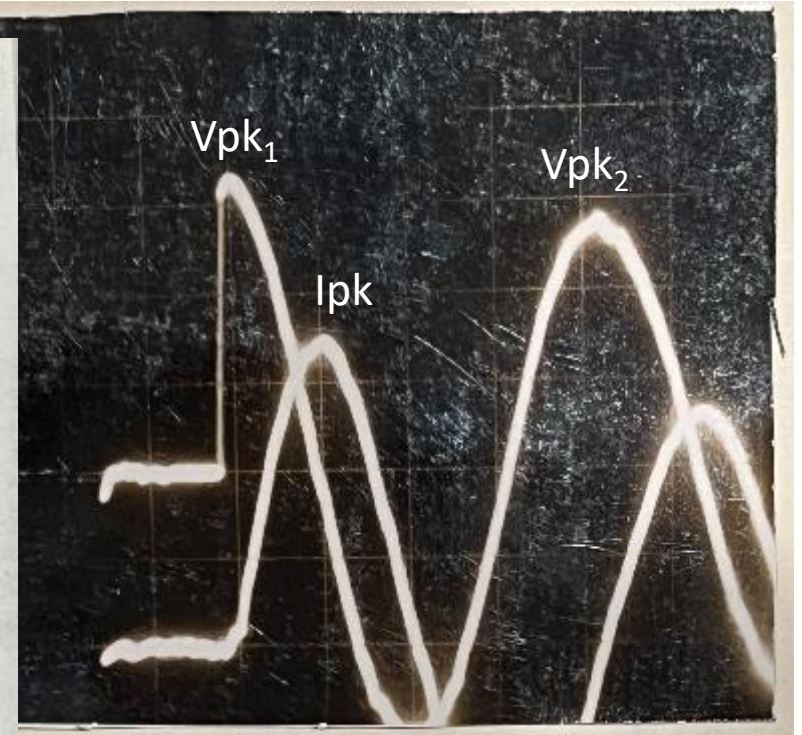
Snubber Inductor



$$L = \frac{(Vpk_1)^{\frac{3}{4}} (Vpk_2)^{\frac{1}{4}}}{\omega Ipk}$$

Inductor V. Gauram 5/12/24

$V(t) = V_0 e^{-\alpha t} \cos \omega t$ Undamped response.
 $V(t) = L \frac{di}{dt}$
 $V(t) dt = L di$
 $\rightarrow \int V(t) dt = L i(t) + K$
 $\Rightarrow \int V_0 e^{-\alpha t} \cos \omega t dt = V_0 \frac{e^{-\alpha t}}{\omega^2 + \alpha^2} [\omega \sin \omega t - \alpha \cos \omega t]$
 Condition $i(0) = 0 \Rightarrow$ VALUE OF K
 So $i(t) = \frac{V_0 e^{-\alpha t}}{L(\omega^2 + \alpha^2)} [\omega \sin \omega t - \alpha \cos \omega t] + \frac{V_0 \alpha}{L(\omega^2 + \alpha^2)}$
 to get $i(0) = 0$



High amplitude and high frequency can be achieved using resonant methods.

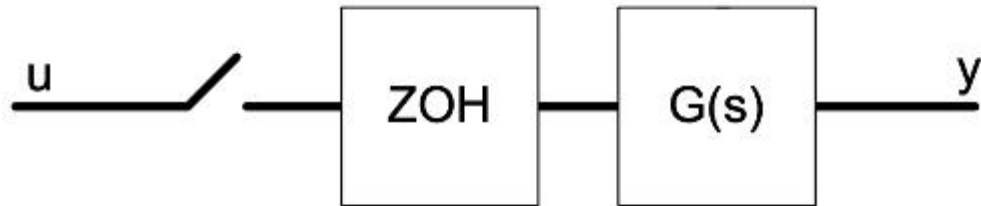
High Energy Inductor

150 J capacitor discharge

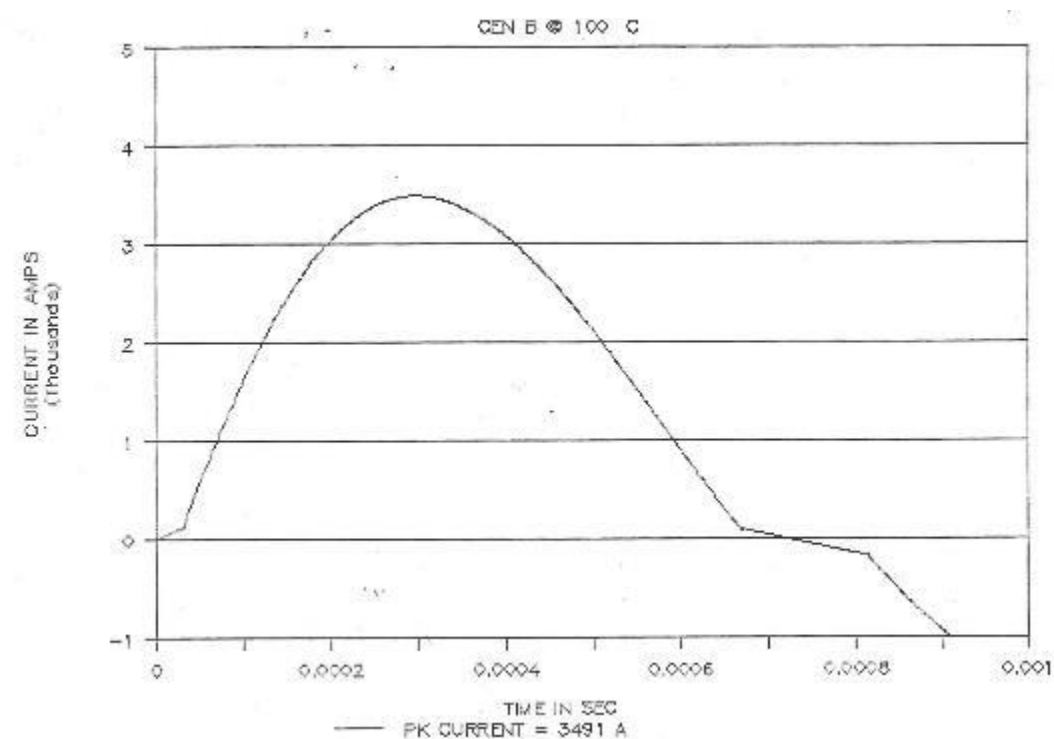
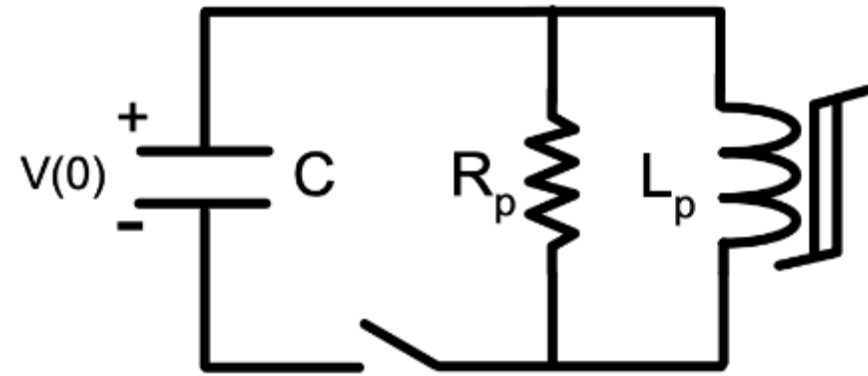
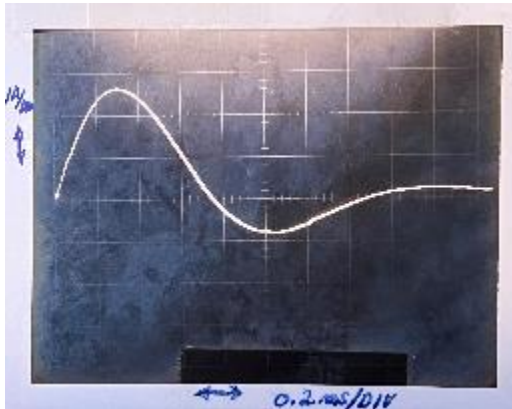
$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$G(s) = C(sI - A)^{-1}B + D$$

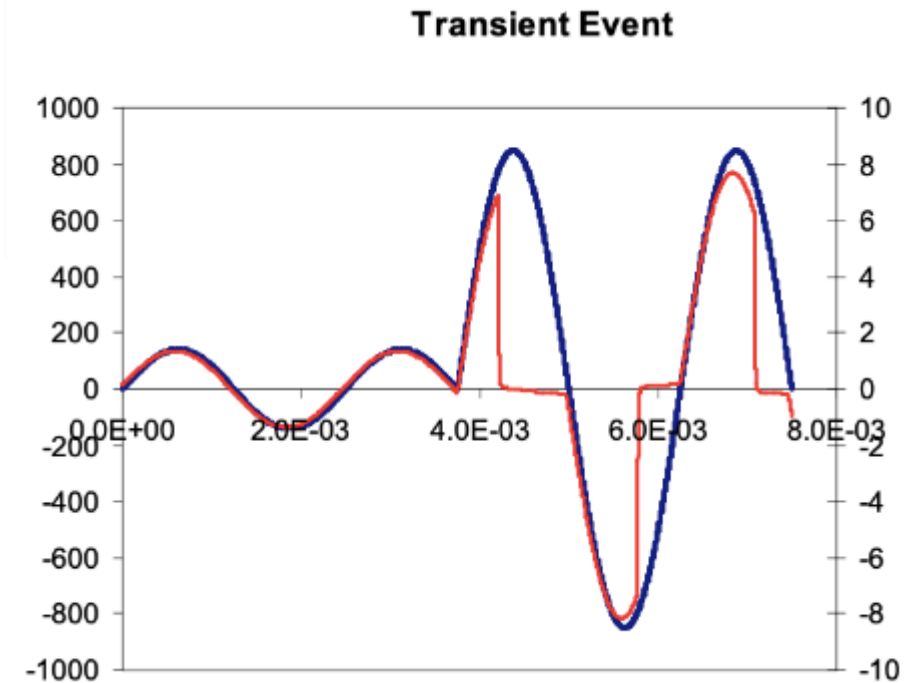
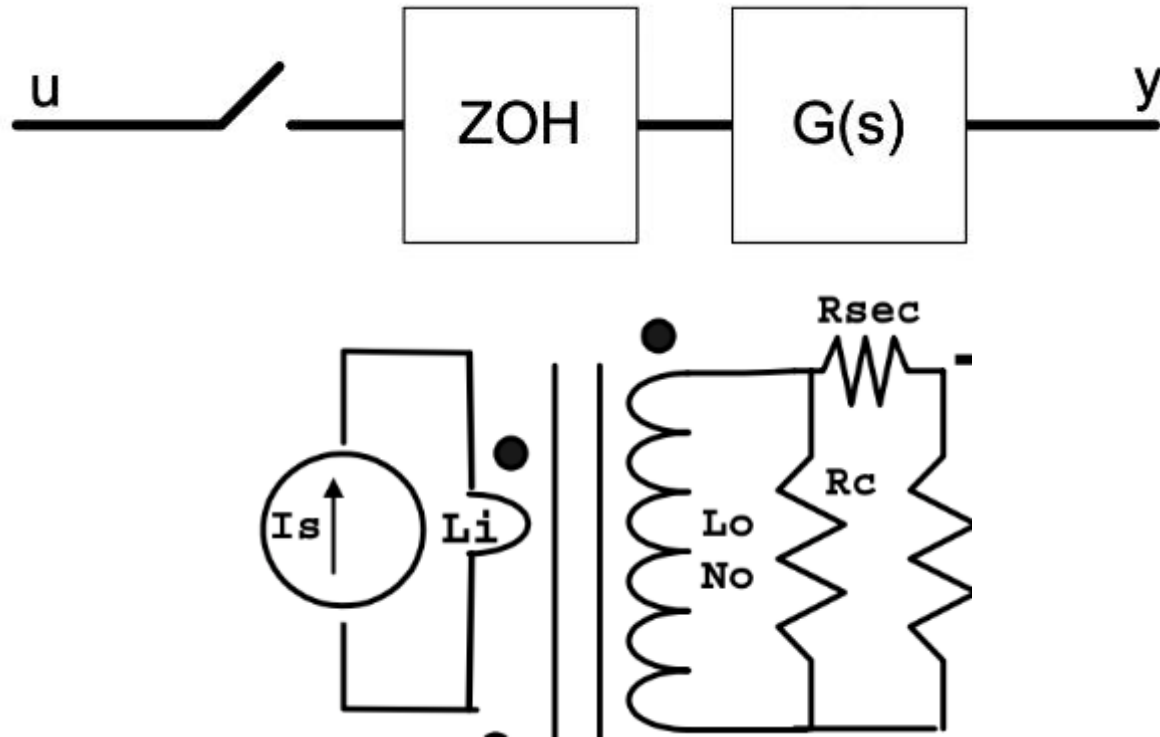


$$x(k + 1) = F x(k) + G u(k)$$



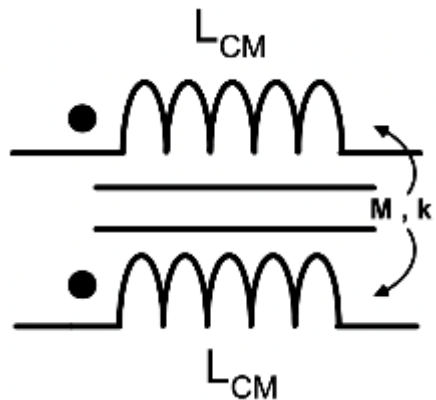
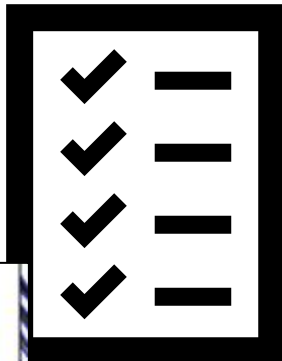
State equations with ZOH can simulate nonlinearity.

Saturating Current Transformer



Transient forcing functions can be considered and incorporated into custom design method.

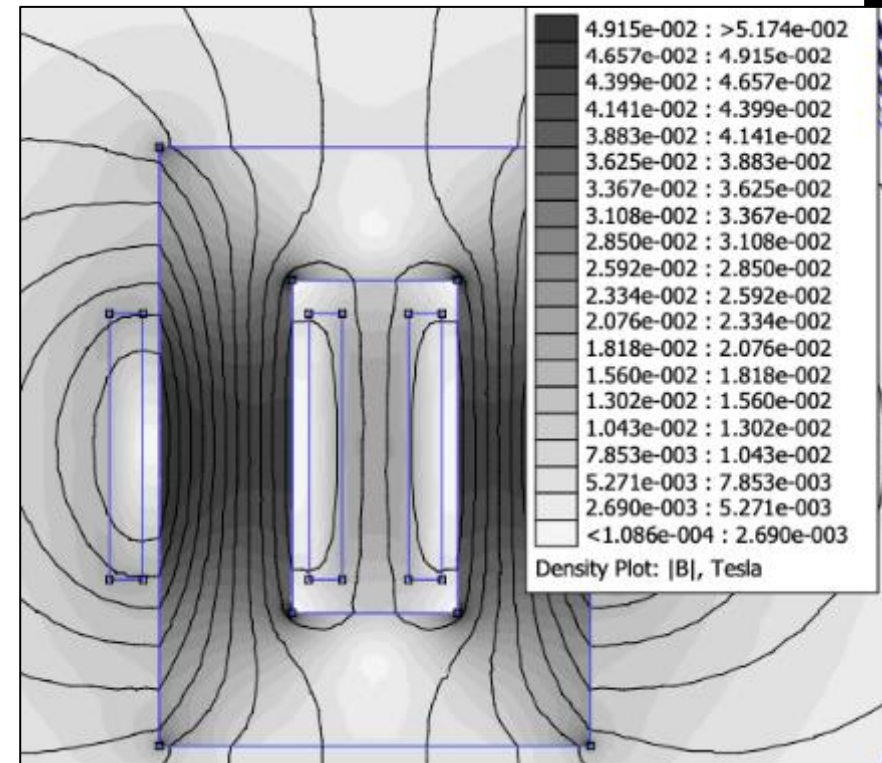
DM Problems with CM Inductor



$$L_{DM} = (1 - k)2L_{CM}$$

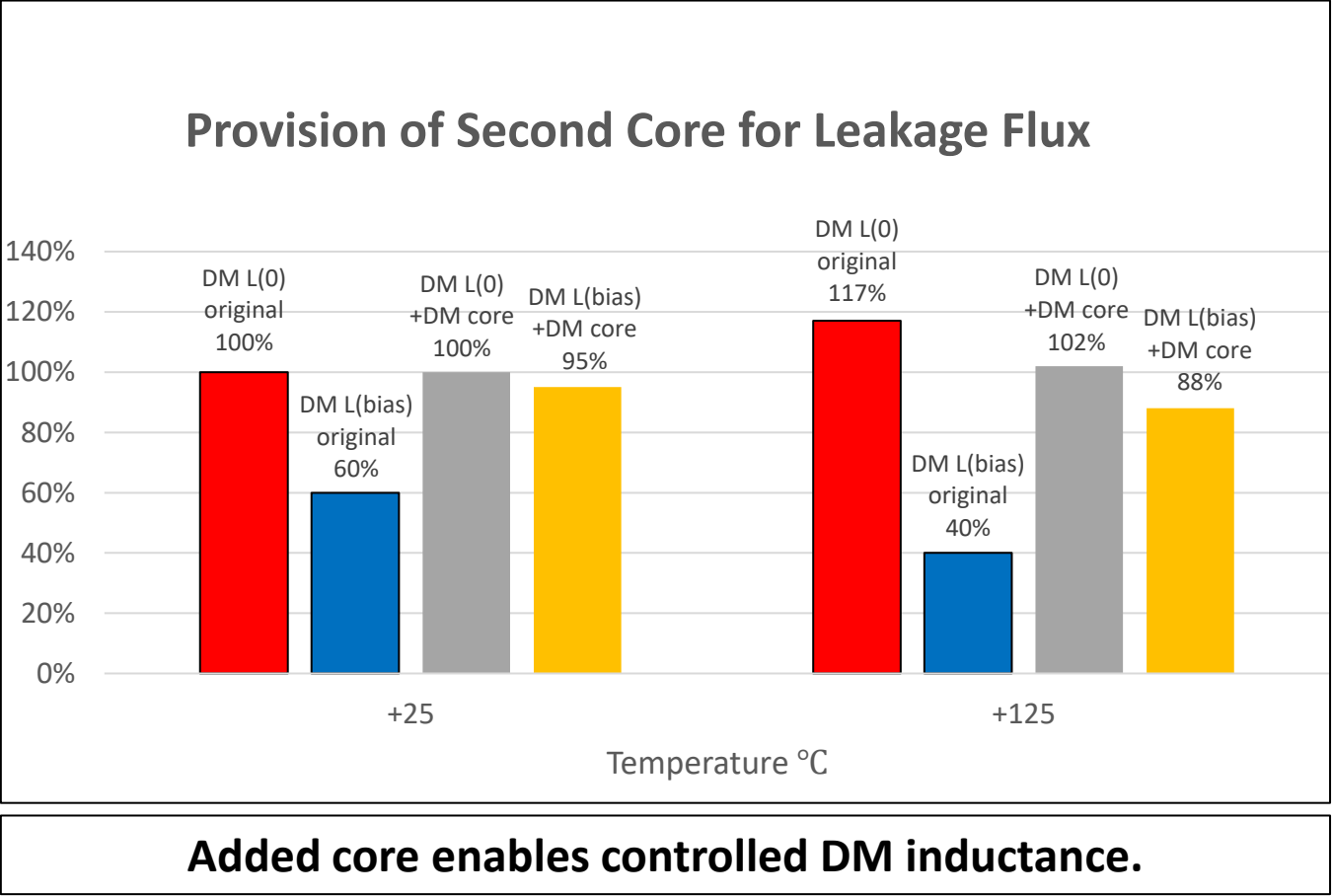
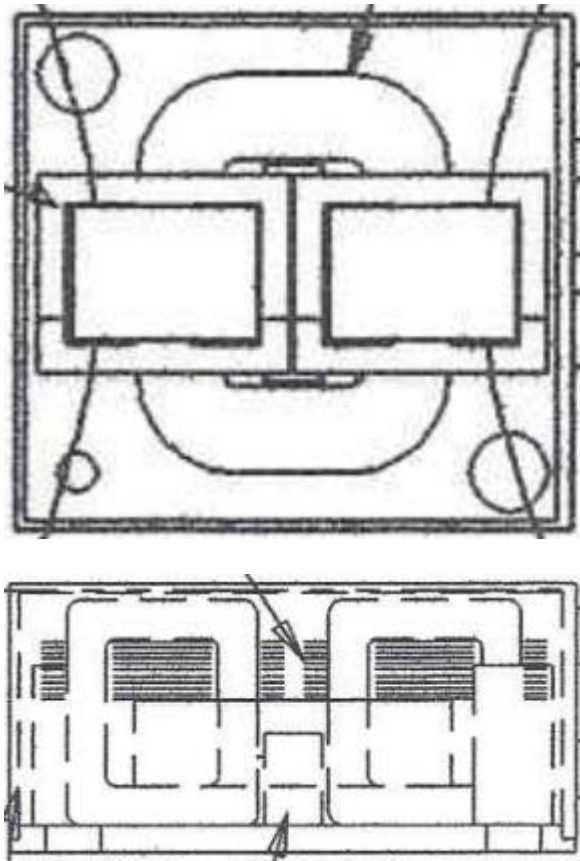
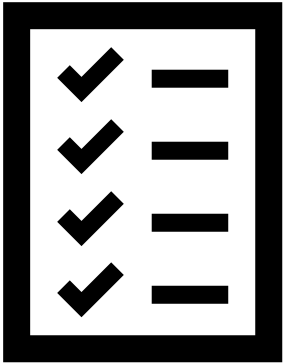
$$k \sim 96.8\%$$

- DC Leakage Flux
 - Intercepts ferrite CM core
 - Polarizing CM core and reducing effective permeability for DM flux especially at high temperature



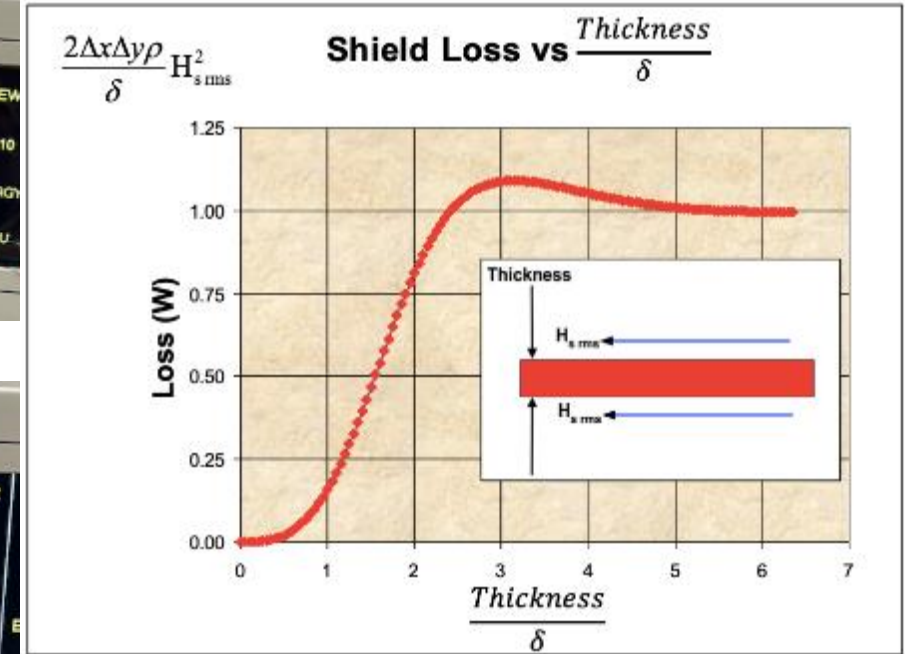
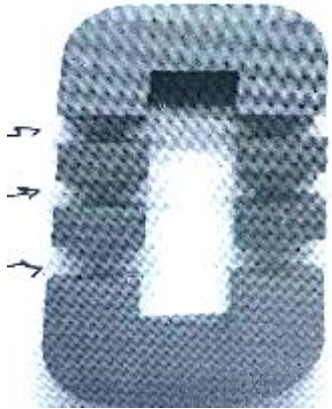
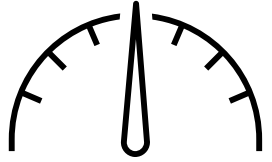
Add laminated core to enhance leakage flux with improved control.

Consistent DM Inductance



Improved design achieves DM inductance at bias current over temperature.

Distributed Gap Control



High amplitude testing successfully controls gapping process results.

A detailed technical drawing of a three-phase circuit breaker assembly. The drawing shows the main body of the breaker, which is a rectangular metal enclosure. On the left side, there is a large, complex operating mechanism with multiple moving parts, including a handle and a locking system. On the right side, there is a terminal block with three large, rectangular terminals for connecting the power lines. The entire assembly is mounted on a base with four mounting feet. The drawing is a perspective view, showing the top, front, and side of the unit.

-

Liquid Cooling Calculations

Reference: Cooling Techniques for Electronic Equipment
 TK 765025, 573
 Dan's Library
 Wiley

V. D. Quinn
 10/12/90

(I) TEMPERATURE RISE OF LIQUID COOLED SYSTEM

Eqn 6.7

$$w = \frac{Q}{\Delta T_{cp}}$$

Q Heat Dissipation	Btu/hr	cal/sec
ΔT_{cp} Temp rise	$^{\circ}F$	$^{\circ}C$
Q & properties	$\frac{Btu}{lb \cdot ^{\circ}F}$	$\frac{cal}{g \cdot ^{\circ}C}$
w Flow	lb/hr	g/sec

OR $\Delta T = \frac{Q}{w \cdot Cp}$

(II) COOLING RATE IN LIQUID COOLED SYSTEM

(USEFUL TO FIND MINIMUM SURFACE & REVERSE PROBLEM)

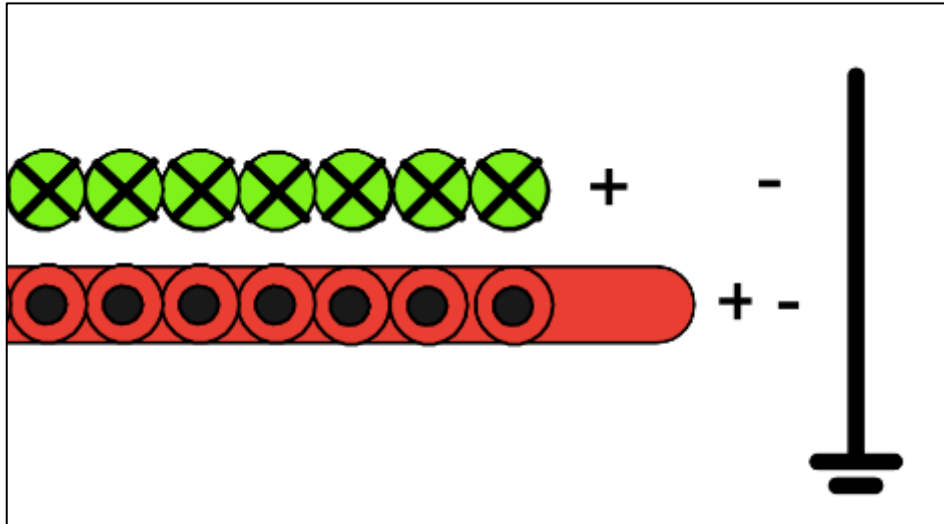
Eqn 5.7

a) $\Delta T = \frac{Q}{A \cdot A}$

Q Heat Dissipation	Btu/hr	cal/sec
A & Forced Convection coefficient	$\frac{Btu}{sq ft \cdot ^{\circ}F}$	$\frac{cal}{sq cm \cdot ^{\circ}C}$
A Surface Area	ft^2	cm^2
ΔT Temp rise	$^{\circ}F$	$^{\circ}C$

Stories VWQ

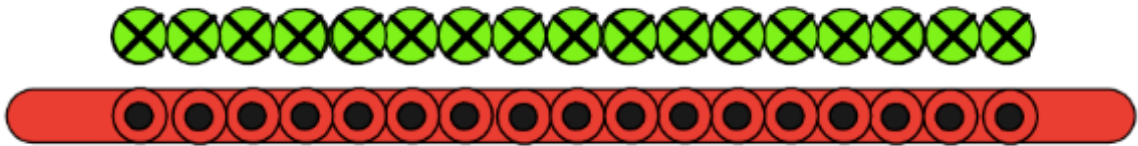
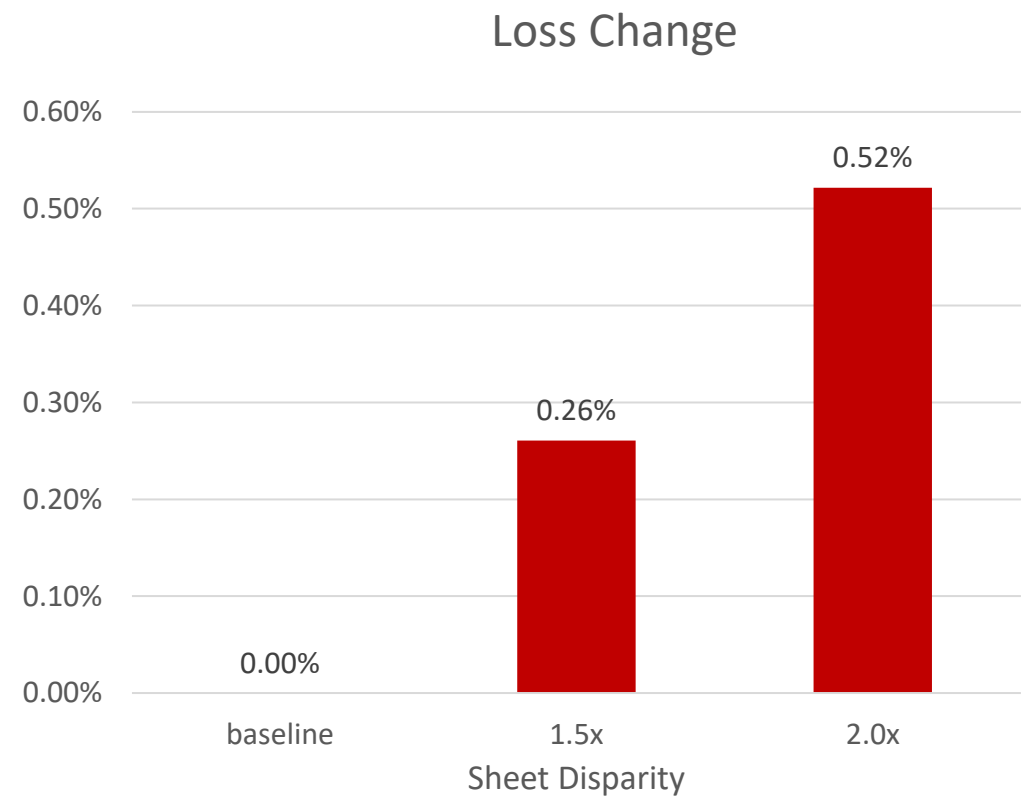
Acute Edge



edge radius mils	5
clearance mils	50
Approximate Field Enhancement Factors:	
sphere & plane	9.90
cylinder & plane	3.76
adjacent cylinders	2.51

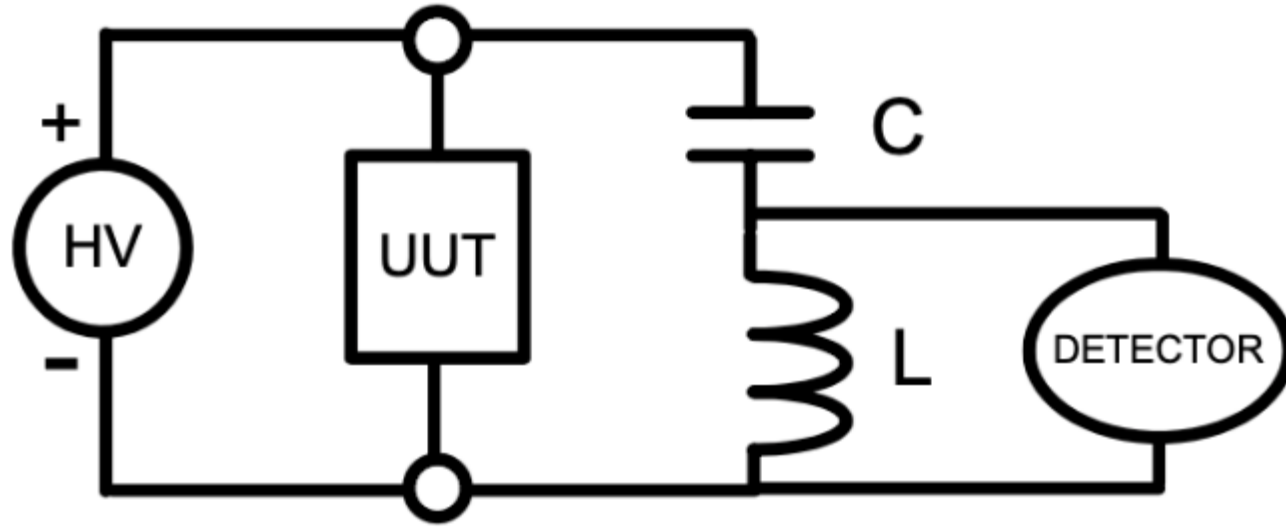
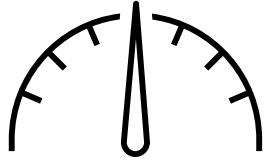
Thin conductors as preferred for high frequency current cause significant electric field enhancement at sheet edges.

Short Sheet



Disparate wider sheet provides negligible loss reduction benefit.

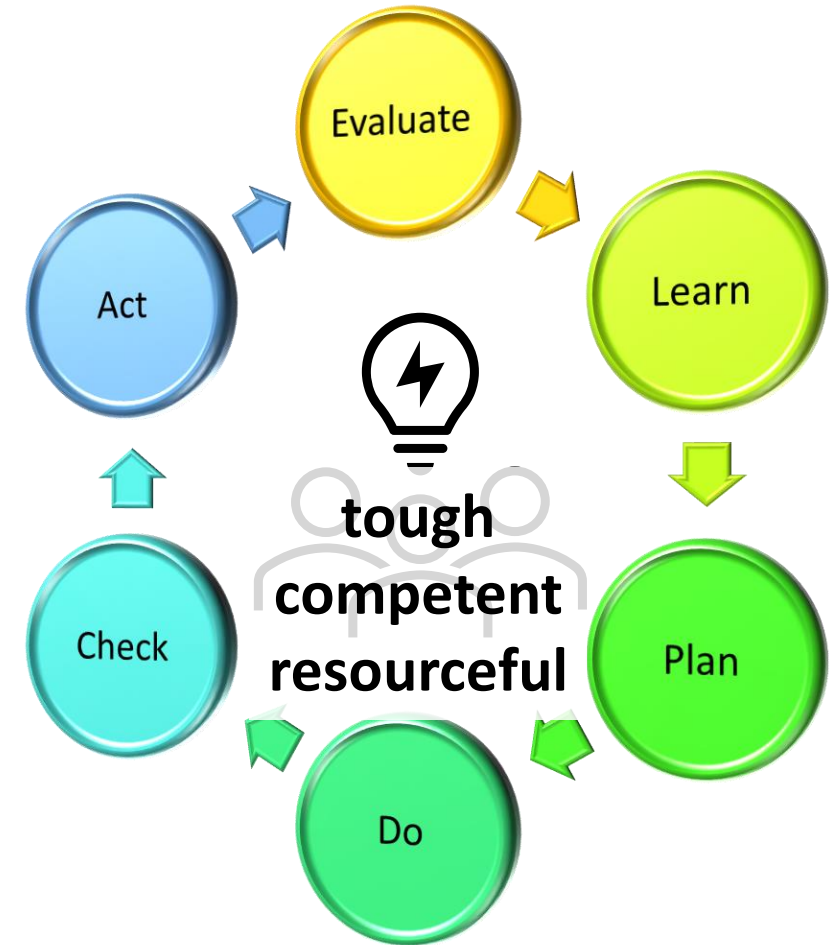
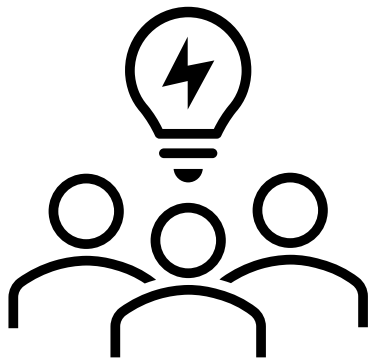
Partial Discharge Test Methods



Custom Partial Discharge equipment is needed for HV intrawinding test condition.

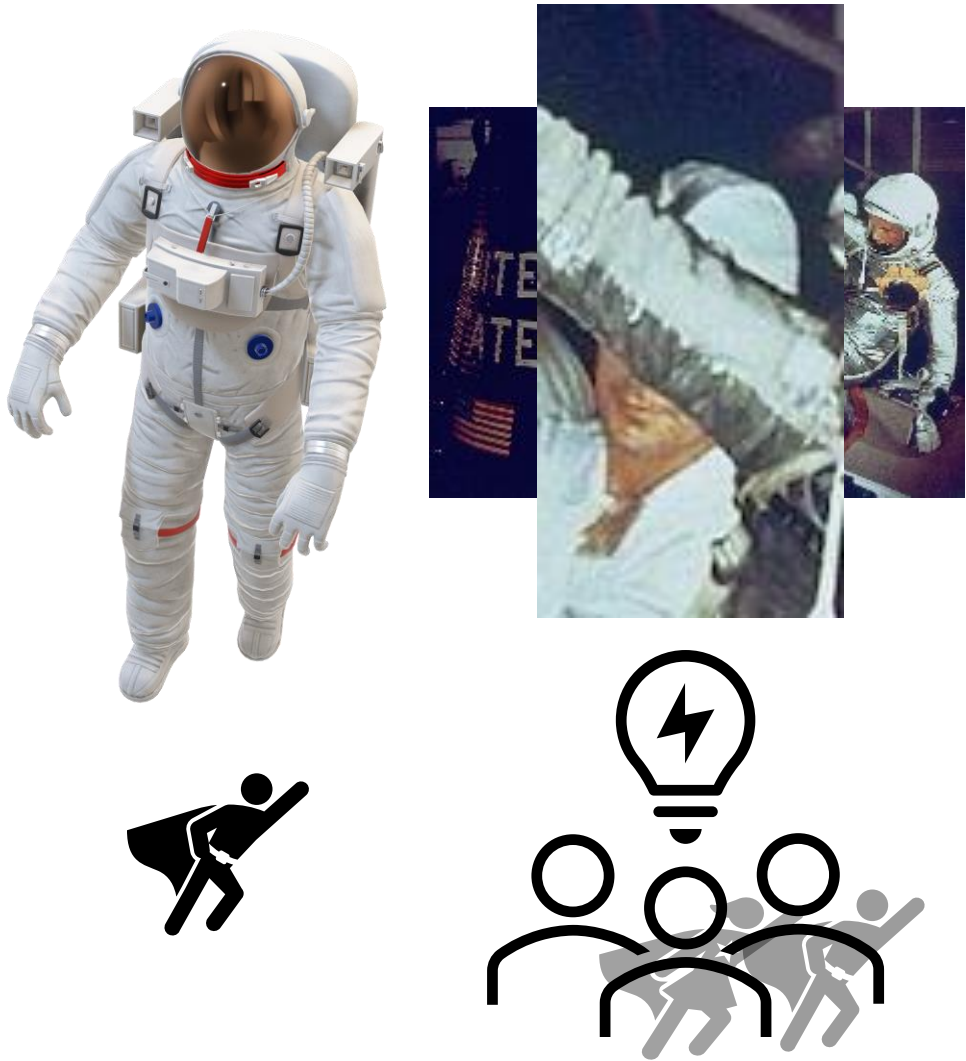
We celebrate ...

- Technology advancement
 - we don't know what we don't know
- Limited resources
 - we can't do everything we wish to do



For the love of Custom Magnetics ...

The story continues ...



Reference and Recognition

<https://www.pσμα.com/publications>

With sincere and deep appreciation for James J. Carey who took a risk and gave a fledgling Physics graduate an opportunity to become a magnetics design engineer ... mentoring me along a path to merge academic theory with practical measurement.