

Frequency, where we are today, and where we need to go

Ionel Dan Jitaru

Rompower Energy Systems Inc.

6262 N. Swan Rd., Suite 200

Tucson, Arizona 85718

Tucson Arizona



OUTLINE

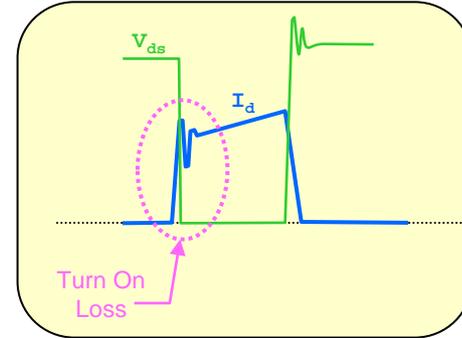
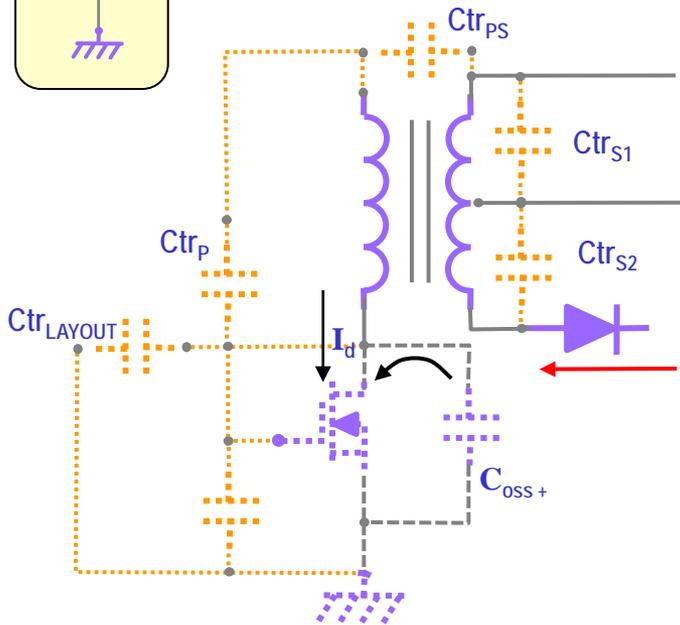
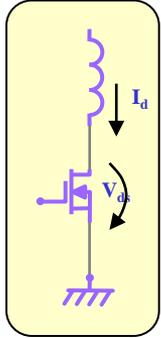
- **Directions in topologies and operation frequency**
- **Magnetic limitations at high frequency**
- **Example of magnetic optimization for high frequency**
- **Magnetic structures for very high frequency**

TRENDS IN TOPOLOGIES

TRENDS IN TOPOLOGIES

- **Trends in Operation Frequency**
- **Resonant derived topologies**
- **”True” Soft Transition topologies**
- **Future Trends**

Switching Losses on the primary switchers



The energy contained in the parasitic capacitance of the transformer/layout is quite often higher than the energy contained in C_{oss}

SiC and GaN technologies will not eliminate the need for Soft Switching

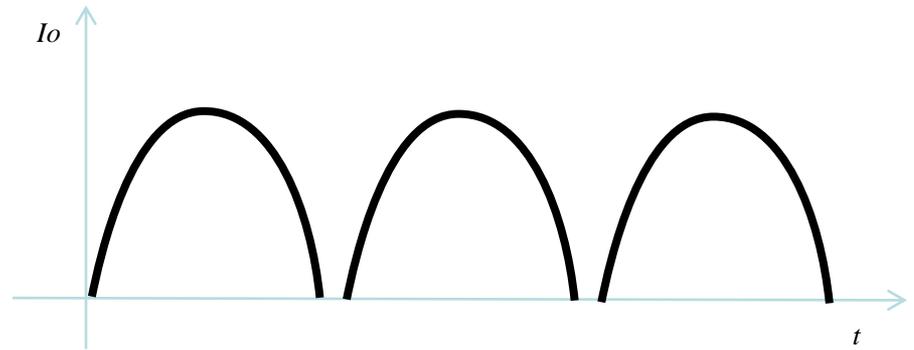
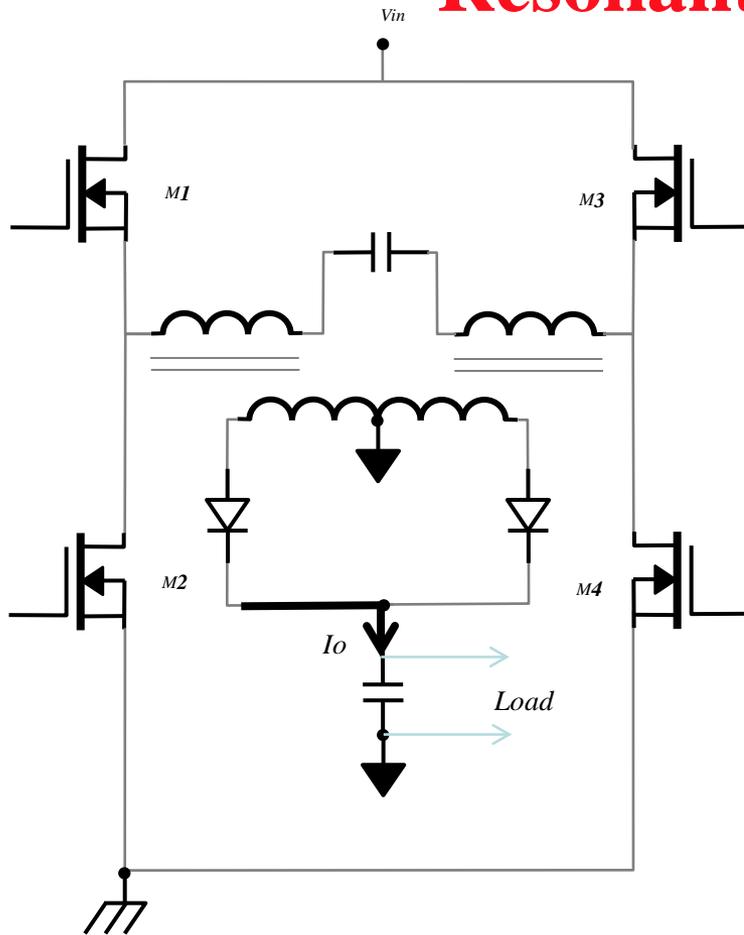
45W Flyback Transformer for adapters



750W Transformer for DC-DC Converter

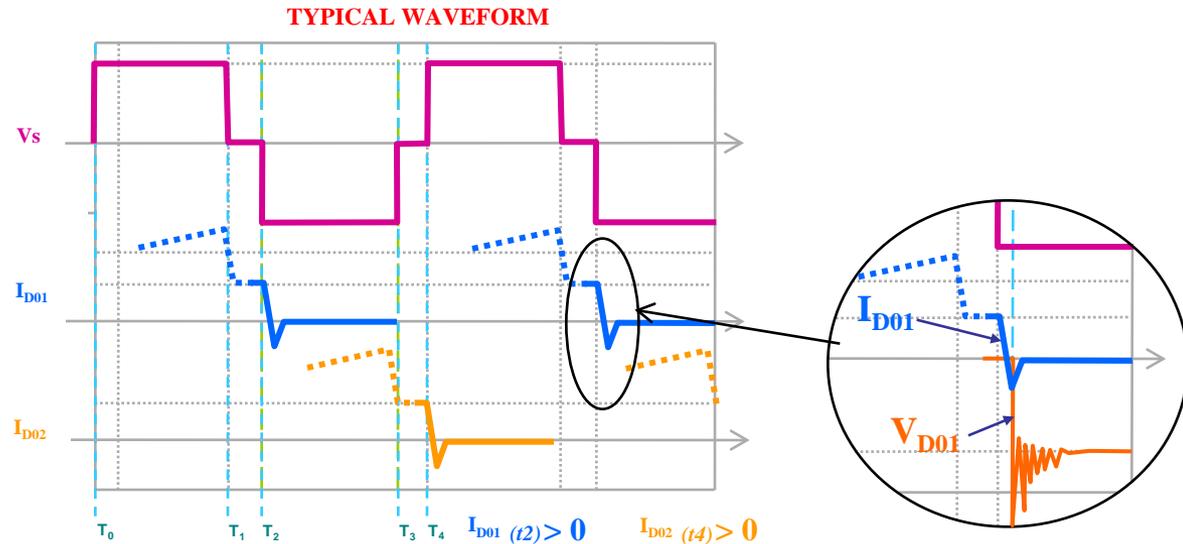
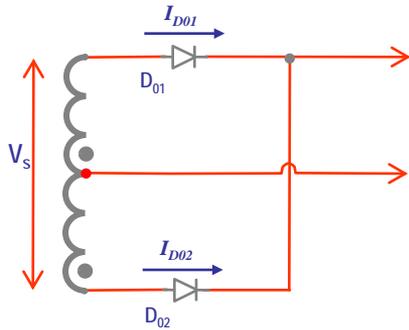


Resonant Derived Converter

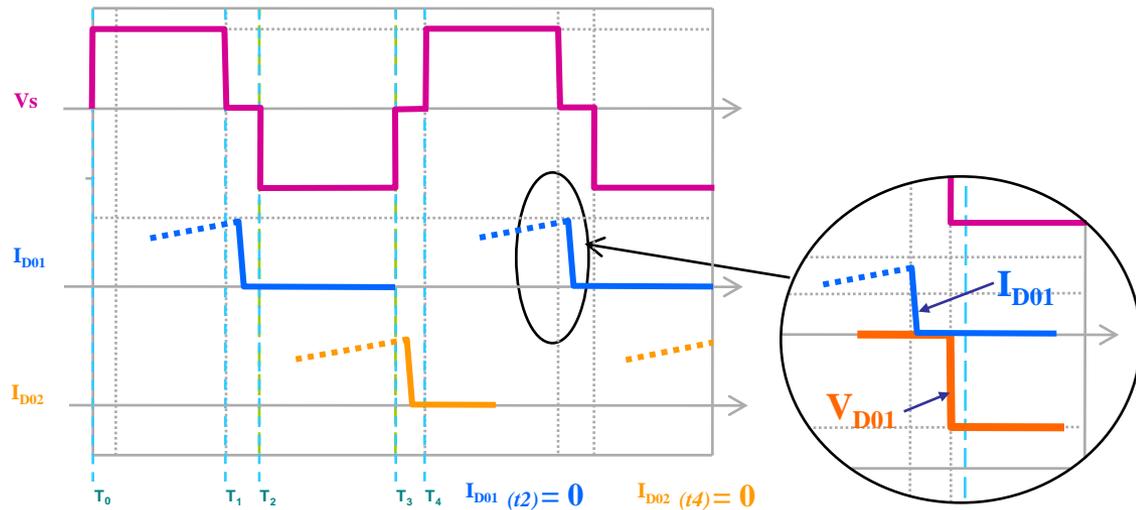
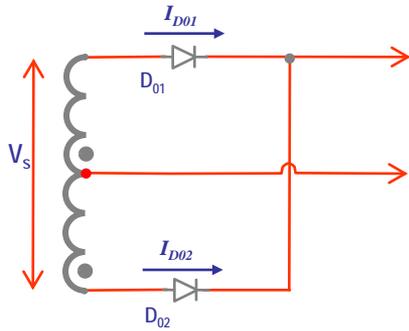


US Patent 7,187,263B2

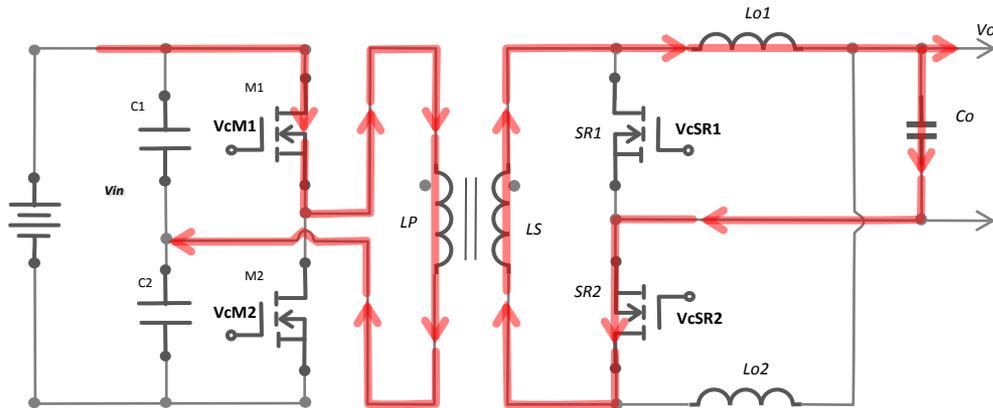
Reverse Recovery Effect in a Double Ended Converter



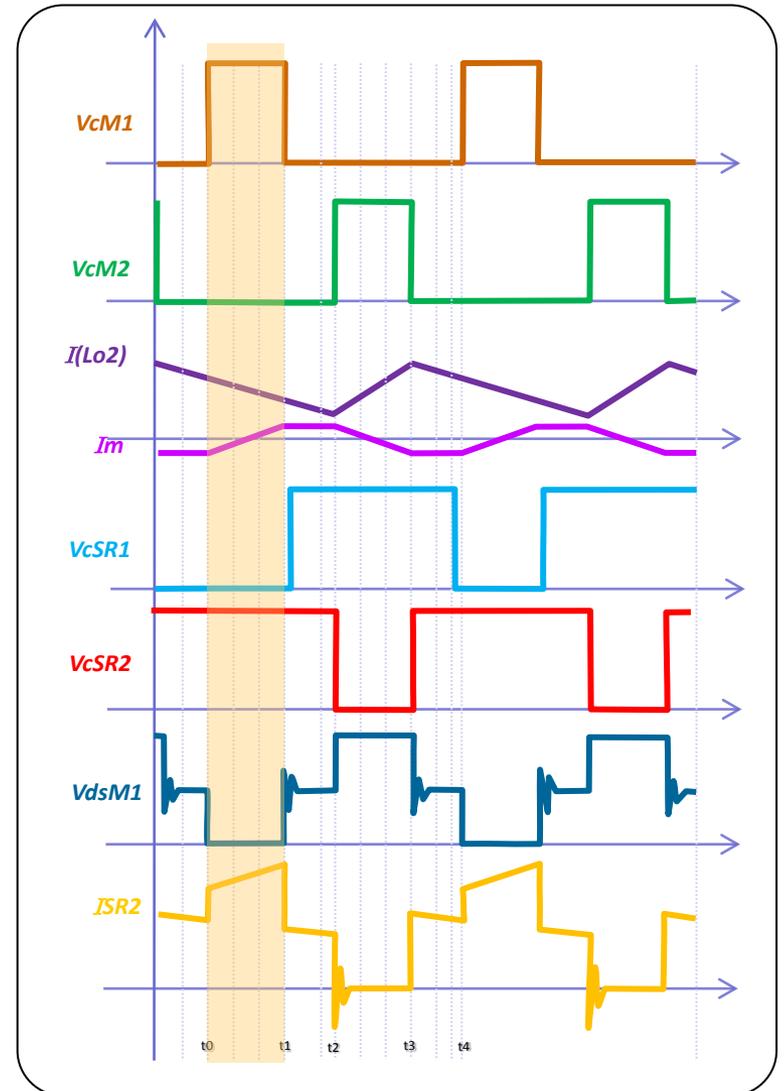
Current Shaping Effect in a Double Ended Converter



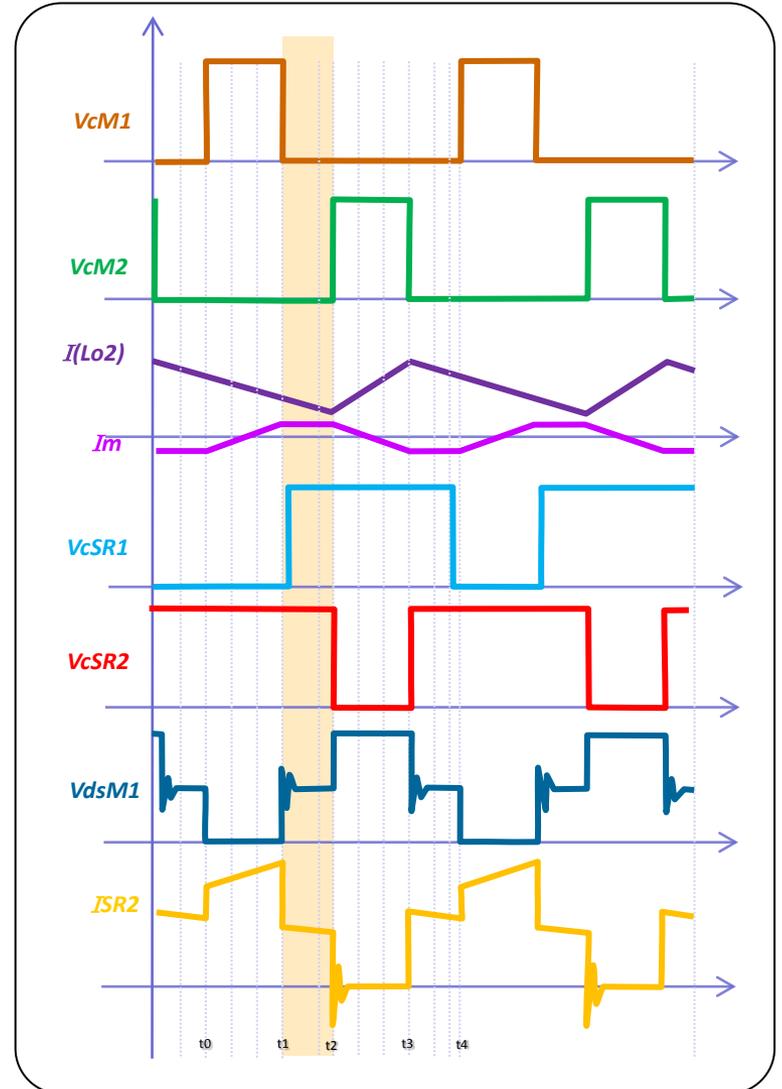
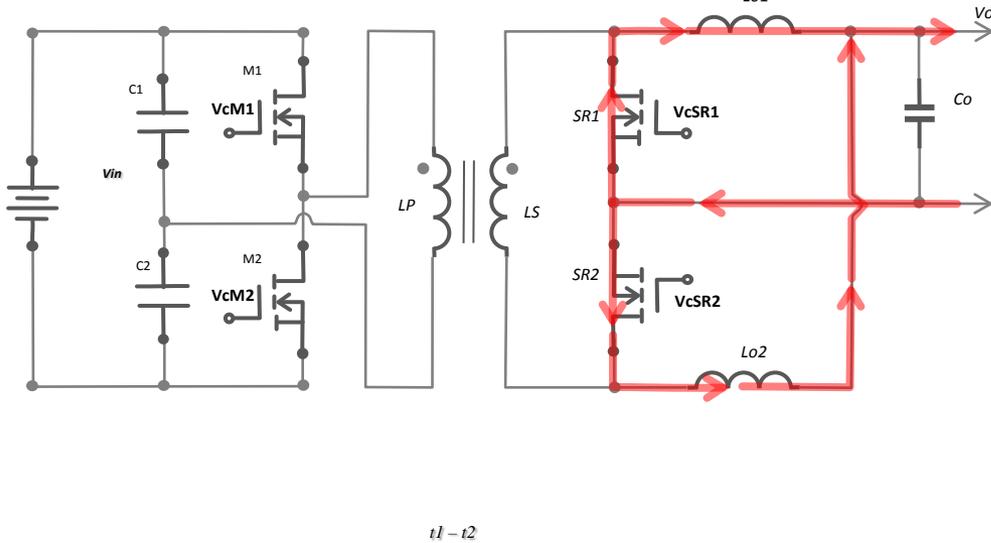
HARD SWITCHING HALF BRIDGE TOPOLOGY



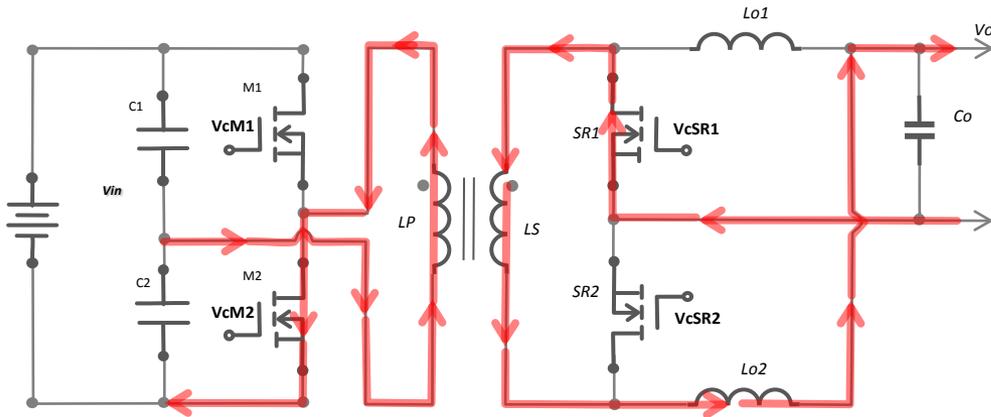
$t_0 - t_1$



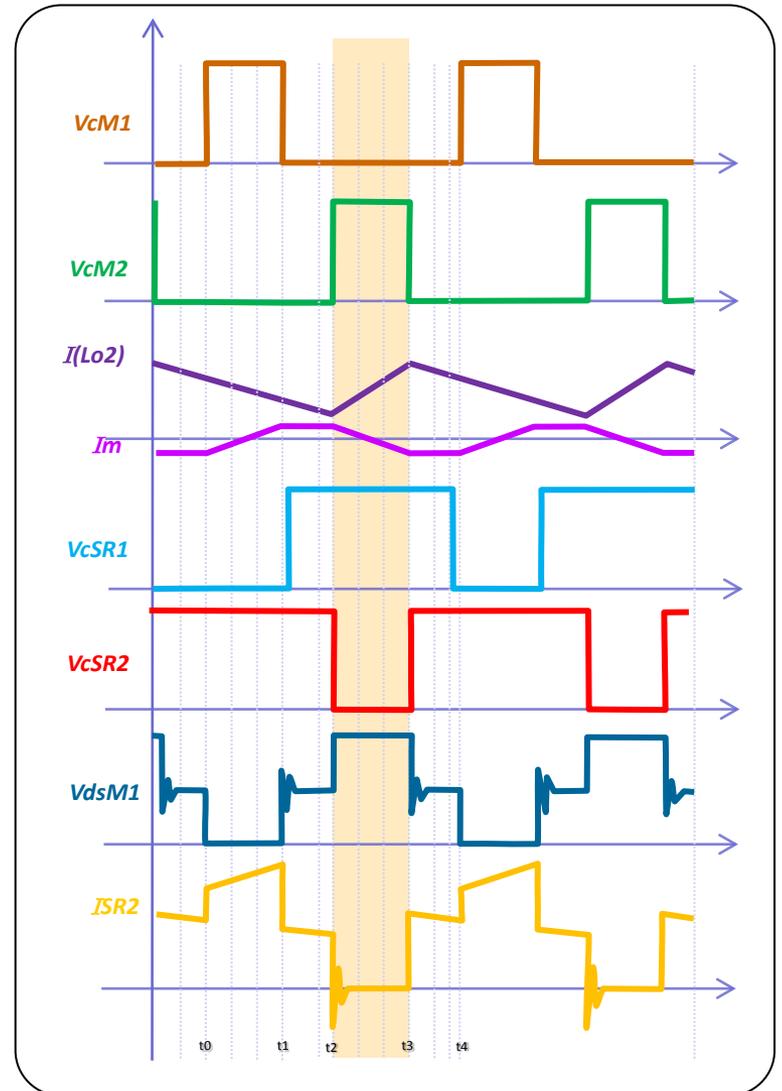
HARD SWITCHING HALF BRIDGE TOPOLOGY



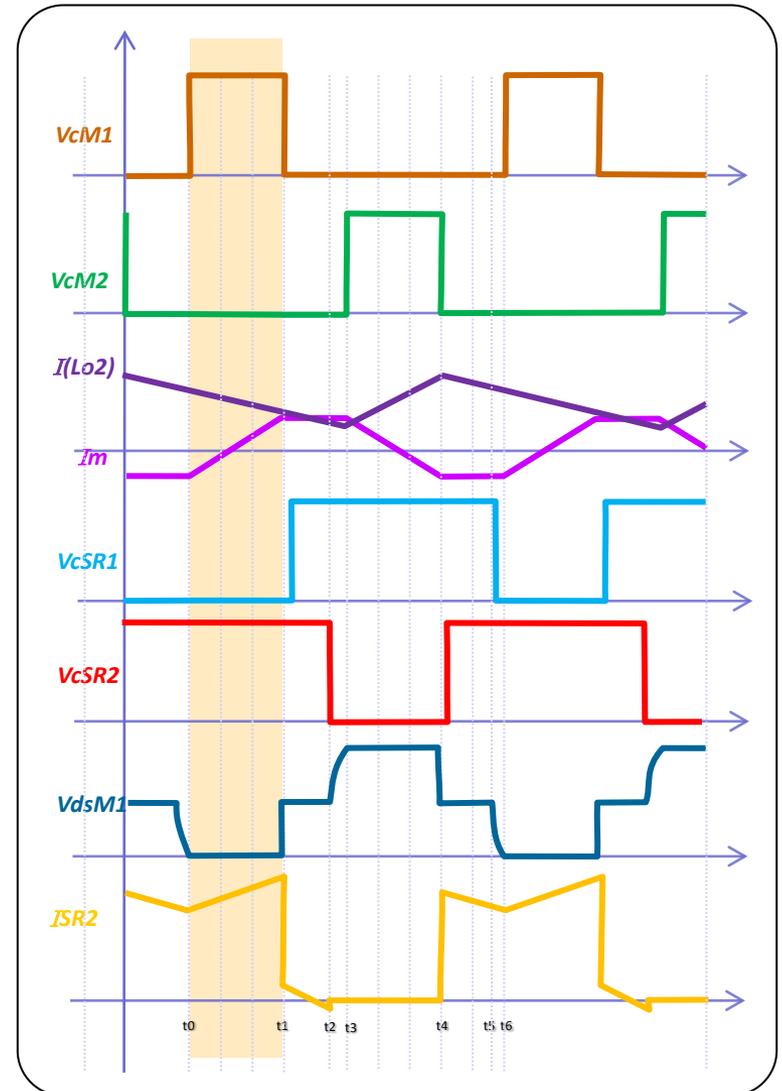
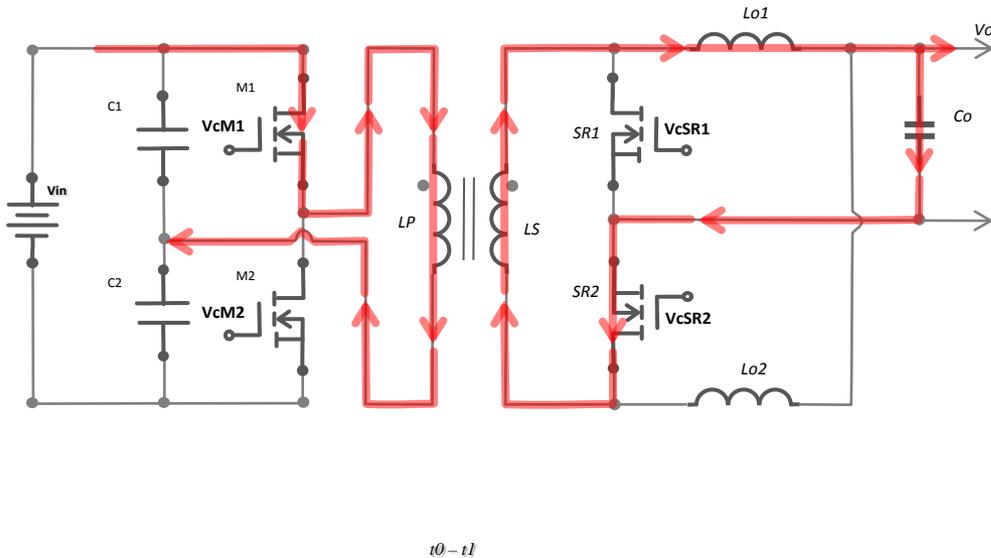
HARD SWITCHING HALF BRIDGE TOPOLOGY



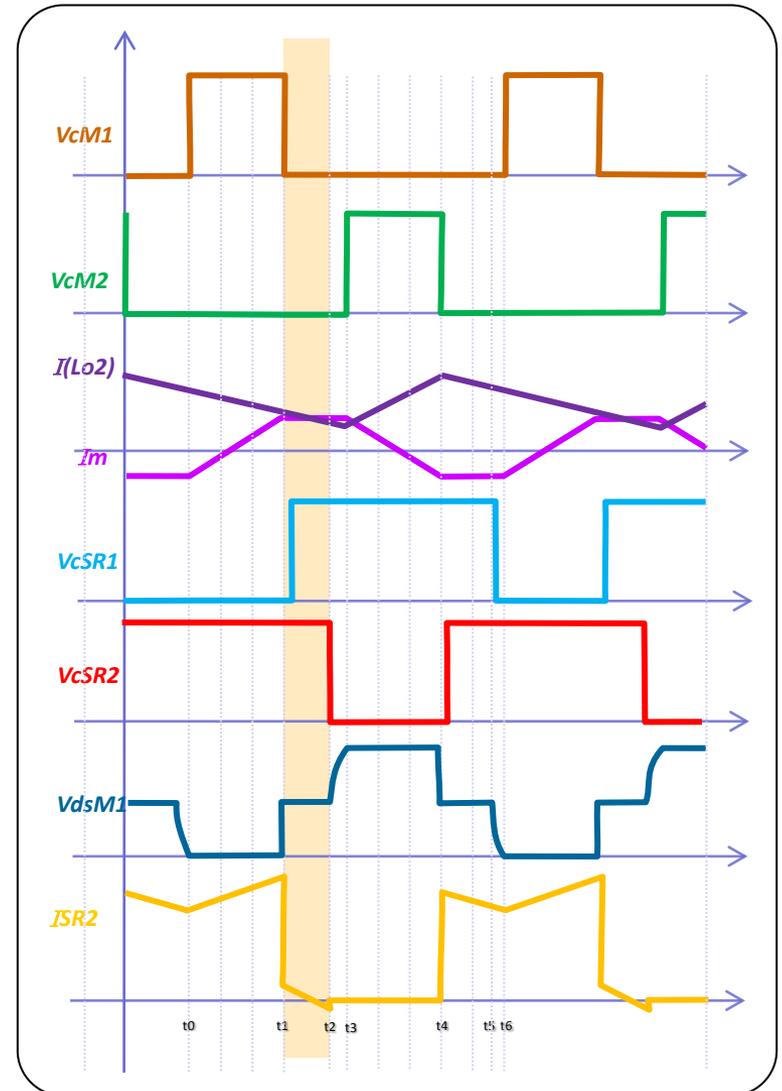
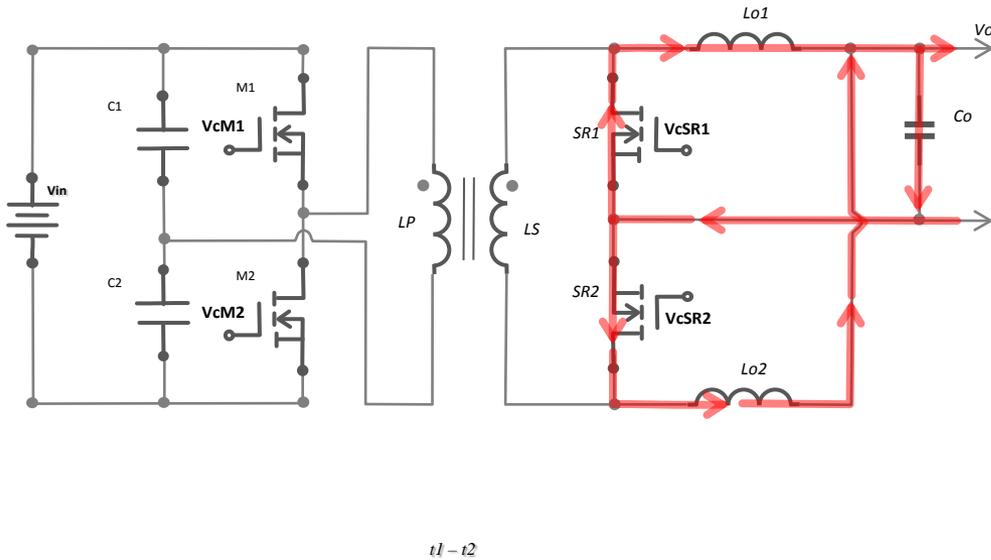
$t_2 - t_3$



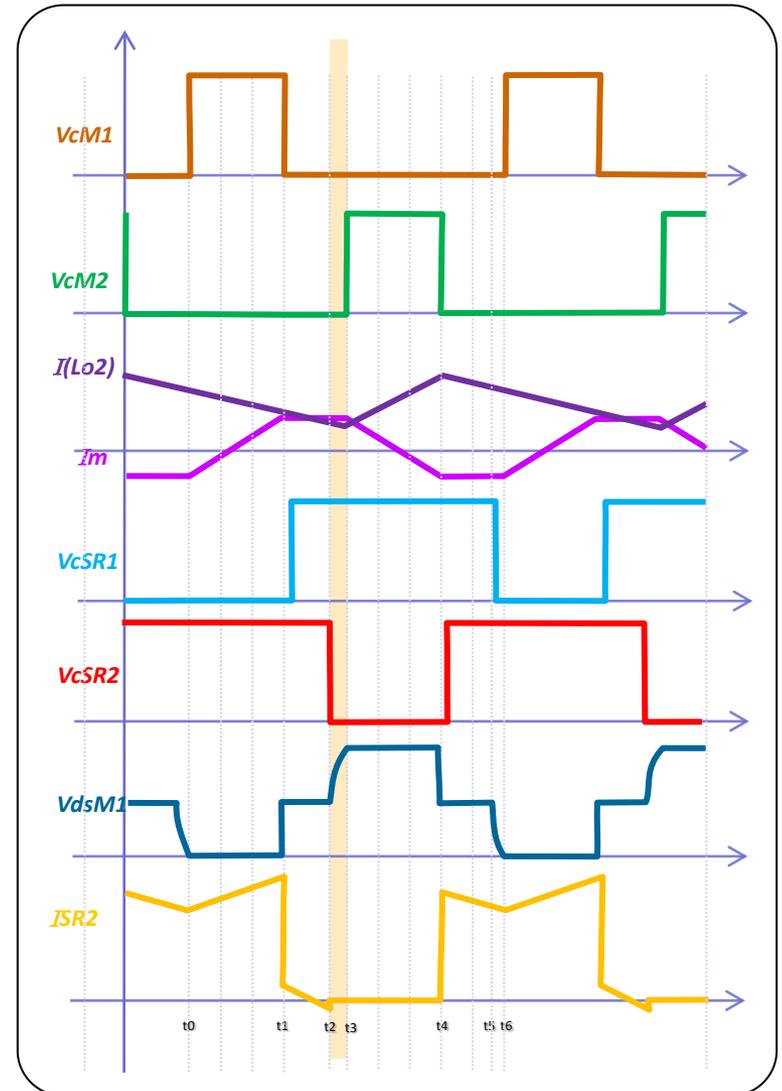
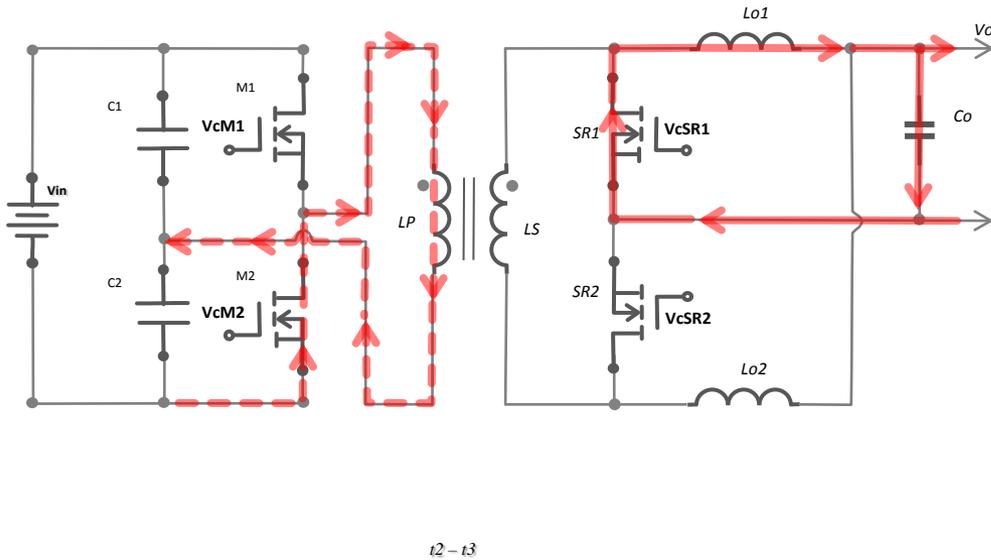
SOFT SWITCHING HALF BRIDGE TOPOLOGY



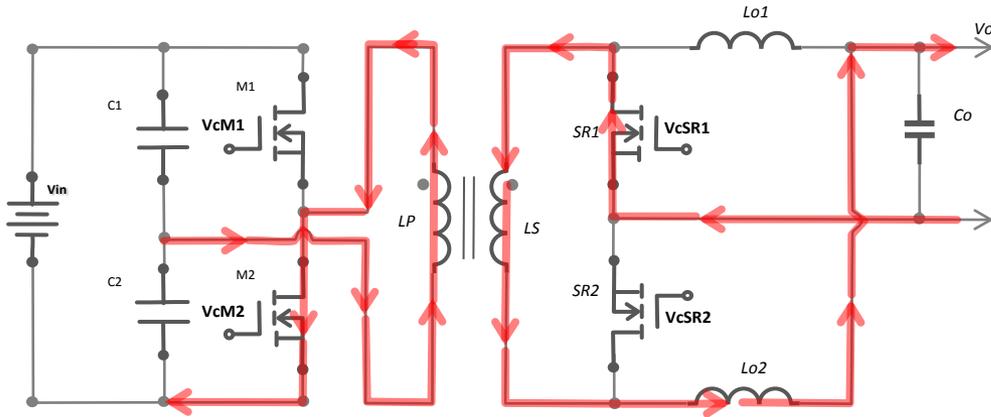
SOFT SWITCHING HALF BRIDGE TOPOLOGY



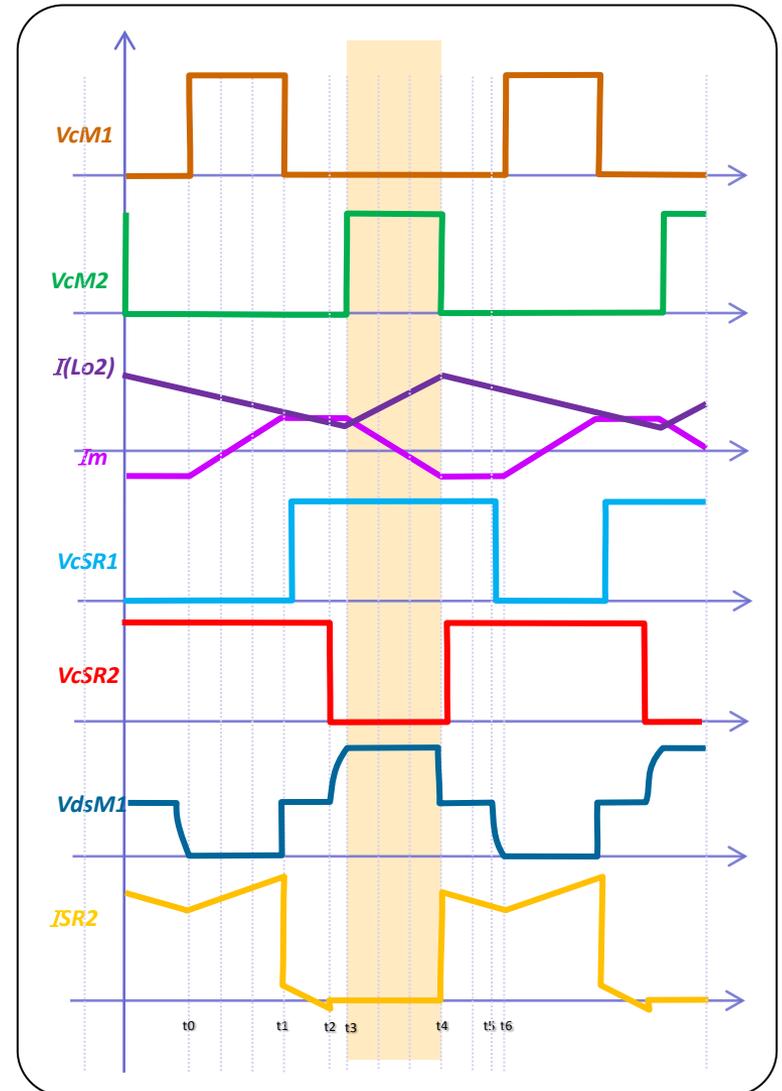
SOFT SWITCHING HALF BRIDGE TOPOLOGY



SOFT SWITCHING HALF BRIDGE TOPOLOGY



$t_3 - t_4$



Experimental Data

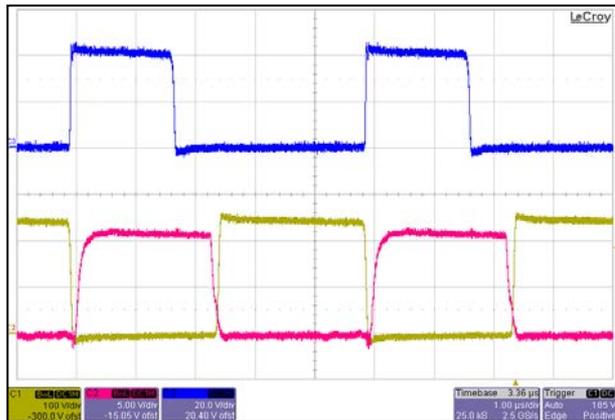


Figure 1: Vin=240V, Iout=15A, Vout=14V
Blue is Syncro Drain, Red is Primary Gate, Yellow is Primary Drain

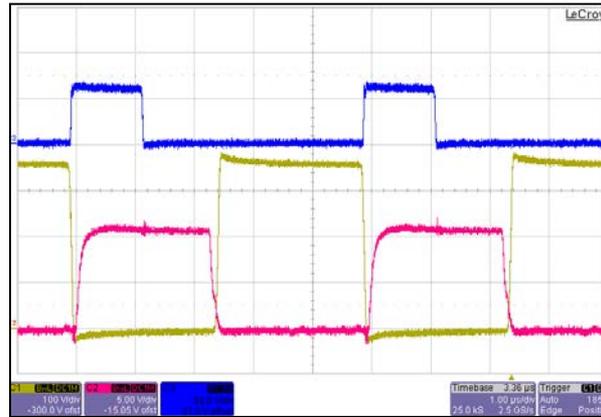


Figure 2: Vin=345V, Iout=90A, Vout=14V
Blue is Syncro Drain, Red is Primary Gate, Yellow is Primary Drain

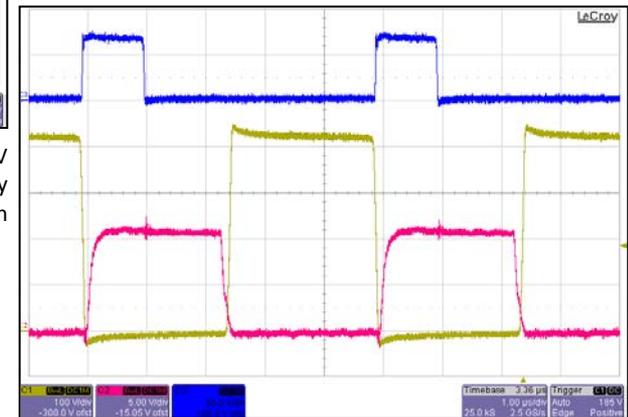


Figure 3: Vin=405V, Iout=120A, Vout=14V
Blue is Syncro Drain, Red is Primary Gate, Yellow is Primary Drain

[8]

FUTURE TRENDS

- “True” Soft Switching topologies suitable for frequency range from 250Khz to 1Mhz will be the preferred choice
- Resonant topologies such as LLC will maintain popularity due to the “idealization” of the switching devices.
- “True” soft switching topologies through sizing and control have the advantage of simplicity, low cost and in most of applications better efficiency than resonant topologies.

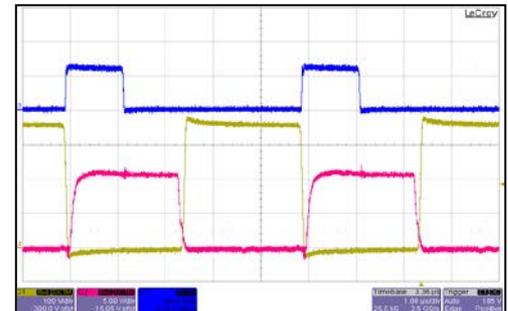
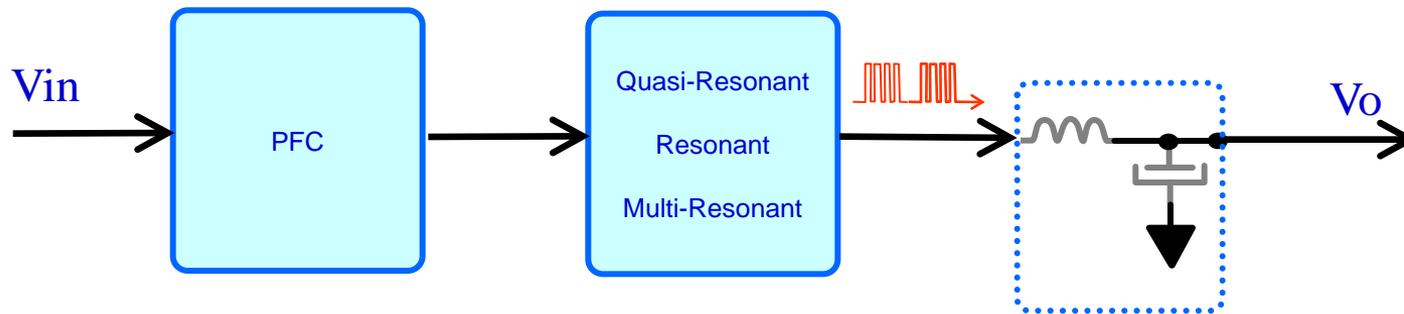


Figure 2: $V_{in}=345V$, $I_{out}=90A$, $V_{out}=14V$
Blue is Syncro Drain, Red is Primary Gate, Yellow is Primary Drain

FUTURE TRENDS...

- In the future the topology may be a Soft Switching Cell operating at Z.V.S at turn on and Z.C.S at turn off. The operating frequency may be very high in Mhz range.

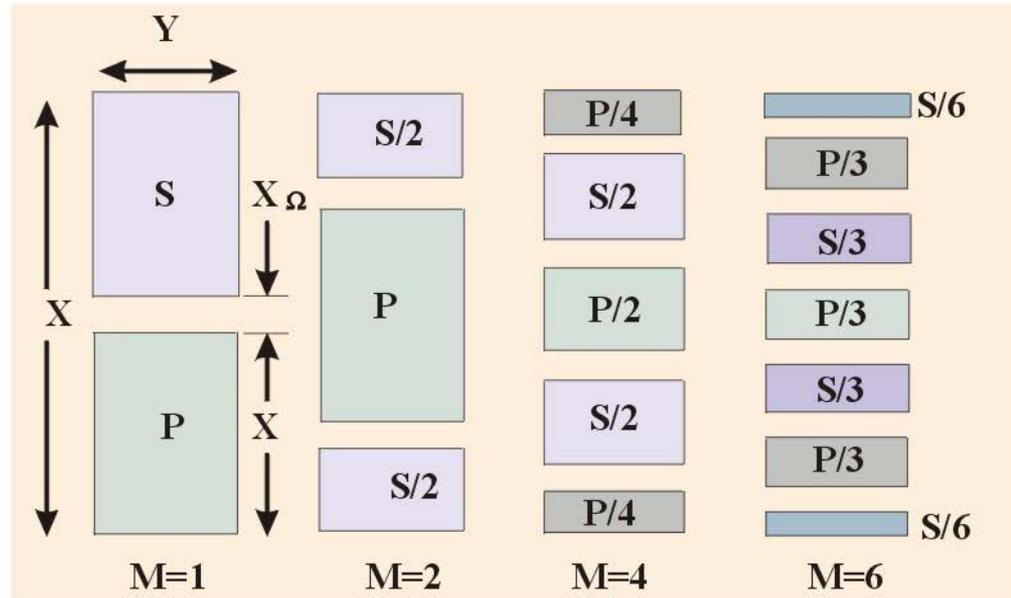
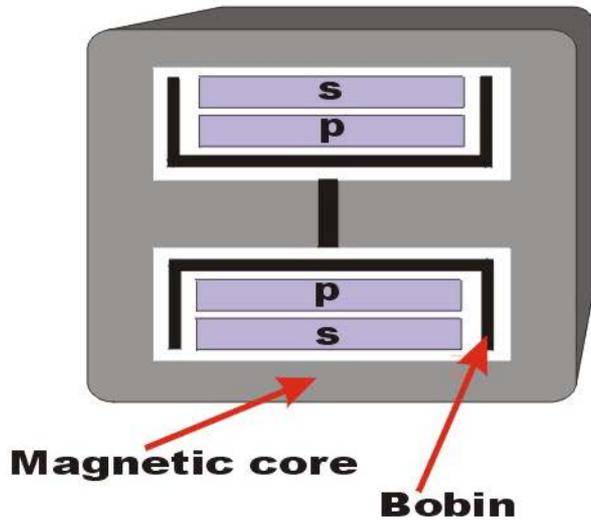


- The regulation may be done in train of pulses with a frequency in hundreds of KHz range. The PWM regulation is the same, the difference is that during the “on” time energy will be delivered at very high frequency.

PRESENT MAGNETIC LIMITATIONS

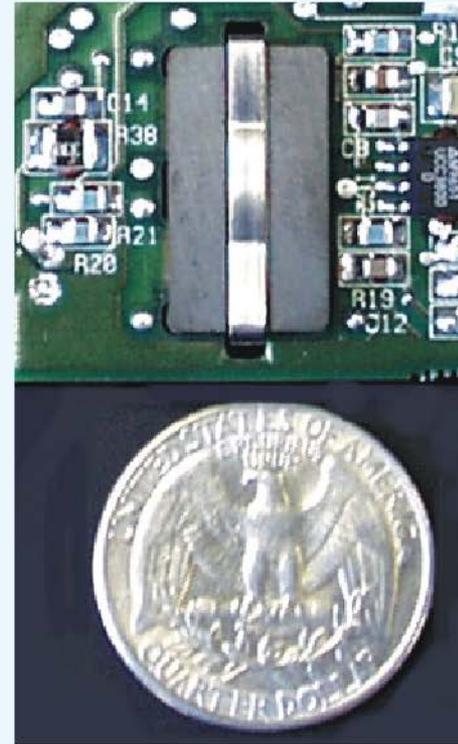
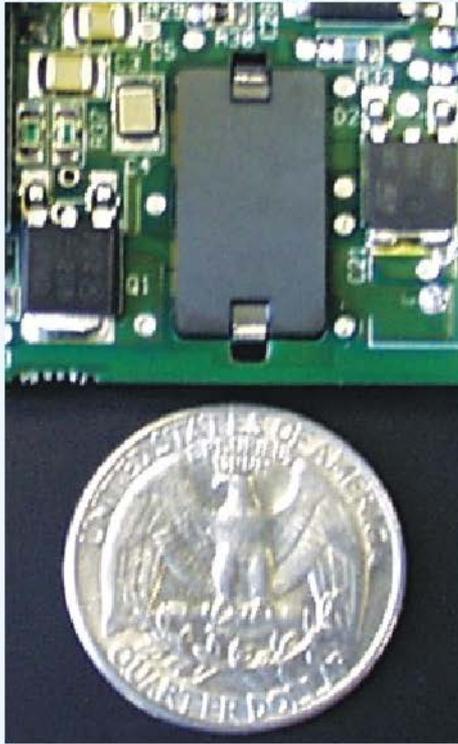
LEAKAGE & STRAY INDUCTANCE

HOW TO MINIMIZE THE LEAKAGE INDUCTANCE

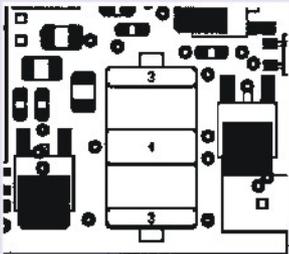


$$L_{lek} = 4 \cdot \pi \cdot 10^{-4} \frac{N^2 l w}{M^2 Y} \left(\frac{\sum x}{3} + \sum x \Delta \right)$$

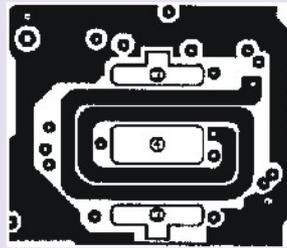
TOP AND BOTTOM LAYERS OF THE 25W DC-DC FLYBACK CONVERTER



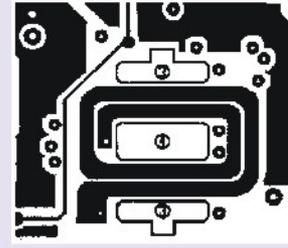
IMPLEMENTATION OF THE 25W DC-DC FLYBACK CONVERTER



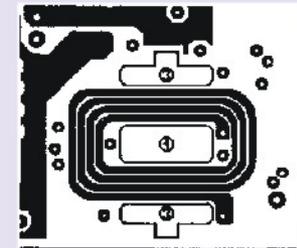
Layer 1: Components



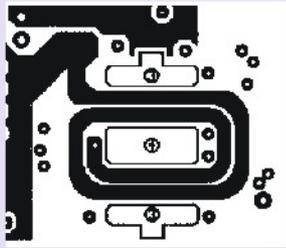
Layer 2: Secondary



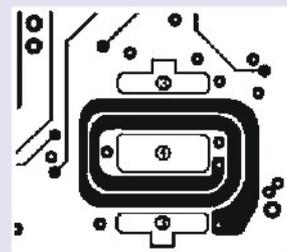
Layer 3: Primary



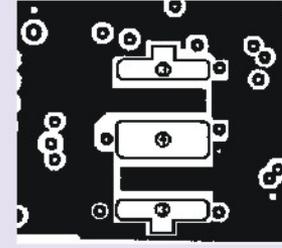
Layer 4: Secondary



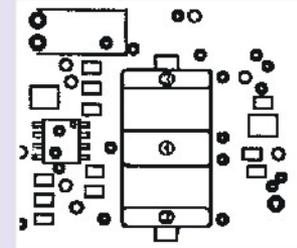
Layer 5: Primary



Layer 6: Secondary

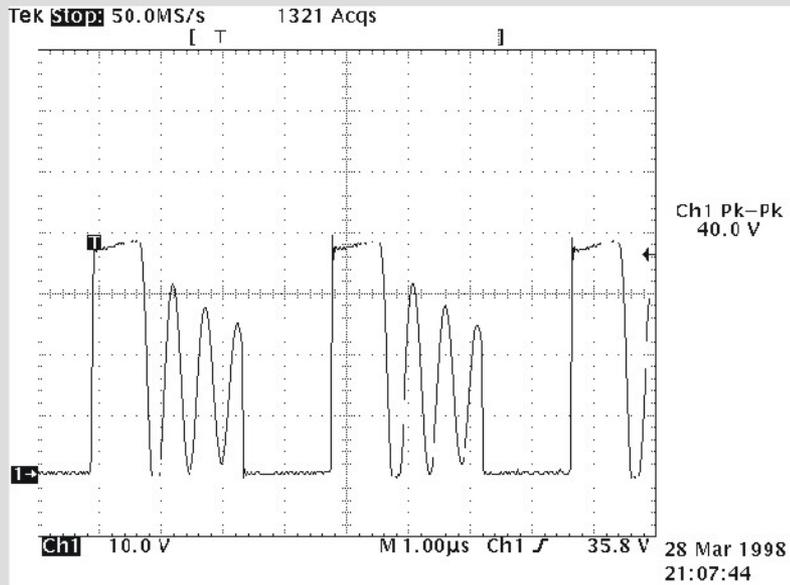


Layer 7: Shield

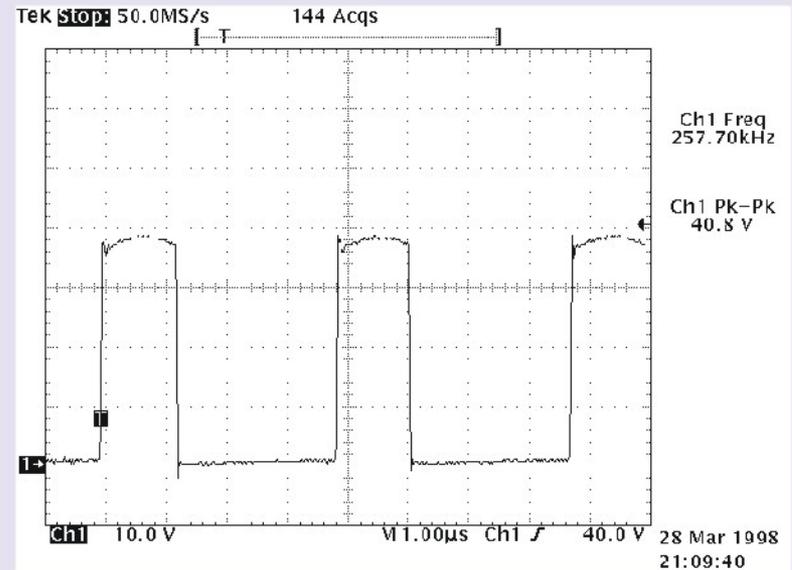


Layer 8: Components

EXPERIMENTAL WAVE FORMS OF THE 25W DC-DC FLYBACK CONVERTER

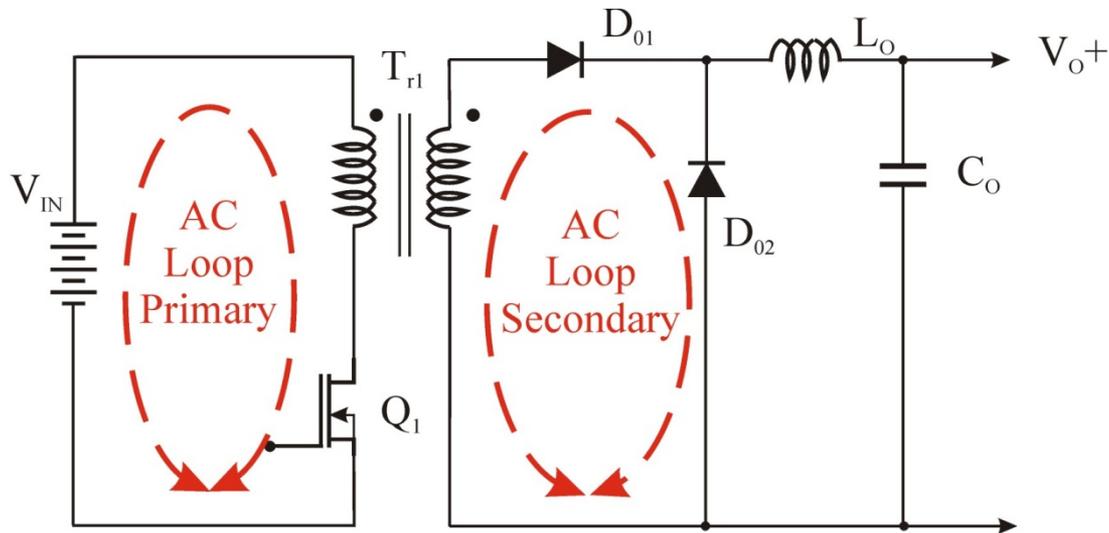


Voltage across Q1
 $V_{in} = 13.7V$
 $I_o = 0.2A$



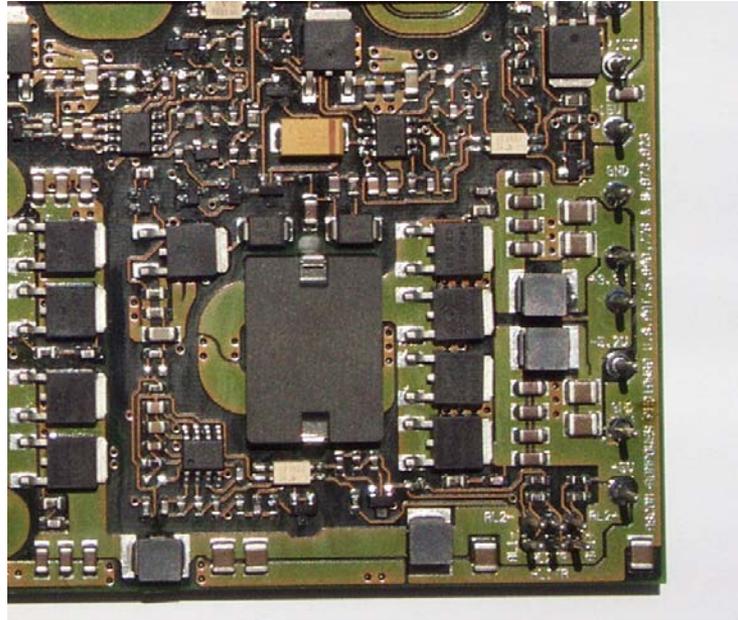
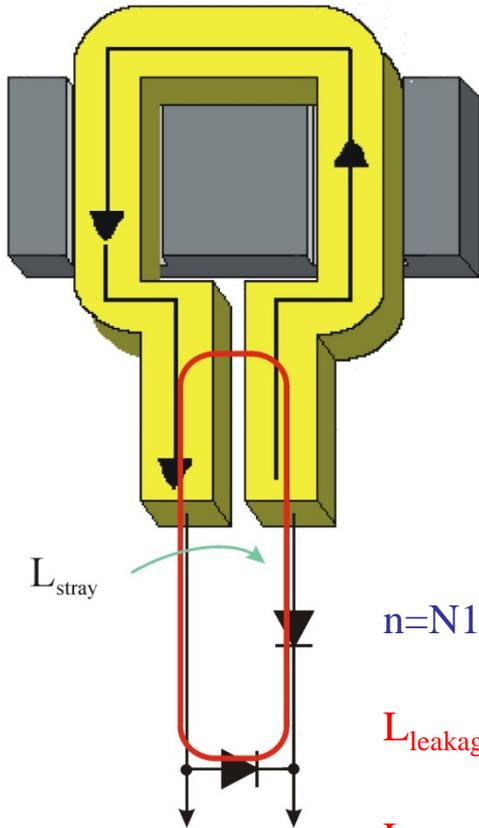
Voltage across Q1
 $V_{in} = 13.7V$
 $I_o = 0.6A$

STRAY INDUCTANCE



- THE STRAY INDUCTANCE ASSOCIATED WITH THE AC LOOP, PLAY A VERY IMPORTANT ROLE IN THE CONVERTER PERFORMANCE.
- THE EFFECT OF THE STRAY INDUCTANCE CAN BE STRONGER THAN THE EFFECT OF LEAKAGE INDUCTANCE.

THE IMPACT OF THE STRAY INDUCTANCE



$$n = N_1/N_2 = 8:1$$

$$L_{\text{leakage}} = 0.63 \mu\text{H}$$

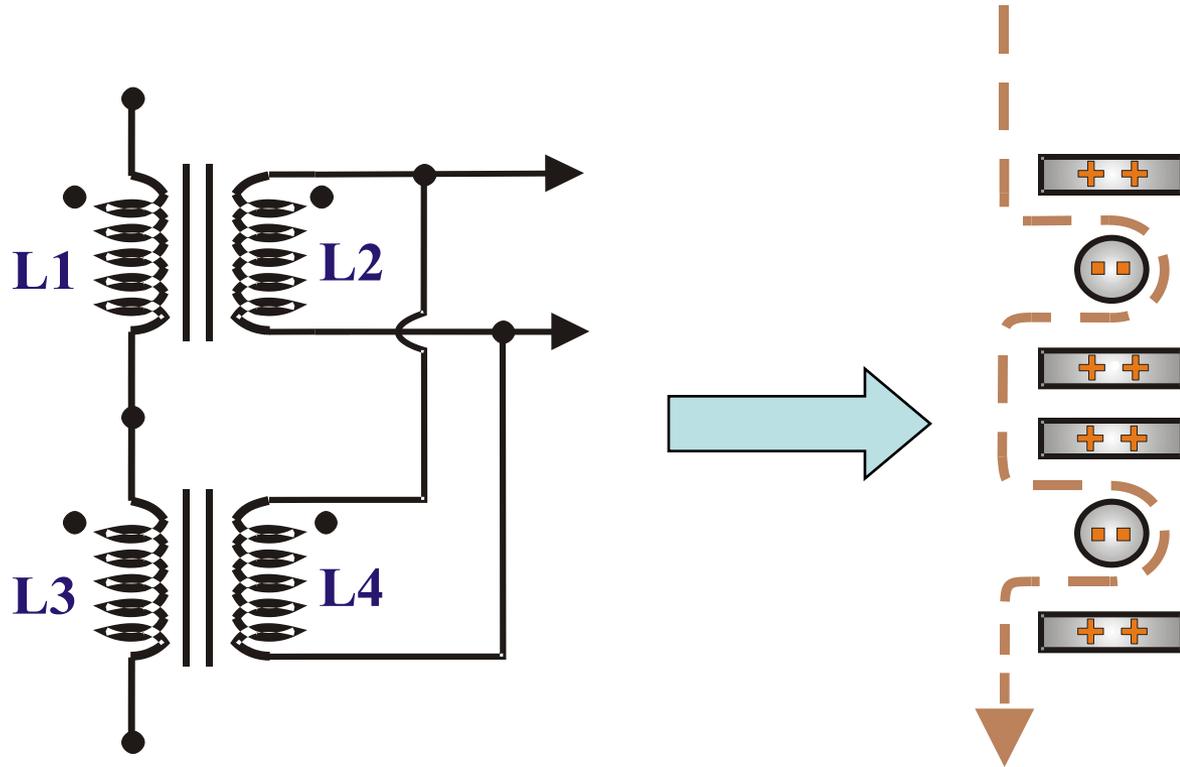
$$L_{\text{Stray}} = 0.0088 \mu\text{H}$$

$$L_{\text{leakage_total}} = L_{\text{leakage}} + n^2 * L_{\text{Stray}}$$

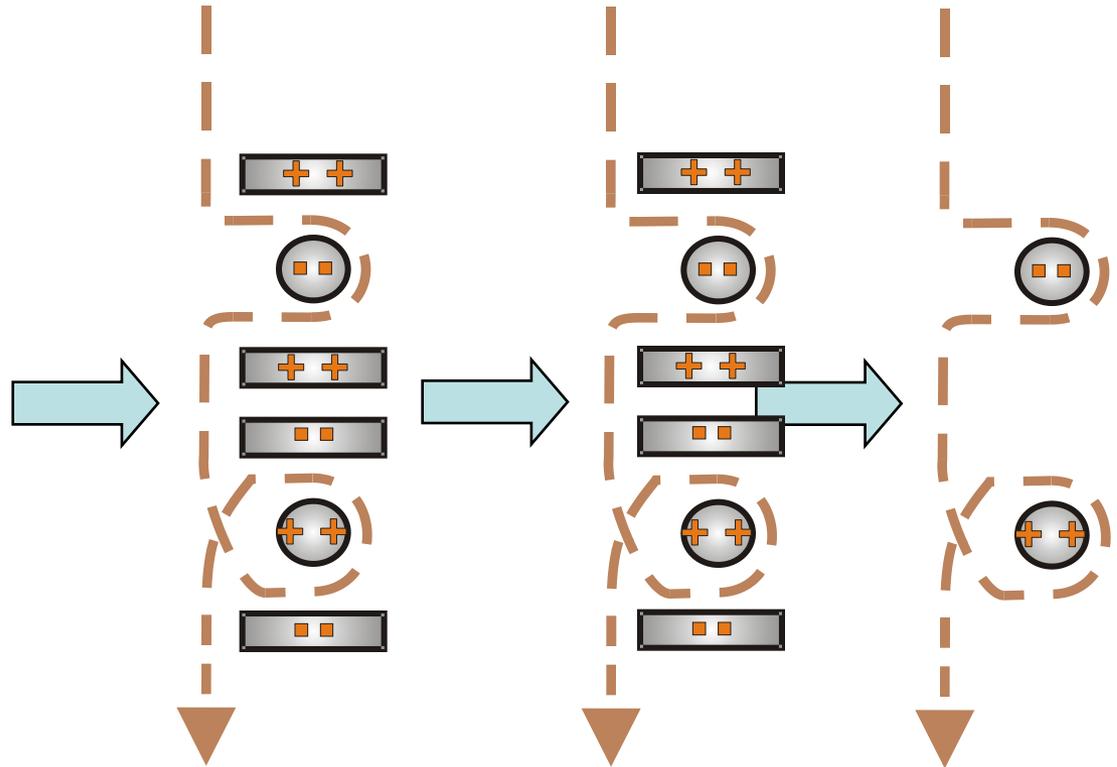
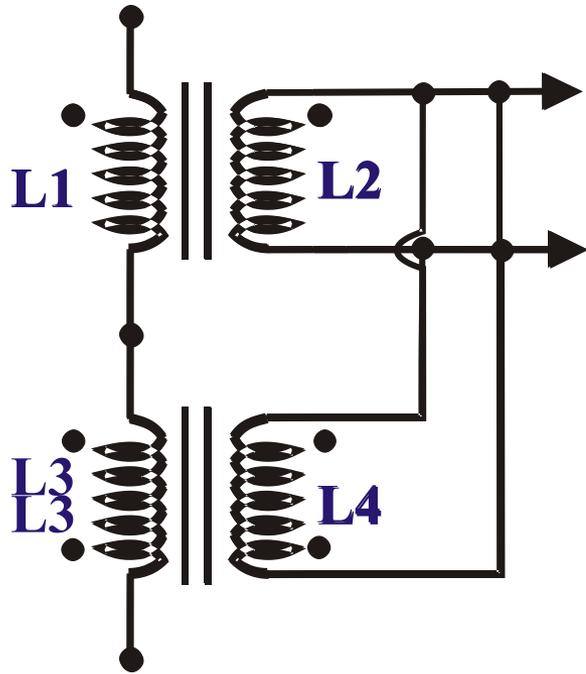
$$L_{\text{leakage_total}} = 1.2 \mu\text{H}$$

**MAGNETIC
OPTIMIZATION AND
ELIMINATION OF THE
END EFFECTS**

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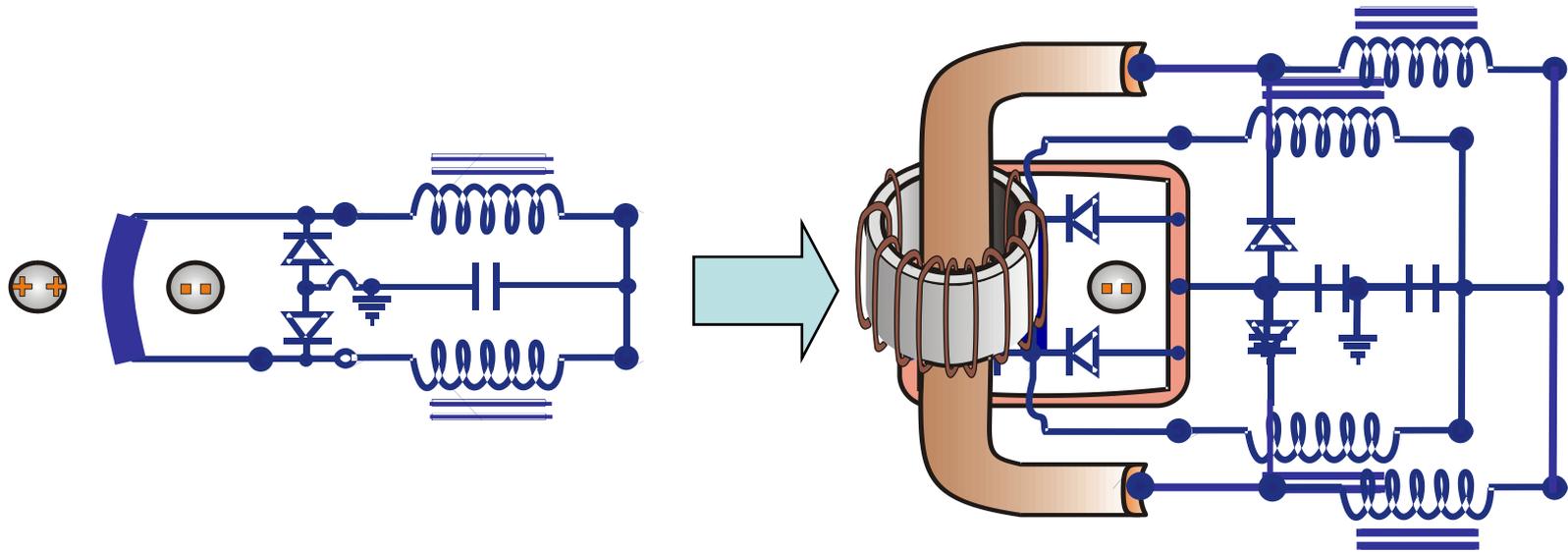


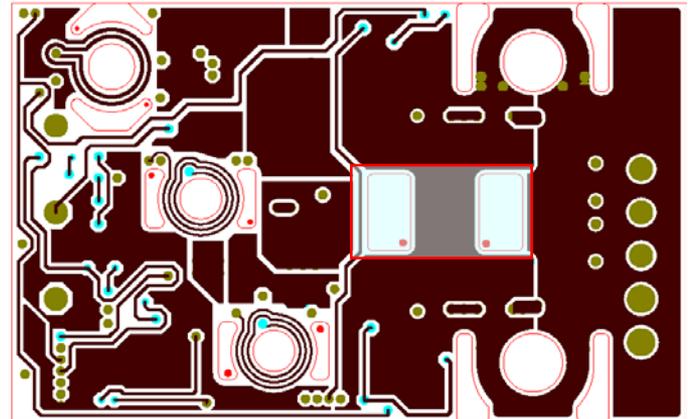
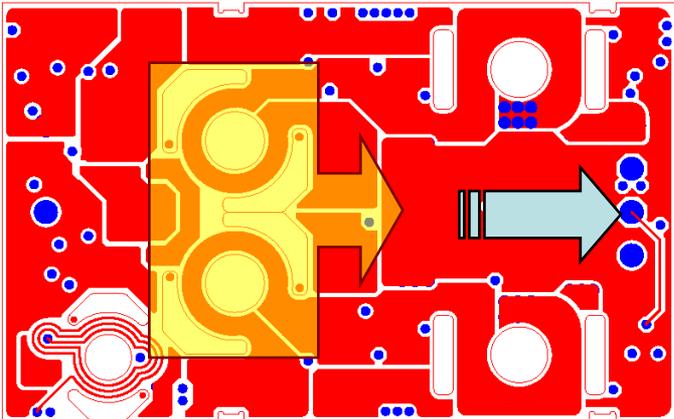
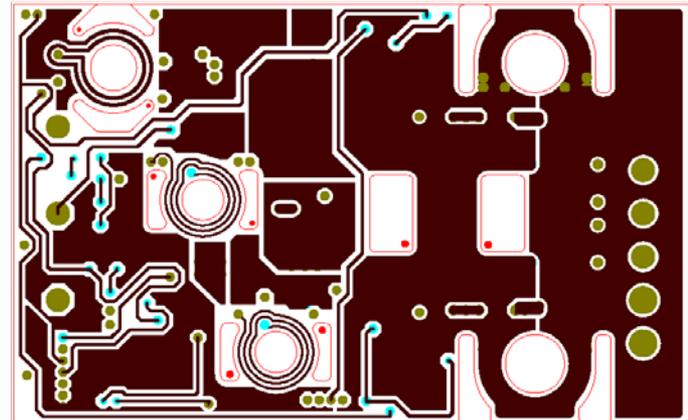
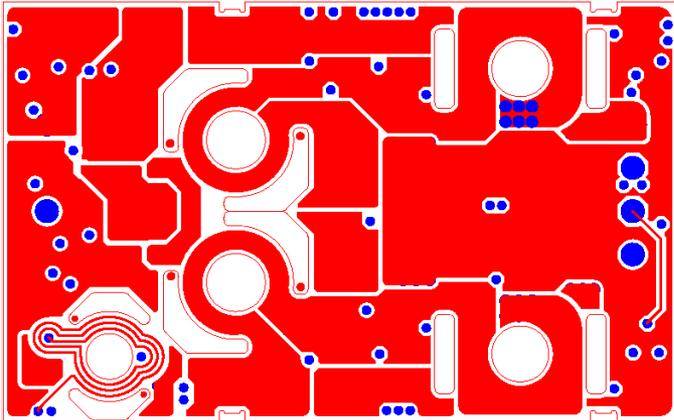
Rompower



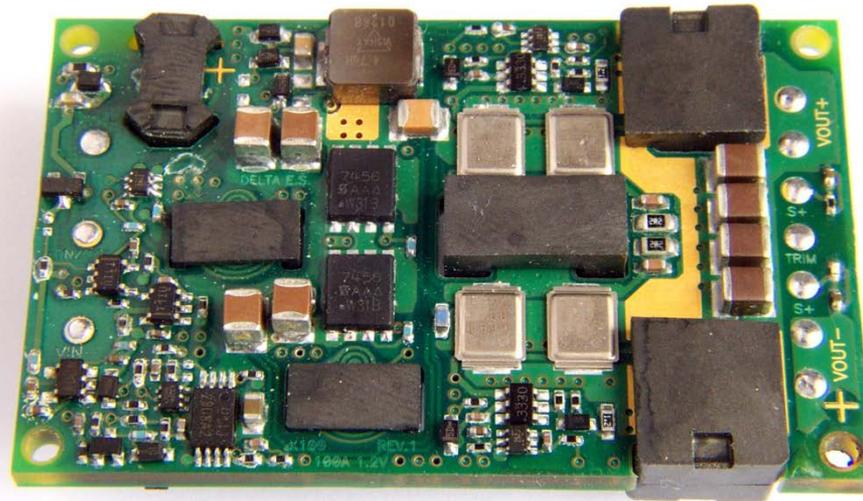
- Significant reduction of the footprint
- Reduction of the magnetic core volume

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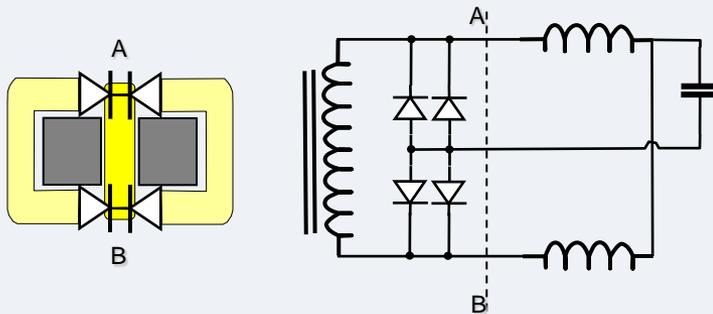
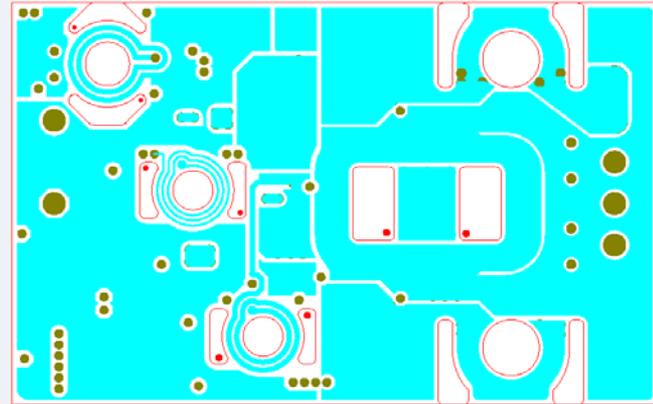
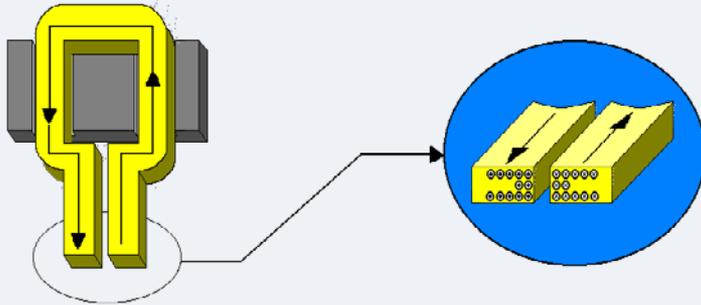




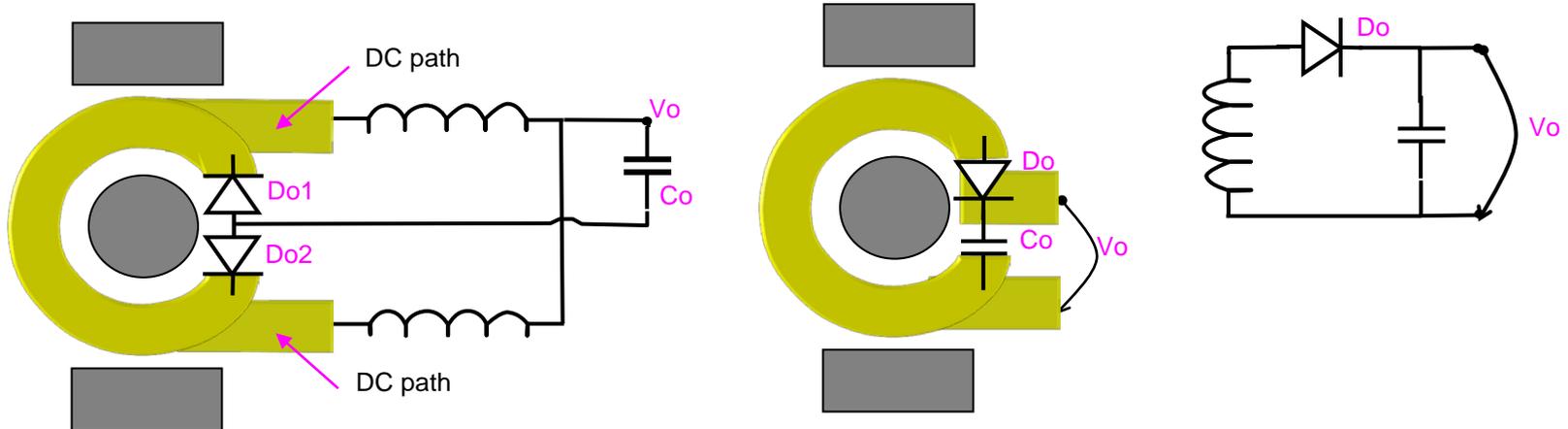
1V2/100A HC_QB



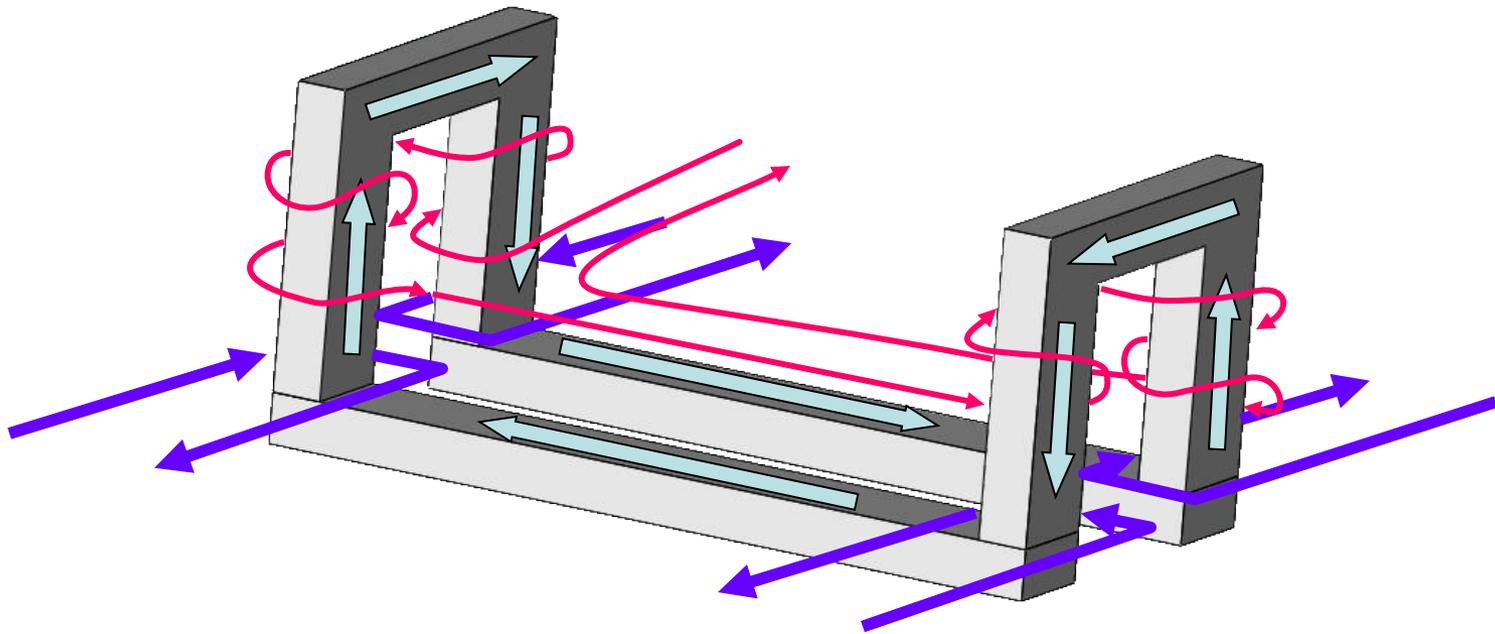
Winding Termination Effects



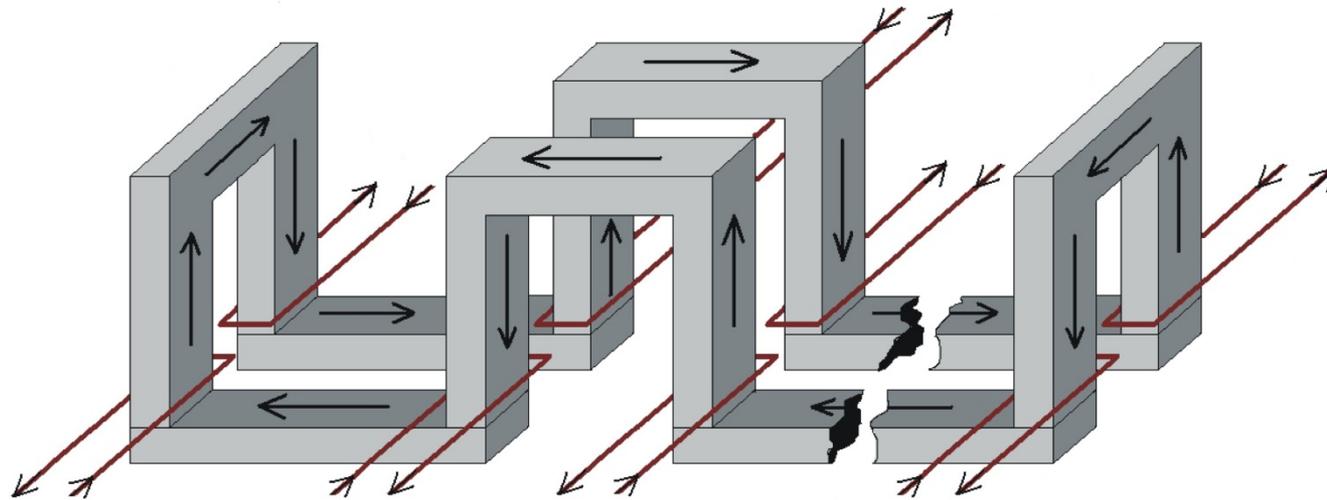
Winding Termination Effects

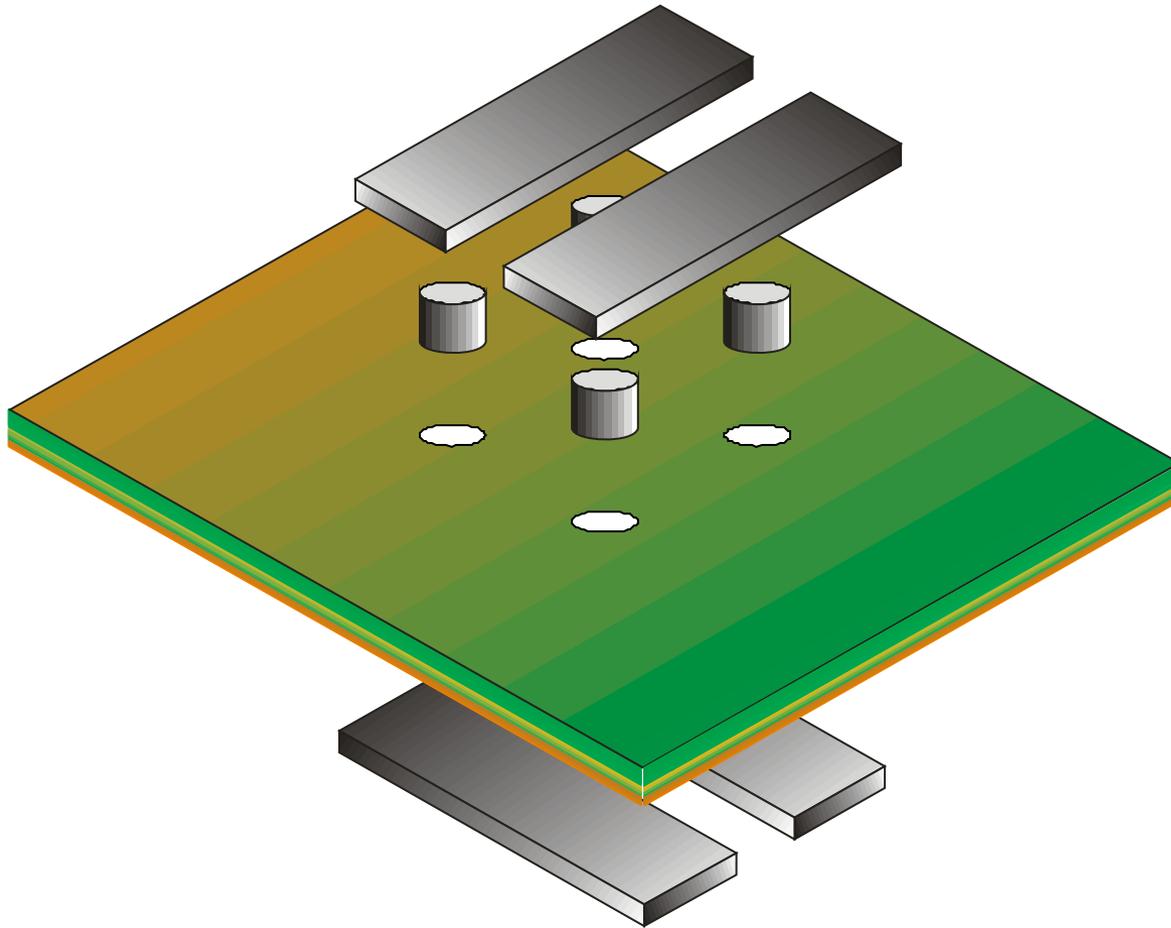


NEW FORM OF DISTRIBUTED MAGNETICS



“N” WINDINGS CONCEPT 1/N TURNS

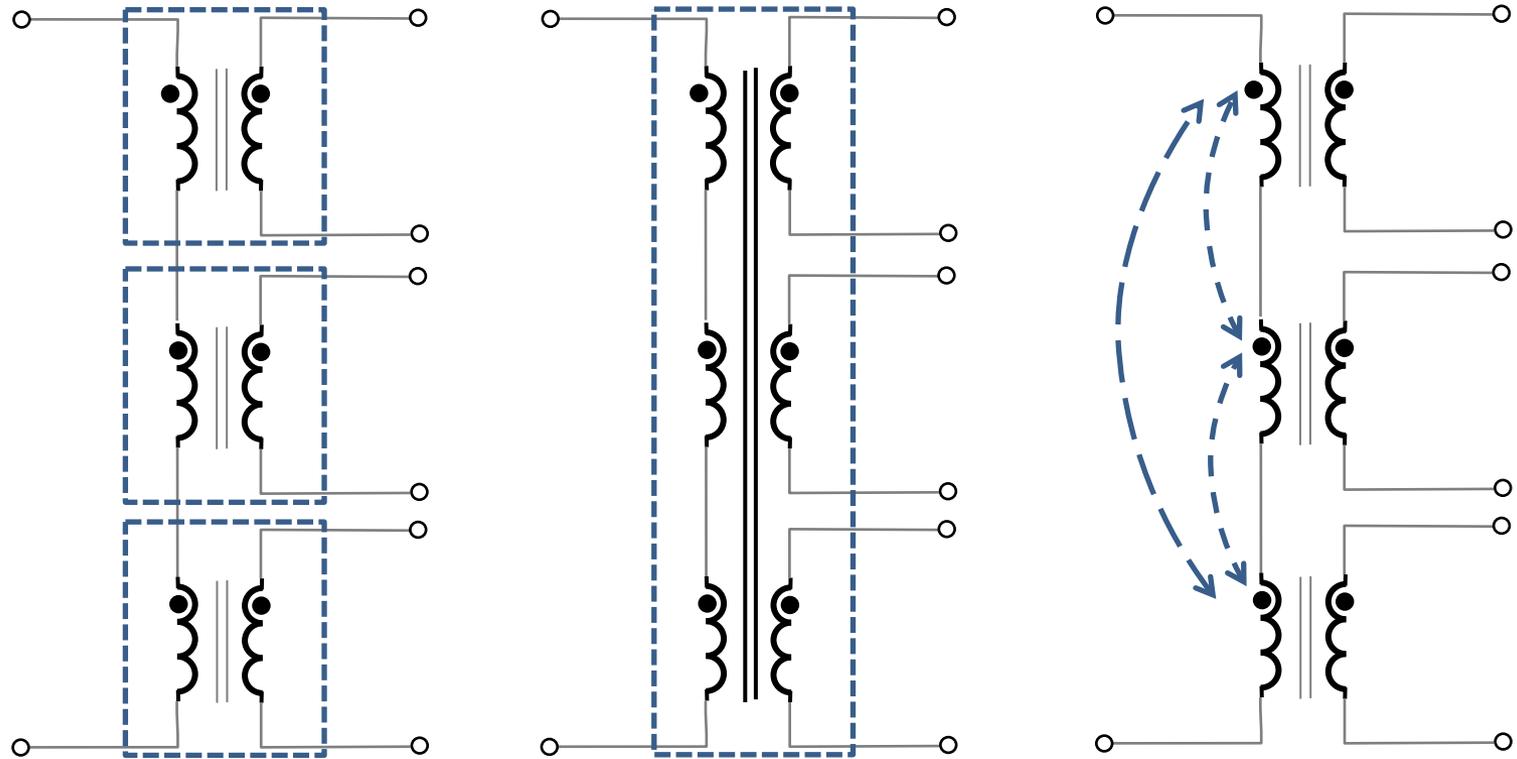




NEW FORM OF DISTRIBUTED MAGNETIC

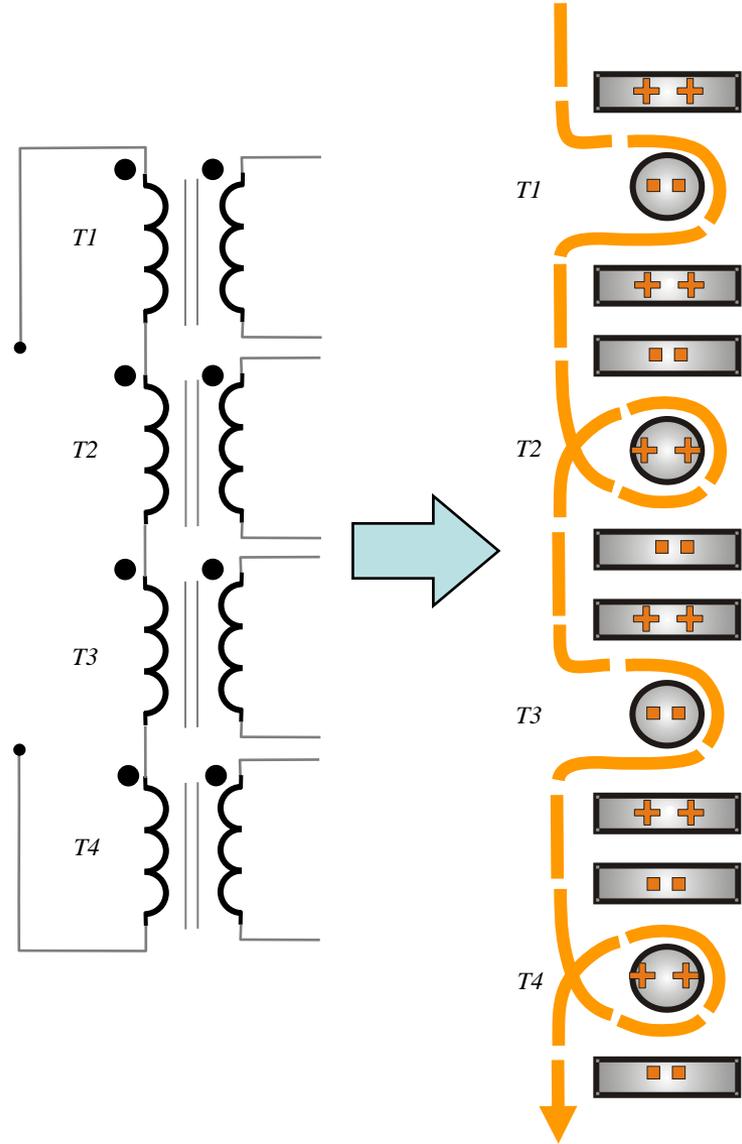
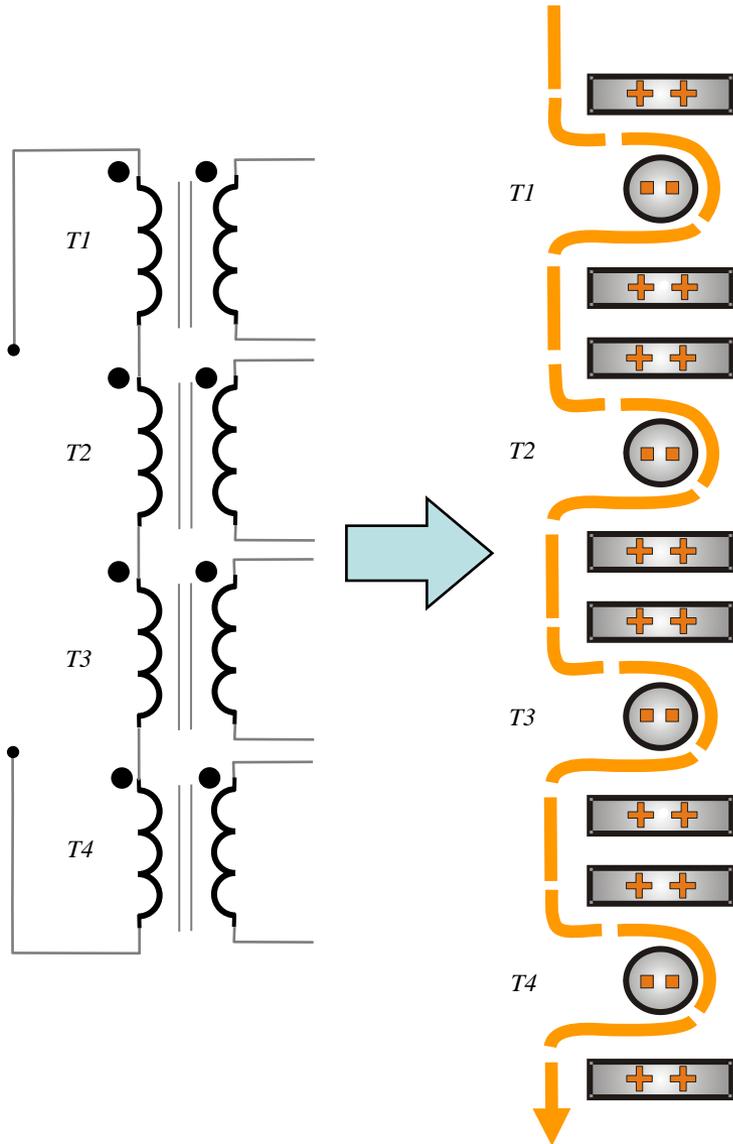
[3]

ELECTRICAL EQUIVALENCY



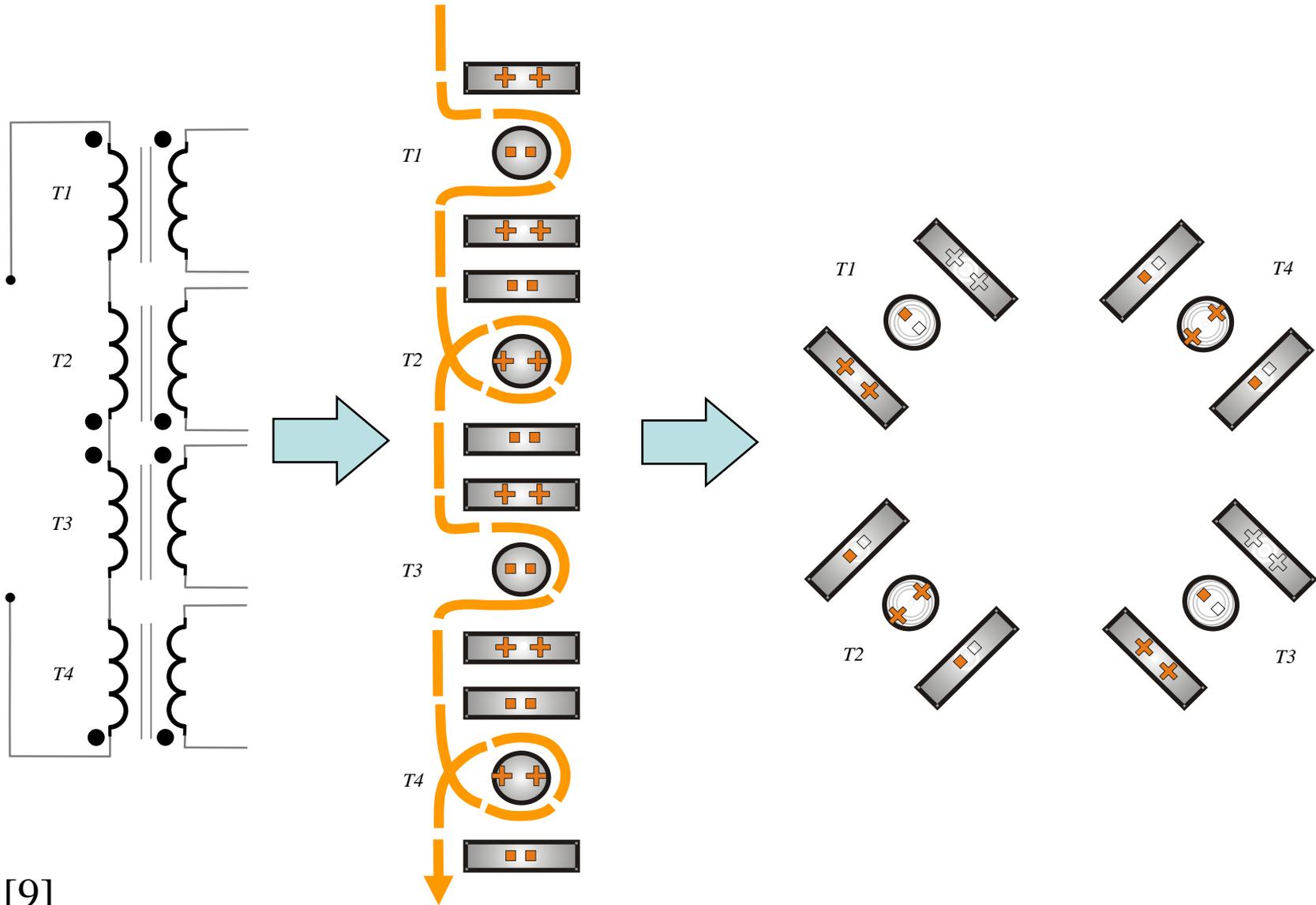
Magnetic Distribution Techniques

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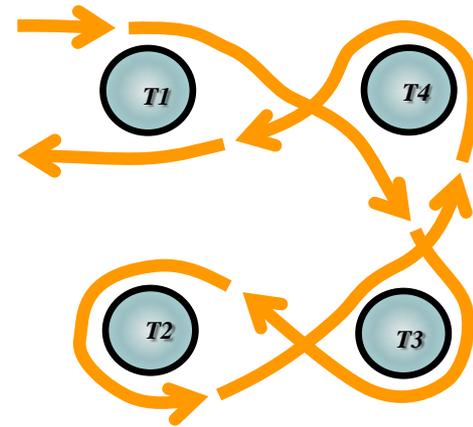
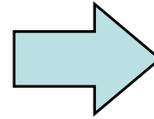
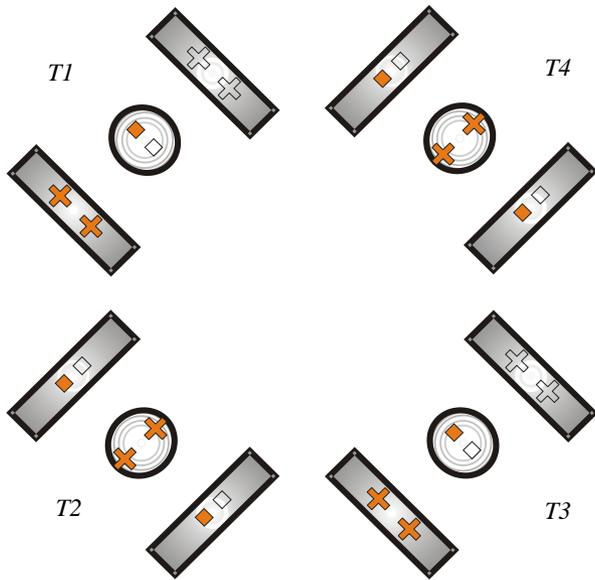


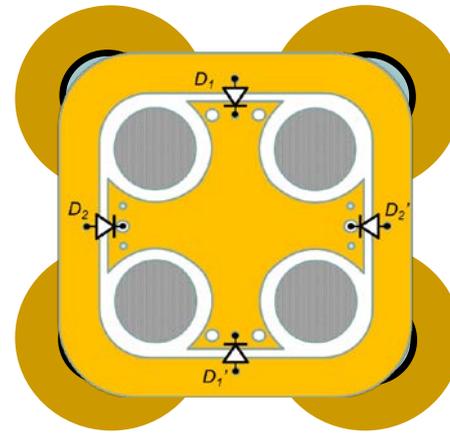
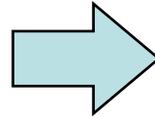
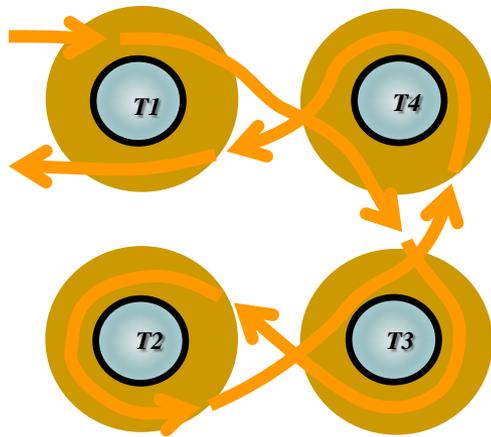
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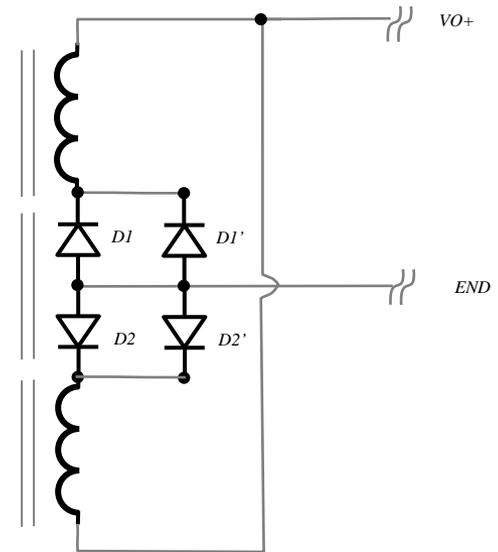
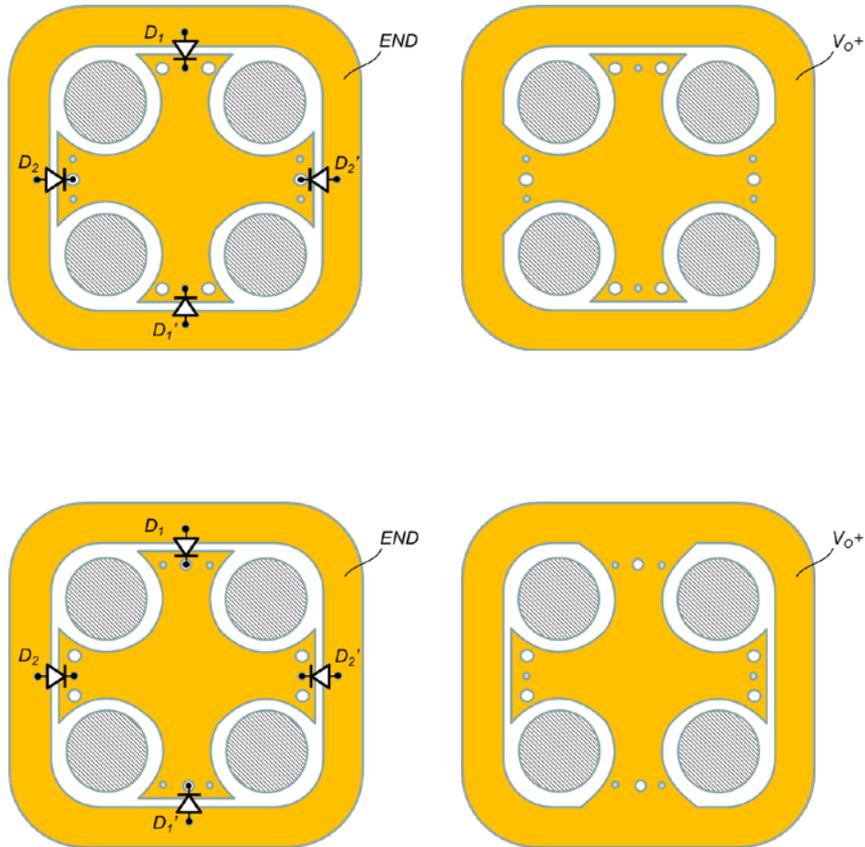
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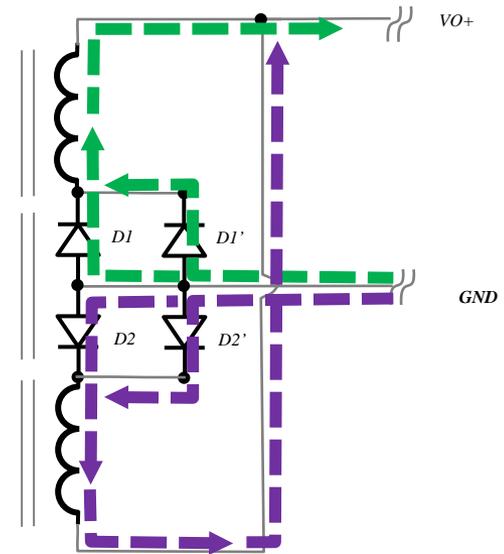
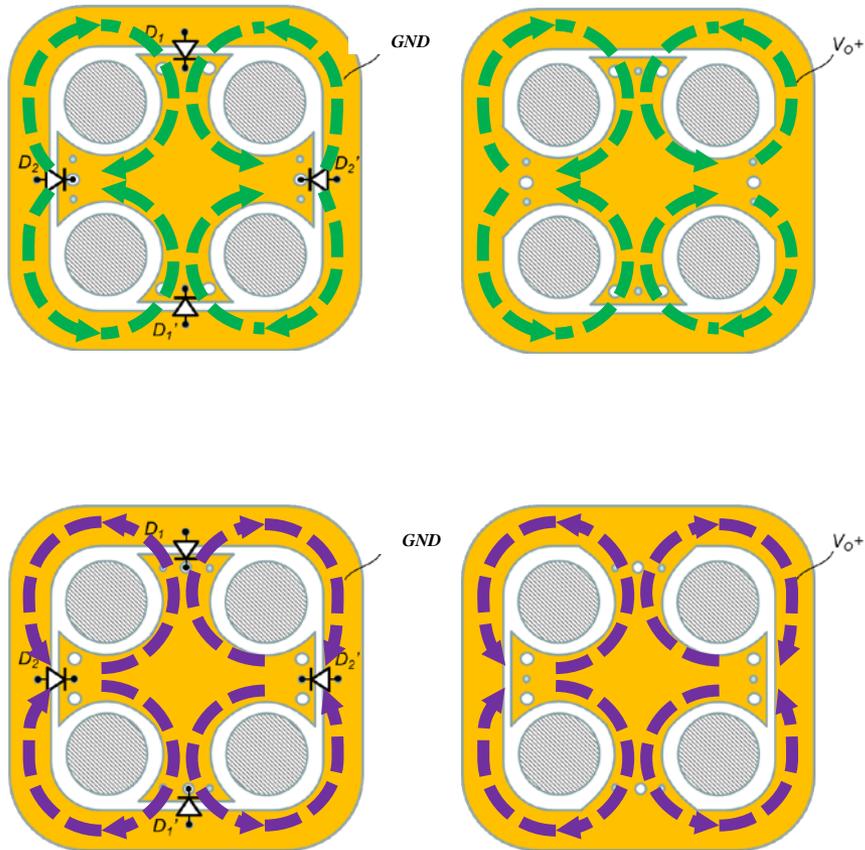


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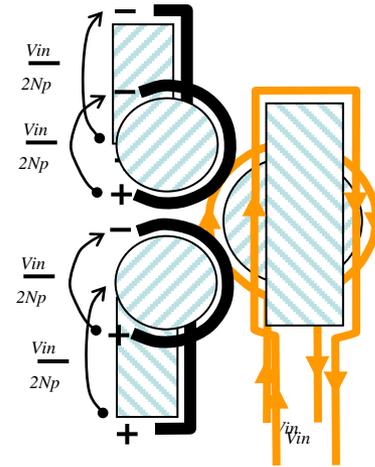
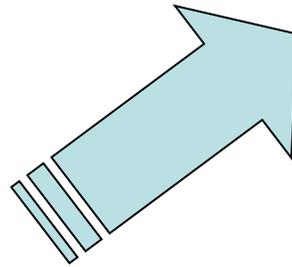
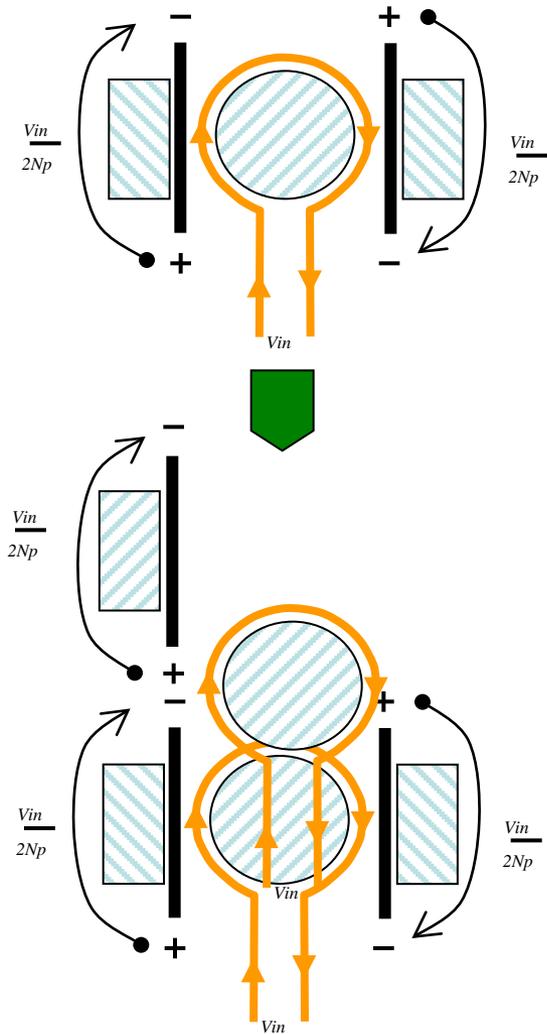






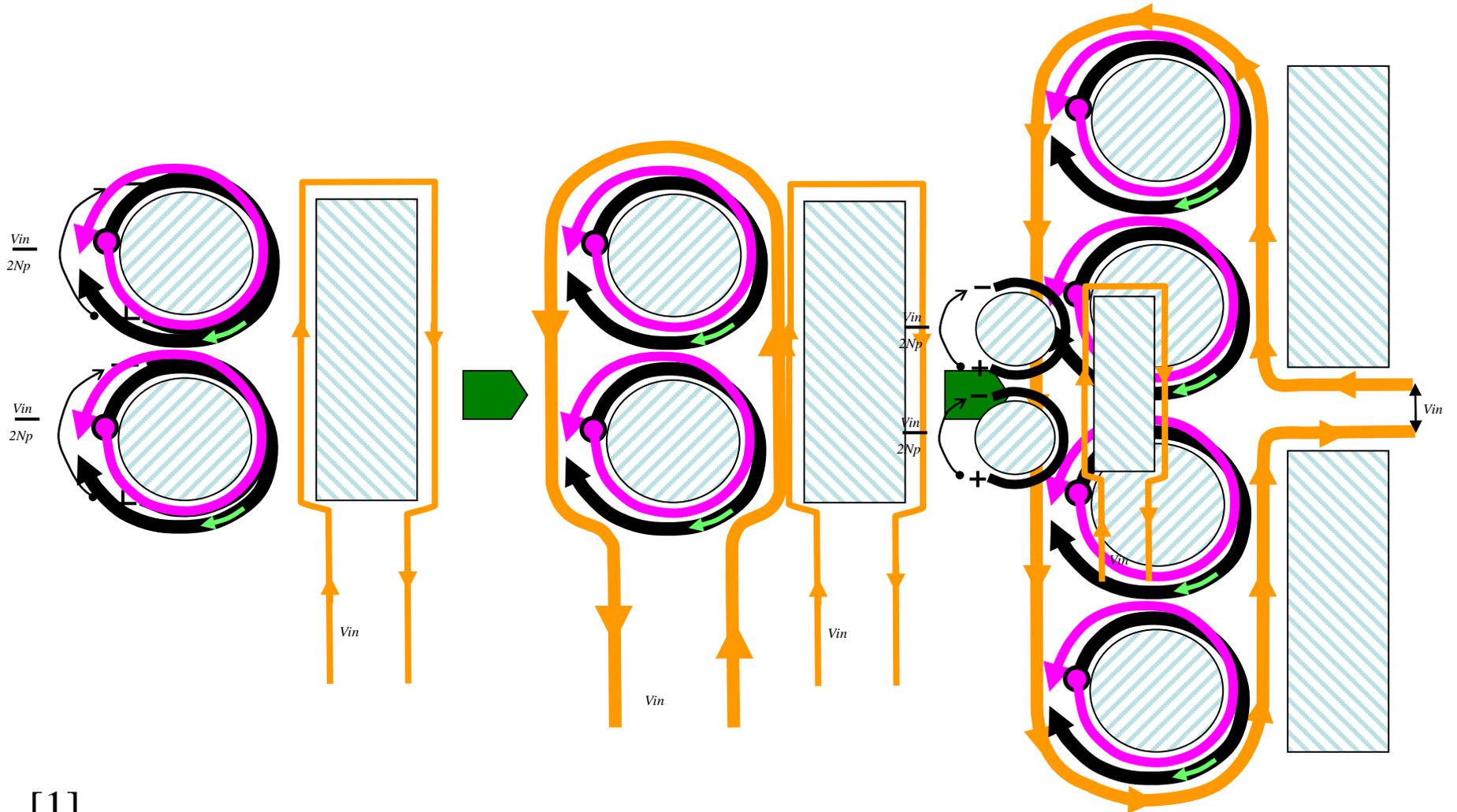
**MAGNETIC
STRUCTURES FOR
HIGHER
FREQUENCIES**

Magnetic Structures for High Efficiency

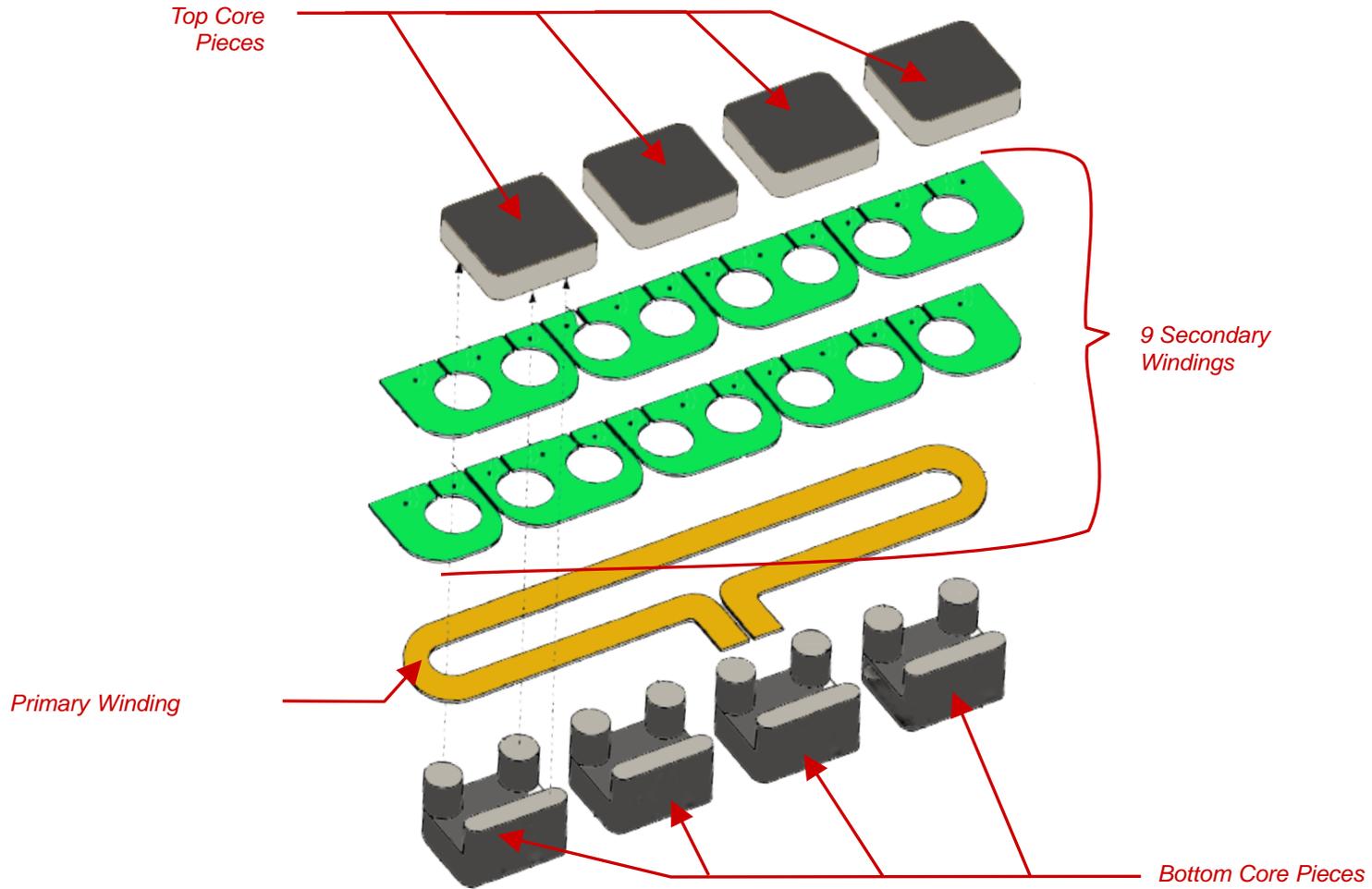


[1]

Magnetic Structures for High Efficiency



Printed Circuit Transformer



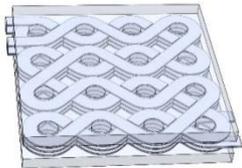
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[14]

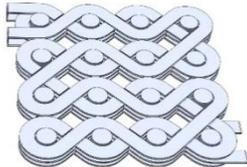
Magnetic Structures for Very High Frequency

Case	K[%]	1MHz		10MHz	
		P Ac/Dc	S Ac/Dc	P Ac/Dc	S Ac/Dc
1 Plates & Posts	99.9	2.26	3.26	3.75	4.54
2 No Core	54.8	2.2	2.63	3.58	3.57
3 Center Posts	72.9	1.72	1.93	3.05	2.61

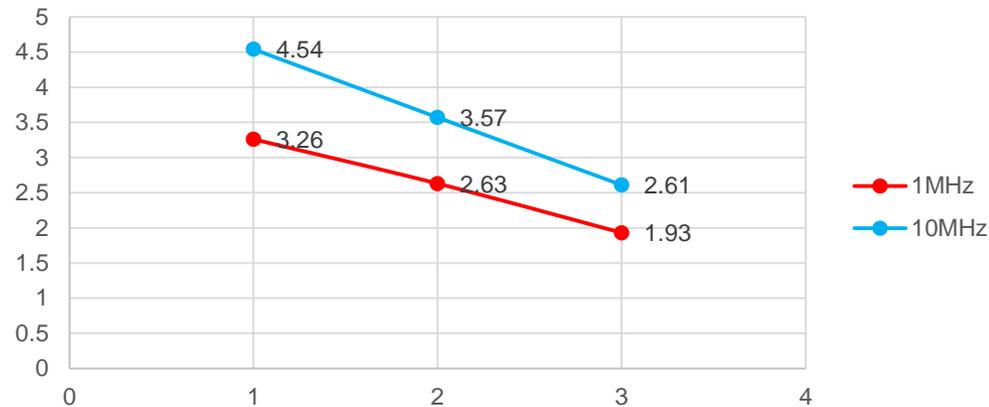
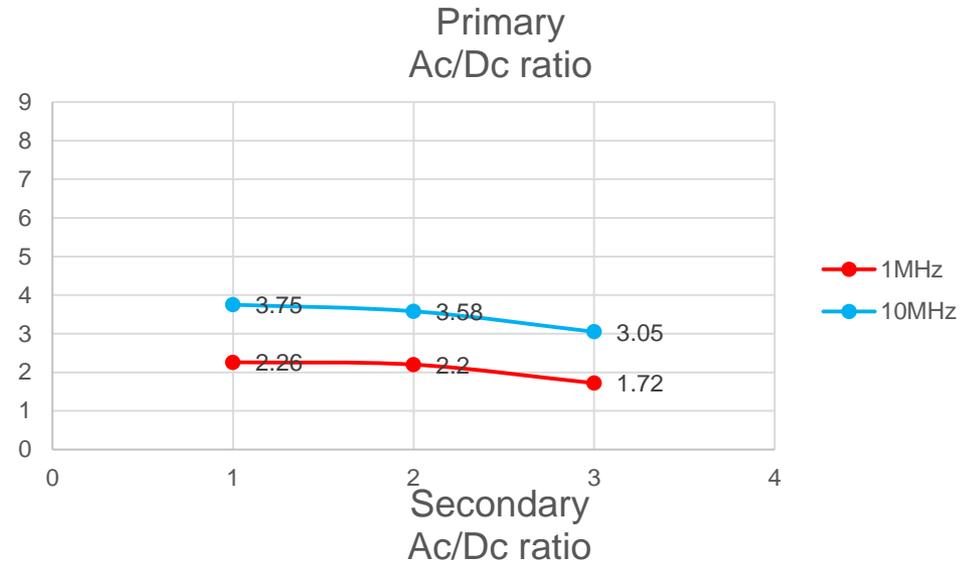
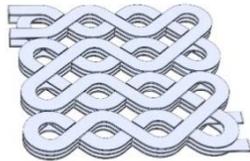
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[9]

MULTI-LEGGED MAGNETIC STRUCTURE

Rac/Rdc Characteristics

CONCLUSION

- **The main target is efficiency and smaller size which may lead to lower cost.**
- **Reduction of number of turns towards one turn secondary.**
- **For efficiency and size minimization present “true” soft switching topologies operate between 300KHz towards 1MHz with new semiconductor technologies.**
- **The new semiconductor technologies allows operation above 5Mhz but it may require high efficiency air core magnetic structures.**

Thanks!

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- [3] Ionel Dan Jitaru “Low Profile Magnetic Element”" US Patent # 7,295,094 B2
- [4] Ionel Dan Jitaru “Planar Inductive Element”" US Patent # 6,967,553 B2
- [5] E.C. Snelling, “Soft Ferrites, Properties and Applications" pp.335-338
- [7] Ionel Dan Jitaru "Low Noise Full-Integrated Multilayer Magnetic for Power Converters" US Patent 5,990,776
- [8] Ionel Jitaru “ Soft Switching Converter by Steering the Magnetizing Current” US Patent Pending
- [9] Ionel Jitaru “Magnetic Structures for Low Leakage Inductance for Low Leakage Inductance and Very High Efficiency” US Patent Pending” US Patent Pending

Some of the technologies presented in this seminar may be the subject of patent applications, please contact Rompower Energy Systems for further details.